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MICROWAVE LANDING SYSTEM PHASE III

(Basic Narrow and Small Community Configurations)



JUNE 1978

FINAL REPORT
Volume II

Document is available to the public through the National Technical Information Service Springfield, Virginia 22151



Prepared for

FEDERAL AVIATION ADMINISTRATION
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Washington D.C. 20591

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Technical Report Documentation Page 1. Report No. 3. Recipient's Catalog No. MLS-BCD-R-2801-1 Microwave Landing System (MLS), Report Date Jan Phase III. Performing Urganization Code (Basic Narrow and Small Community Configurations), final Report, vol. A. Performing Organization Report No. Volume I MLS-BCD-R-28Ø1-1-VOL-2 9. Performing Organization Name and Address
The Bendix Corperation 10. Work Unit No. (TRAIS) Communications Div East Joppa Road DOT-FA72WA-2801 Baltimore, Maryland 21204 13. Type of Report and Period Covered 12. Sponsoring Agency Name and Address Federal Aviation Administration Final Report, Vol. II Development Section C, ALG-313 800 Independence Avenue, S. W. 14. Sponsoring Agency Code Washington, D. C. 20591 15. Supplementary Notes This volume contains five Appendices to the Final Report. 16. Abstract Appendix A describes the design considerations that were applied to the Rotman lenses used in a Basic (Narrow) and a Small Community configuration for the Microwave Landing System. Appendices B thru E contain a detailed reliability and maintainability analysis of the two configurations including the airborne equipments. 18. Distribution Statement 17. Key Words Microwave Landing System, Basic Narrow Configuration, Small Community Configuration, Reliability, Maintainability

Form DOT F 1700.7 (8-72)

19. Security Classif. (of this report)

UNCLASSIFIED

Reproduction of completed page authorized

UNCLASSIFIED

20. Security Classif. (of this page)

4028 85

22. Price

21. No. of Pages

222

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SUMMARY

The Bendix Communications Division of The Bendix Corporation, was tasked, as prime contractor under DOT/FAA Contract DOT-FA72WA-2801, to design and fabricate two prototype Microwave Landing System configurations and to install them at the National Aviation Facilities Experimental Center (NAFEC) at Atlantic City, New Jersey.

The Basic Narrow configuration included ground azimuth, ground elevation, and DME subsystems and four airborne receivers. The Small Community configuration included ground azimuth and elevation elements and four airborne receivers.

The task has been successfully completed with the Basic Narrow and Small Community Ground Subsystems delivered to NAFEC in May 1976 and July 1976, respectively. The airborne subsystems have been installed and evaluated in numerous test aircraft. Independent field and flight testing by FAA (NAFEC) and Bendix personnel have proven that both systems meet or exceed the specified performance requirements.

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Appendix A

Design Considerations for Rotman Lens Antennas

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APPENDIX A

DESIGN CONSIDERATIONS FOR ROTMAN LENS ANTENNAS

A.1 INTRODUCTION

Rotman and Turner have derived various geometric relationships to minimize the phase aberrations across the aperture of a one-dimensional microwave lens antenna. In their work, they consider a lens in which the inputs consist of several horns, each of which generates a discrete beam in the far field. Scanning is accomplished by mechanically moving a horn along the focal arc.

For the MLS application, electronically steerable Rotman lens antennas were built. The inputs for these lenses consist of a number of closely spaced probes along the focal arc. The probes are spaced closely enough that exciting several simultaneously results in a single beam in the far field. Fine scanning is accomplished by electronically commutating a weighting function across the input probes. Design of a commutated lens posed several problems which are not considered in Rotman's work:

- (a) How closely spaced should the input probes be?
- (b) How many inputs should be simultaneously excited to generate a beam?
- (c) With that amplitudes and phases should the inputs be excited?

In addition to these problems, other problems were involved in determining an optimum lens geometry. Given a desired beamwidth and maximum steering angle, Rotman's equations do not yield a unique solution. One must specify three addition parameters (f, α , and g -- see Reference (l)) in order to uniquely

^{1.} Rotman and Turner, "Wide-Angle Microwave Lens For Line Source Applications", IEEE Transactions on Antennas and Propagation, November, 1963.

determine a lens design. Although Rotman offers some suggestions for appropriate values for these parameters, careful consideration must be given to their selection. It is the purpose of this appendix to explain how these problems were approached in the design of the MLS Rotman lens antennas.

A.2 COMPUTER SIMULATION

The major tool used in the design of the MLS Rotman lens antennas was a computer program BPORT. Given various lens design parameters (focal length, aperture size, etc.) BPORT used Rotman's equations to determine the contours of a lens antenna. The user could specify any combination of excitations on the inputs and BPORT would compute the resultant aperture distribution and far field pattern. Use of this program provided a means of evaluating the effects of different input weighing functions, input probe spacings, lens geometries, etc.

A second useful computer program was BPOR2. This program is essentially the inverse of BPORT. Whereas BPORT used given input excitations to compute a resultant far field pattern, BPOR2 used a given far field pattern (e.g., Taylor beam) to compute the required input excitations.

A.3 APPROACHES TO PROBLEMS

A.3.1 Lens Geometry

Given a desired beamwidth and maximum steering angle, Rotman's equations do not yield a unique lens design. One of the MLS lens design problems was to determine optimum Rotman lens design for a given application. Knowledge of the beamwidth, frequency, and maximum steering angle determines the number of aperture elements and the interelement spacing. Complete determination of a lens design requires the specification of three additional parameters: f, the focal length; a, the off-axis angle of perfect focus; and g, the ratio of the lens dimension from front to back to the focal length. In order to

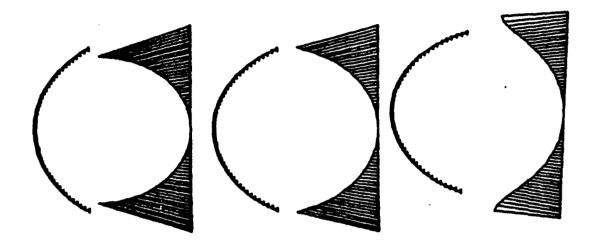
minimize phase aberrations across the lens aperture, Rotman made the following recommendations:

- (a) α should be near the maximum scan angle
- (b) f should be approximately equal to the aperture size (Rotman built a lens in which the focal length was 83% of the aperture size)
- (c) g should be equal to $1 + \alpha^2/2$

Rotman recommended these values in order to keep the maximum phase aberration less than ±0.003 of the focal length (less than 2° for the Basic Narrow Azimuth lens). If less stringent phase requirements are tolerable, then f and g can be reduced.

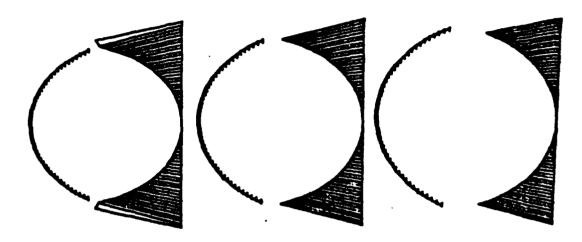
In designing the MLS lens antennas, it was discovered that internal reflections posed a much more significant problem than phase aberrations. The g parameter proved particularly critical in these considerations. A large value of g results in a large, highly curved focal arc (see Figure A-lc). A small value of g results in a highly curved lens surface (see Figure A-la). These highly curved surfaces will tend to reflect much of the energy within the lens and cause beam shape distortion and higher sidelobe levels. It was empirically found that for $\alpha = 40^{\circ}$, setting g = 1.10 caused both contours to have approximately the same curvature and minimized the internal reflections (see Figure A-lb). This value of g was used in the Basic Narrow and Small Community lenses.

The value of f affects the shape of the lens surface. A value of f that is too small results in a lens surface that begins to bend "backwards" (see Figure A-2). A value of f that is too large results in a large, unwieldy lens design (see Figure A-2c). It was decided to use a value of f that would minimize the antenna size without any "backward bending" of the lens surface (see Figure A-2b). The Basic Narrow and Small Community lenses have a focal length that is 57% of the aperture size.



a. g = 1.05 b. g = 1.10 c. g = 1.15 (actual lens geometry)

FIGURE A-1. EFFECT OF VARYING g PARAMETER ON LENS GEOMETRY $(\alpha = 40^{\circ}, f = 1.14 \text{ m})$



- a. f = 1.05 m
 (51% of aperture)
- b. f = 1.14 m
 (actual lens
 geometry)
 - c. f = 1.25 m
 (61% of aperture)

FIGURE A-2. EFFECT OF VARYING FOCAL LENGTH ON LENS GEOMETRY $(\alpha = 40^{\circ}, g = 1.10)$

A.3.2 Input Probe Spacing and Weighting Function

Through using BPOR2 to compute ideal input excitations, it was observed that each input probe had a characteristic phase associated with it independent of the beam shape and steering angle. It turned out that these phases corresponded to the path length differences between the various input probes and the lens center. By incorporating coaxial cables of varying lengths in series with each input probe to compensate for these path length differences, it was possible to decrease sidelobes, increase gain, and decrease beamwidth. These results were verified by BPORT and the cables were incorporated in the lens design. (Because Rotman excited only one horn at a time, it was not necessary for him to consider its phase.)

Through running BPORT, it was observed that excitation of a single input probe resulted in a nearly uniform aperture distribution and a far field pattern that is very nearly sin x/x (sinc (x)). It was proposed that the input probes should be spaced such that the sinc (x) beams generated by adjacent probes would be orthogonal. Beams generated by simultaneously exciting several probes with different amplitudes would be the superposition of several orthogonal sinc (x) beams of different amplitudes. A set of weights was also derived which would fine scan the beam in tenth beamwidth increments.

Considering the far field beams as the superposition of several sinc (x) beams clarified the significance of the input probe phases. If the input probe phases were not compensated for the path length differences, then the beams of adjacent sinc (x) patterns would not be in phase. Superposition of those out-of-phase beams would result in beam distortion. Because of the phase errors, the alternate sidelobes of adjacent

beams would not cancel each other and the sidelobe level would increase.

The input weighting function proposed has worked very well in the MLS lens antennas. These weights result in a nearly constant beam shape, theoretical sidelobe levels from -23 dB to -31 dB, theoretical beam gain changes of 0.06 dB over one cycle of 10 fine steps, and theoretical maximum beam pointing errors of 0.0134 of the probe spacing angle (approximately 0.02° error for the Basic Narrow lens). However, these weights are not necessarily the optimum weights for a Rotman lens antenna. For example, different weights may result in lower theoretical sidelobes at the expense of beam pointing accuracy. Future commutated lens designs may involve consideration of different weighting functions.

The orthogonal probe spacing has also worked very well. Orthogonality has the advantage that the input probe VSWR, excluding mutual coupling effects, is independent of the excitations on other input probes. However, there may be applications in which non-orthogonal spacing may be desirable. For example, closer spacing of the inputs and excitation of more than three inputs simultaneously may result in an improvement in beam pointing accuracy and sidelobe level. To do this, it would be necessary to determine a new weighting function.

A.4 CONCLUSIONS

The following recommendations are made for future designs of Rotman lens antennas:

- a. Phase aberrations have not been a serious limitation on the performance of the MLS Rotman lenses. Therefore, f and g should be chosen to minimize the lens size and the internal reflections.
- b. The phases of the input probes should be compensated for the path length differences between the probes

- and the lens center. These phases seem to be optimum whether or not the probes are spaced orthogonally and regardless of the input weighting function.
- c. Spacing the inputs orthogonally is probably optimum for most lens designs. However, it is possible that applications in which beam pointing accuracy or sidelobes are particularly critical may require non-orthogonal inputs.
- d. The input weighting function proposed and used in the MLS lenses has worked very well. However, it is not necessarily the optimum weighting function for all lenses. Future Rotman lens designs may warrant consideration of other input weighting functions.

Appendix B

Reliability Test Plan

for

MLS Ground Equipment

Contract No.

DOT-FA72WA-2801

prepared by

The Bendix Corporation

Communications Division

Towson, Maryland 21204

November 1977

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B.1 SCOPE

This document describes the test program which will be followed to demonstrate that the MLS Ground Subsystem Equipment meets the mean-time-between-failure (MTBF) requirements specified in the Functional Requirements Specification. The plan has been prepared in accordance with MIL-STD-781.

B.2 REFERENCED DOCUMENTS

The following specifications and references form a part of this test plan to the extent specified herein:

- a. MIL-STD-781B Reliability Tests: Exponential Distribution
- b. FAA-ER-700-07, Amendment 1, 2/25/75, revised 3/26/75, MLS Functional Requirements Specification
- c. Statement of Work, Appendix (Reliability, Maintainability and Demonstration Plan)
- d. 4041035 Engineering Test Procedure, Basic Narrow Azimuth Subsystem (Bendix document)
- e. 4041036 Engineering Test Procedure, Basic Narrow Elevation Subsystem (Bendix document)

B.3 GENERAL TEST REQUIREMENTS

B.3.1 NUMERICAL RELIABILITY REQUIREMENTS

The specified MTBF for the MLS Ground Subsystem equipment is 3000 hours for each functional element (azimuth, elevation, back course, etc.) For the reliability demonstration, functional elements may be interchanged if they are comparable in their design and general parts populattion. The DME is excluded from the demonstration.

B.3.2 DESCRIPTION OF TEST SAMPLE

The prototype demonstration will be performed on Civil Basic systems built in compliance with FAA-G-2100. Since the azimuth angle equipment and the elevation angle equipment are reasonably comparable in both design and part population, the reliability tests will be performed on a common functional element basis using basic narrow azimuth and elevation equipment.

B.3.3 GENERAL TEST PLAN

The prototype reliability demonstration will be performed in two phases; factory and field.

B.3.3.1 FACTORY DEMONSTRATION

Two functional elements (azimuth and/or elevation) will be placed on test, prior to shipment, so that each may accumulate five days of continuous operation with no restarts should failures occur. Corrective action will be taken for each failure.

Assessment of the validity of the corrective action will be accomplished by "off-line" test before continuation of the demonstration and ultimately through the results of the on-site field test.

Three additional elements will be tested using Test Plan XXV of MIL-STD-781B with no restarts. If failures occur, corrective action will be taken and verified by off-line test before continuation of the demonstration. This test plan is a short term (0.37 $\theta_{\rm O}$), fixed length, test with a 3/1 discrimination ratio and with consumer and producer risks of 30 percent.

A 48-hour burn-in period is allowed.

B.3.3.2 FIELD DEMONSTRATION

Demonstration tests in the field will involve all of the Basic Narrow elements fielded. The demonstration will be performed to Test Plan VI of MIL-STD-781B. This test plan is a short term (maximum -1.25 $\theta_{\rm O}$), variable length test with a discrimination ratio of 5 to 1 and with consumer and producer risks of 10 percent. Corrective action of failures will be in accordance with para. 5.7 of MIL-STD-781B.

B.3.4 TEST LEVELS

All factory reliability testing will be performed to Test Level A-1 of MIL-STD-781B to simulate the use environment. Test Level A-1 is a 25°C constant temperature test with no vibration or on/off cycling.

Field testing will be performed with each equipment installed and operating in its particular environmental shelter configuration.

B.3.5 Test Scheduling

The two-element factory test in paragraph B.3.3.1 will be performed on a 24-hour per day, 5-day per week basis until the specified test requirements are satisfied. The duration of this test will be 5 days of operation plus time lost for any corrective actions which may be required.

Factory tests to Test Plan XXV will be performed on a 24-hour per day, 7-day per week basis until the test requirements are met. The duration of this test is 1100 hours accumulated across three elements. Assuming equal distribution of time between the elements, the expected test duration is 16 days, plus time lost for the off-line verification of required corrective actions.

The field demonstration is a variable length test, depending on the number and frequency of failures, and can range from 1650 to 3750 accumulated hours, not including any time which may be required to perform retests. Assuming five elements, the expected duration of the field test would be about 5 weeks.

B.3.6 PERIODIC PERFORMANCE CHECKS

Performance checks will be made to determine equipment failures as defined in paragraph B.3.7. These checks will be made once every 24 hours during the normal working hours. For the factory tests, no measurements will be taken on weekends or holidays. Test instrumentation will be provided to the extent practical, to monitor and record the time of occurrence of equipment failures or test set-up malfunctions between performance checks.

The performance checks are given in paragraph B.5.3.

B.3.7 DEFINITION OF FAILURE

A failure during the reliability testing is defined as a malfunction in the equipment which causes a departure from the performance requirements to a degree which requires Facility shut down, i.e., an executive level equipment malfunction which fails to restart. Nuisance shut downs caused by operational considerations or external interference, rather than equipment malfunction, are not failures with regard to MTBF determination.

All failures will be classified with respect to dependency and relevancy in accordance with the following definitions:

1. Independent Failure: An independent failure is a failure which has no significant relationship to prior failures of other parts in the equipment. In the case of simultaneous related failures, at least one failure will be classified as independent.

- 2. <u>Dependent Failure</u>: A dependent failure is a failure which resulted either in part or in total from prior or simultaneous failures of other parts of the equipment or test set-up.
- 3. Relevant Failure: A relevant failure is a failure which does not fall into the nonrelevant classification. Relevant failures are chargeable to the equipment for determining accept/reject decisions.
- 4. Nonrelevant Failure: Any failure whose ultimate cause is due to accidental damage, mis-adjustments (operator), failure of another part (dependent), installation errors, operator errors, scheduled replacement, or failure of test equipment or facilities shall be classified as nonrelevant. Nonrelevant failures are not chargeable to the equipment and are not used for determination of accept/reject decisions.

B.3.8 DATA ANALYSIS

Compliance of the field test to the specification shall be determined by the accept/reject criteria given in Test Plan VI of MIL-STD-781B. Compliance will be reviewed after each equipment failure and when the accumulated test time reaches each accept decision point.

To synthesize the test data, accumulated hours and failures will be recorded in the Failure/Time Log and will be reviewed for compliance as noted above.

B.4.0 MODIFICATION OF UNITS FOR FACTORY TESTING

Each element (azimuth or elevation) will be operated with the equipment configured in an actual operating mode, and with power radiating. The far field monitor will be situated to receive the radiated signal so that the monitor subsystem is fully operational. Each element which is used in factory testing will be operated independently. That is, elevation elements will not be synchronized to azimuth elements.

B.5.0 TEST PROCEDURES

B.5.1 PRE-TEST CHECKOUT

Prior to all system tests, every unit is subjected to individual tests verifying satisfactory operation of each unit and of the supporting test equipment and facilities and subsystem performance. During these checkouts all necessary adjustments, calibrations and attrition replacements are made. These standard checkouts will be performed on the reliability test samples, and verification of their satisfactory completion recorded on the operator's log by the test conductor. In addition to these tests, a checkout will be made to verify that subsystem interfaces have been properly connected.

B.5.2 BURN-IN

Since all units and the equipment group will have been performance tested prior to commencing the reliability test, as noted in B.5.1 above, no formal burn-in is presently planned for the factory demonstration.

If the field demonstration is to commence immediately following equipment installation, a period of 48 hours of failure-free operation, under normal operating conditions, shall be accrued prior to the start of formal reliability testing to verify the proper installation of the equipment. This burn-in will be applied at the element (azimuth/elevation) level. After completion of the burn-in a reference set of measurements will be taken to assure that all burn-in failures have been detected and are corrected before the start of the reliability test. This test will consist of Engineering Test Procedure 4041035 for the Azimuth Subsystem and 4041036 for the Elevation Subsystem.

B.5.3 PERIODIC PERFORMANCE CHECKS

Performance checks will be made to determine if equipment failures, as defined in paragraph B.3.7 have occurred. The checks will be made daily as outlined in paragraph B.3.6. Results of these tests will be recorded in the appropriate subsystem status log (Figure B.8-2 or B.8-3).

Since the subsystems are self-monitoring, the daily performance checks will consist of recording the subsystem status.

The performance checks will be performed as follows:

- 1. Record the appropriate unit identification data.
- 2. Perform the lamp test on the Local/Control and Maintenance Monitor Panels.
- 3. Verify the Presence of Morse Code. (Note: Loss of Morse Code does not constitute an executive malfunction. This data is recorded for completeness.)
- 4. Record Subsystem Status by indicating on the Monitor Panel chart the lamps which are lit.
 - a. If the System Status executive function is normal, the check is completed.
 - b. If the System Status executive function indicates a fault;
 - 1. Record the lamps which are lit, for reference.
 - Place the Mode Switch on the Maintenance Monitor Panel in the maintenance position.
 - 3. Place the operate/test switch on the Local Control/Status panel in the test position.
 - 4. Operate the RESET switch on the Local Control/ Status Panel.
 - 5. Consult the chart recorder (if employed) to determine the time of occurrence of the outage.
 - c. If the subsystem successfully Resets, return the positions to the operate mode and record the appropriate data on the data sheet.

d. If the subsystem fails to reset, record the information in the appropriate logs and begin diagnosis to determine if an equipment failure has occurred as noted paragraph B.6.

B.5.4 UNATTENDED OPERATION

The equipment normally operates in the unattended mode. At the completion of the performance check, the chart recorder (if employed) should be checked to be sure that sufficient paper and/or ink is provided for the next interval.

B.5.5 REQUIRED SUPPORT EQUIPMENT

The support equipment required for the initial checkout is outlined in Engineering Test Procedures 4041036 and 4041036.

The support equipment for use during reliability testing, includes:

Oscilloscope Tektronix 545B or equivalent
Logic State Analyzer HP 1600A or equivalent
RF Detector HP 420 or equivalent
Dummy Load Narda 376NM or equivalent
Chart Recorder 2 channel (for each Element under Test)

B.6 FAILURE PROCEDURE

When a subsystem registers an executive fault which fails to reset, appropriate entries shall be noted in the General Test Log and the Subsystem Status Log. The first step in the diagnosis is to determine whether an equipment malfunction has occurred or whether the shut down is due to external causes (e.g. a truck parked near the test area disturbing the monitor pattern.)

If the shutdown is due to an equipment malfunction, appropriate entries shall be recorded in the failure/time log and troubleshooting procedures begun. The failed subsystem will be restored either by repair or replacement, whichever is appropriate.

If the failure involves a discrete part or module the procedures outlined in paragraph B.6.1 will be followed.

B.6.1 FAILURE REPORTING, ANALYSIS AND CORRECTIVE ACTION

If a malfunction involving a discrete part or module is revealed during a periodic check, it will be recorded on a defect tag whose format is shown in Figure B.8-7 and the necessary maintenance performed to restore system operation. Malfunctions causing system failure, as defined in B.3.7 will be entered in the failure/time log, Figure B.8-4. The failure will be investigated and the tagged failed part analyzed to discover its failure mode. Results of the analysis and an investigation of circuitry will be used in arriving at corrective action, consisting of a better part choice for the application or circuit redesign to improve performance. It should be noted that this corrective action will be applied to the system as defined in paragraph B.3.3. A description of each failure, its analysis, and recommended corrective action will be recorded in a failure analysis report, whose format is shown in Figures B.8-8 and B.8-9.

B.7 TERMINATION OF TESTS

The factory tests will be terminated upon the completion of the specified requirements. The two-element factory test in B.3.3.1 will be terminated when 120 hours of operation have been accumulated on each element, and correction action has been implemented for each failure.

The factory test To Test Plan XXV will be terminated when a total of 1110 hours have been accumulated and corrective action has been implemented for each failure.

The field test will continue until either an accept or reject decision is reached in accordance with paragraph B.3.8. If a reject decision is reached the following procedure will be initiated:

- a. Testing will be halted.
- b. The results of the analysis of the failed part causing the reject decision together with the failure reports on all pertinent preceding failures will be reviewed for the corrective action recommendations. Appropriate corrective actions will be undertaken with the concurrence of the procuring activity.
- c. A retest will be performed.

B.8 TEST RECORDS

Continuous test records will be kept throughout each of the reliability demonstrations. The data that will be recorded include performance check data, test time, number of failure, test facility data, and failure analysis data.

B.8.1 GENERAL TEST LOG

The General Test Log will be used to provide a chronological record of all test activities and interruptions occurring during the test to both the test units and the test facilities. Figure B.8-1 gives a sample of the General Test Log.

B.8.2 SUBSYSTEM STATUS LOG

A Subsystem Status Log will be kept for each unit under test to provide a complete history of the equipment. In this log will be recorded all performance data, and running time meter readings. These logs are given in Figures B.8-2 and B.8-3.

B.8.3 FAILURE/TIME LOG

Figure B.8-4 shows the Failure/Time Log. This sheet provides a separate tabulation of all data necessary for reaching an occept or reject decision. Entries will be made each time an apparent equipment failure occurs, and at the accumulation of the discrete test times associated with accept decision points.

B.8.4 FACILITIES AND CALIBRATION LOG

A log shall be kept of all test equipment in use at any time during the reliability test together with a record of calibration dates and the period of allowable use before recalibration. A sample of this log is given in Figure B.8-5.

B.8.5 EQUIPMENT FAILURE SUMMARY LOG

A summary log of equipment failures will be kept to provide a ready reference of all equipment failures along with the RTM readings required, to delete from accumulated test time the equipment operating time logged retween the time of failure and the return of the restored equipment to test. Such invalid operating time includes time logged between the time of failure and the start of normal working hours, and time logged during failure verification, and equipment checkout. A sample log is given in Figure B.8-6.

B.8.6 FAILURE RECORDS

Figure B.8-7 shows the defect tag for the recording of information pertaining to malfunctions of discrete parts or modules.

Figures B.8-8 and B.8-9 give the failure report form which will be kept for all failures occurring during the reliability test. The first part of the report concerns equipment symptoms and data pertinent to the reliability test. The second part of the report is the analysis section, recording the ultimate cause of failure and corrective action recommendations.

General Test Log Reliability Test MLS Basic Narrow Ground Subsystem Angle Elements

Entry No.	Date	Time	Remarks	Init.
			-	
		<u> </u>		

Figure B.8-1

Azimuth Element Subsystem Status Log

ET.	ement	S/N					I	Data S	Sheet	Page	No		-
Re	ferenc	ce :	Genera	l Tes	st Log	Entr	y No.		_ Test				
Da	te				Time					RI	M		_
La	mp Tes	st:	Local	Cont	rol/St	atus	Panel		OK;		LED	OUT	
	-		Mainte	enance	e Moni	tor F	anel		OK;		LED	OUT	
Мо	rse Co	ode:		OK;		FAUL	T.						
							Indic	ations	5				
			(Check							Reset))		
/ 5	YS STA	TUS -	•	. -		ODE			NITOR			AMP	
FAULT	0			•	of the			a di	2				
NORM	0	0											
					W /	TMP			•				
			·		·	- EXECL	JTIVE ~	·					
FIEL	D MONI	TOR —					ENNA -						
Bram Maj a	BEAM	TEST PULSE	PRAMEL.	LEFT		ERF	SW		CONT				*
C	O	0	0	0	0	0	0	. 0	0	0	0	0	1
					MAINTE	NANCE	MONITO	R ———					
~ PWE		SMITTER			- DATA -				MP —	AC	- UPS - BTRY	RVS	
ATWT		PHASE		BSC I			LINK	ELEC	_	PWR	LIM	XFR O	
			_	_	ER SUPPLI	_	_						
+5	ANTELNA -40	+24			TRONICS -15			MON	TOR	-15			
0	0	0	0	0	0	0	0	0	0	0			
E	œcuti	ve S	tatus	After	Rese	t	No:	rmal		Faul	t		

Figure B.8-2

Elevation Element Subsystem Status Log

			Genera		st Loc								
											rm		-
La	mp Te	st:	Local	Cont	rol/St	atus	Panel	·	_ ok;		LED	OUT	
			Mainte	nanc	e Moni	tor I	Panel		_ OK;		_ LED	OUT	
Mo	rse C	ode:		OK;		FAUI	LT						
				Mon	itor F	Panel	Indic	ation	s				
			(Check	Lam	ps Whi	ich A	re Lit	Ве	fore	Reset			
<u></u> S	YS ST	ATUS -		- ;-		ODE			NITOR			LAMP	
FAUL	7 0	0		•	er.			K	ESET			TEST	
NORN	• 0	0						ŧ				(0)	
					w	INT							
- FIFE	D MON	TOR —				EXECL	JTIVE -			-	·		
ERP		UHALT -			LS —	ANT	ENNA -	- SCAN				_	
C C	EEAM	PULSE	PRAMEL	LEFT	RICINT	erh	SW	MOD	CONT	CONT	TPEQ	DME REPLY	MON TMG
													J
		SMITTER		•	MNNTE		MONITOR	₹			- :P5 -	_	
WTA	STOKE STOKE	PHASE		BSCI			DATA	ELEC.	TI:A		BTRY	R/S XFR	
0	0	0	0	0		0		.0	0	0	.0	0	
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<u>ö</u> _	Ö	Ö	Ö	Ö	0	0	Ö	Ö	Ö	0			
	ecut:		tatus /		Rese			mal		Faul	t		
_													

Figure B.8-3

Failure/Time Log Reliability Test MLS B/N Ground Subsystem Angle Elements

Failure Time on	•	2-10 2011-0
Falled Element		

Figure B.8-4

Facilities & Calibration Log

\		Date on Test	
tion Entry		No. & Due Date	
Recalibration		Asset 1 Calib.	
or		Date on Test	
Replacement		No. & Due Date	
		Asset Calib.	
		Date on Test	
	Initial	ž	
-		and Asset Calib.	
		Equipment Model No.	
		Item No.	

Figure B.8-5

Equipment Failure Summary Log

_		
	Remarks	
Failed	Board, Module, LRU	
Failed	Unit, Drawer, Assembly	
	Failure Report No.	
	Element RTM	
	ent S/N	
	Failed Element Description S/N	<i>y</i>
	Date & Time Replaced	
	Date & Time Removed	
	Line No.	

Figure B.8-6

SAU SECT | 15-04 | 15-04

BENDIX RADIO NYTHAN AV SERIEZ AVIATION SOMPHATION TEST AND INSPECTION DEFECT TAG

QTY.
l. O. #
DATE
FOR DEFECT

r Assy. Circuit Symbol	Repair Time	Originator
Discrepancy Date System Pkg. Mod. or Assy.	Log Book No. Symptoms:	Date

1. Discrepancy Date - Enter here the date the part malfunction occurred.

2. Part No. - Enter here the Bendix number assigned to the part. This number will appear on the body of the part if large enough and will also appear in the assembly parts lists for the assembly the part is to be removed from.

3. System Pkg. MCd. or Assy. - Enter here the name of the assembly the part is to be removed from. This name will appear on the assembly name plate.

4. Part Name - Enter here the common name of the part removed, such as tube, transistor, resistor, etc.

5. Circuit Symbol - Enter here the circuit symbol that applies to the part that is to be removed. This symbol will appear on the assembly circuit schematic diagram and also on the assembly parts list for the assembly the part is to be removed from.

6. Log Book No. - Enter here the Log Book Number, page number, the entry line number in the Log Book that lists the defect being tagged.

The equipment log book is maintained by the cognizant design engineer or test supervisor.

7. Repair Time - Enter here the time actually used to remove the part and to install a replacement part, in minutes. Do not count the time to obtain a replacement part, or to obtain tools or test equipment.

8. Symptoms - Enter here the most appropriate of the following symptoms; choose only one - Circuit not operating

Circuit out of tolerance

Overheating

Circuit intermittent
Other

If "Other" is entered, tell briefly how the malfunction affected circuit operating conditions.

9. Date - Enter here the date the defect tag is signed.

10. Originator - Enter here the name of the indvidual who filled out the defect tag.

Figure B.8-7

FAILURE ANALYSIS REPORT NO. _____

RELIABILITY TEST

Discrepancy Date Test Operator Failed Element: Serial No Serial No Failed Board Serial No Line No Test Data Log Line No. Unit Accum. Operating Time Troubleshooting Time Replacement Time Associated Defects (Log, Page, Line) Failure Symptoms:	MLS Ground Subsystem Si	heet 1 of 2
Failed Unit/Drawer Serial No. Failed Board Serial No. Operator's Log Line No. Test Data Log Line No. Unit Accum. Operating Time Troubleshooting Time Replacement Time Associated Defects (Log, Page, Line) Failure Symptoms:	repancy Date Test Operator	
Serial No. Operator's Log Line No Test Data Log Line No. Unit Accum. Operating Time Troubleshooting Time Replacement Time Associated Defects (Log, Page, Line) Failure Symptoms:	ed Element:	
Operator's Log Line No Test Data Log Line No. Unit Accum. Operating Time Troubleshooting Time Replacement Time Associated Defects (Log, Page, Line) Failure Symptoms:	ed Unit/Drawer Serial No	
Unit Accum. Operating Time Troubleshooting Time Replacement Time Associated Defects (Log, Page, Line) Failure Symptoms:	ed Board Serial No	
Replacement Time Associated Defects (Log, Page, Line) Failure Symptoms:	ator's Log Line No Test Data Log	Line No.
Associated Defects (Log, Page, Line)	Accum. Operating Time Troubleshooting Time	_
Failure Symptoms:	acement Time	
•	ciated Defects (Log, Page, Line)	
Diagnostic Tests:	·	
	nostic Tests:	
Corrective Action to Repair Equipment:	ective Action to Repair Equipment:	

Figure B.8-8

RELIABILITY LABORATORY ANALYSIS REPORT

Figure B.8-9

RELAS 1A: 1-77

B-20



Bendix Communications Division

	NO			•	l					PAGE	0	F_	
COMP	ONENT/PART NAME PER GE	NERIC CO) E		Program	1	Req	veste	,	Request	No.		
-					Equipm	ent S/N	Nex	t Ass	/. Name	1	Day	Mo.	Yr.
					Failure	Site/Date	Nex	t Ass	y. P/N	Request			
LOG B	00KP	P		8Y						Test		_	_
OBJEC	TIVE/PURPOSE/SYMPTOM				TORRI	No.	Ass	, Ope	erate Time	Compl. Report		-	+
										Compl.			<u> </u>
					Ckt. Sy	mbol	Test	Тур	, etc.				
THIS T	'EST (SUPERSEDES) (SUPPLE	MENTS) R	EPOF	RT(S) NO:									
Item	Part Type, Size, Rating, Lo	ot, etc.		Vendor and H4	Code	Vendor P/N	& Da	te Co	de In	d/Govt. St	d. No.		Qty.
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2			_										
			\prod										
BCD S	PECS/DWGS, ETC.		MI	IL SPECS/STD. ET	c.			VEN	DOR, OTHE	R SPECS			
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Appendix C

RELIABILITY, MAINTAINABILITY, HUMAN FACTORS AND SAFETY REPORT

Contract No.
DOT FA72WA-2801

Prepared by

The Bendix Corporation Communications Division Towson, Maryland 21204

November 1977

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RELIABILITY, MAINTAINABILITY, HUMAN FACTORS AND SAFETY REPORT

C.1 INTRODUCTION

This document is a final Reliability, Maintainability, Human Factors, and Safety Report covering results of analysis efforts on the Basic Narrow and Small Community Ground Equipment during Phase III of the MLS Program.

C.2 REQUIREMENTS

FAA-ER-700-07 specifies a mean-time-between-failures (MTBF) of 3000 hours for each of the Azimuth, Elevation, and DME functions, with a total system MTBF of 1,000 hours for the Basic Narrow Ground Equipment. Since the specification was prepared, the decision to utilize a commercially available DME has deleted this equipment from the reliability specification. Therefore, the system MTBF requirement for the Basic Narrow Azimuth and Elevation functions of the Ground Equipment is 1,500 hours,

The maintainability requirement is a mean-time-to-repair (MTTR) of 0.5 hours.

C.3 ANALYSIS RESULTS

C.3.1 RELIABILITY ANALYSIS

The reliability predictions for the Ground Equipment were performed in accordance with the procedures in MIL-STD-756A and using the prediction data in MIL-HDBK-217B as the primary source for failure rates. Failure rates of SMA connectors for semi-rigid cable were derived from field data obtained during the last phase.

C. 3.1.1 Environmental Factors

Fixed ground environmental factors were used at the expected operating ambient temperature of 25° C. Temperature rises of from 0° to 10° C were applied based on the location in the cabinet rack. These temperature rises were added to the

ambient temperature in performing the prediction. That is, for an assembly with a 10° C internal rise, the prediction was made using 35° C to enter the part failure rate tables of MIL-HDBK-217B.

C.3.1.2 Quality Factors

For the Basic Narrow Configuration, the quality factors used represent the actual parts complement supplied in the Phase III Basic Narrow hardware. Essentially, FAA-G-2100 parts were assumed, the MIL-HDBK-217B factors being military specification with high-rel quality factors for M level parts. For integrated circuits, Bl level quality factors were used, and for discrete semiconductors JAN level factors were used.

For the Small Community Configuration, lower quality level factors were used to represent a more commercial configuration. Generally, nonhigh reliability passive parts were assumed and "C" level quality was assumed for the integrated circuits. The quality level for discrete semiconductors was generally assumed to be JAN.

C.3.1.3 Detailed Reliability Analysis Results

C.3.1.3.1 Basic Narrow Configuration - The results of the reliability prediction for the Basic Narrow Configuration yield an MTBF of 4,580 hours for the active azimuth equipment and 5,570 hours for the active elevation equipment. The MTBF's predicted for the executive monitoring are 7,760 hours for the azimuth monitoring and 8,840 hours for the elevation monitoring.

The combined MTBF for the system functions and executive monitoring are: azimuth - 2,880, elevation 3,420. These figures yield a total system MTBF of 1,560 hours.

Paragraph 1.2 of the Appendix to the Functional Requirements Specification (FAA-ER-700-07) implies that the monitoring functions should be at least 10 times more reliable than the equipment being monitored. This requirement further

implies a monitor which is of very simple complexity to achieve an MTBF in the order of 30,000 hours. The integrity section (paragraph 11.0) of the same specification requires monitoring with sophistication sufficient to validate correctness of operation for all variations of the ground facility, instantaneous status changes, two-step monitoring/alarm and communication of status changes. The hardware complexity required to meet the integrity and monitoring specifications is not consistent with the simplicity implied in the statement that the monitoring should be 10 times more reliable than the system.

The approach, therefore, has been to simplify the monitoring to the maximum extent deemed appropriate for meeting the integrity requirements, and designing this required monitoring for high reliability. The individual items comprising the executive monitor are each highly reliable. However, the number of different functions which must be monitored to ensure maximum integrity precludes a simplified monitor approach.

In addition to the executive monitoring, maintenance monitoring is provided to aid in isolating failures to the faulty LRU. This maintenance monitoring is not included in the model since it has no effect on system operation and performs no executive or downgrading function. The MTBF's of the maintenance monitoring was calculated, however, for inclusion in the calculations for average number of maintenance actions required. The maintenance monitor MTBF's are 19,070 hours for azimuth and 20,870 hours for elevation.

Figures C.1 thru C.4 show the reliability models for the Basic Narrow Configuration. Figures C.5 thru C.8 contain the computer output summaries of the reliability prediction. The prediction details, showing the part level failure rates are too voluminous for inclusion in this document. They are on file at Bendix and will be made available for customer review upon request.

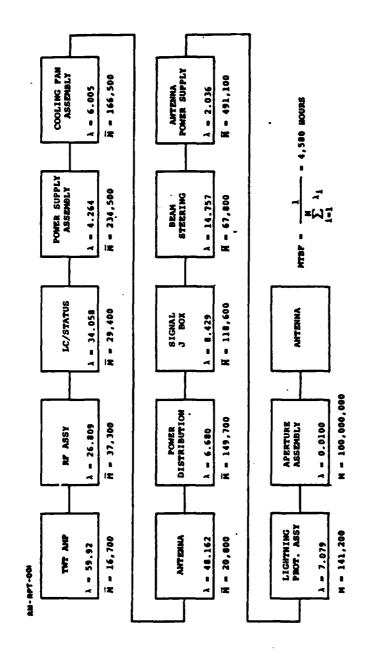


FIGURE C.1. BASIC NARROW AZ ACTIVE RELIABILITY MODEL

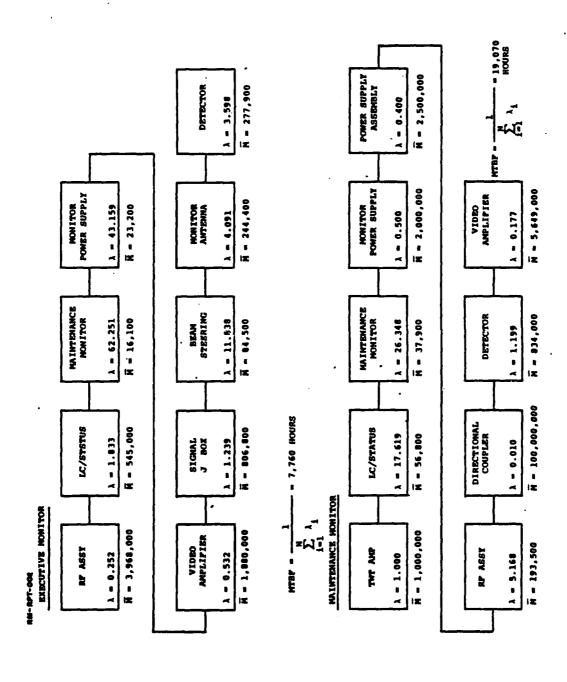


FIGURE C.2. BASIC NARROW AZ MONITOR RELIABILITY MODELS

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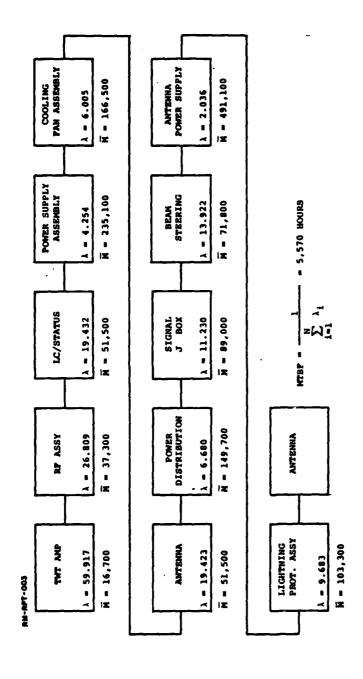


FIGURE C.3. BASIC NARROW EL ACTIVE RELIABILITY MODEL

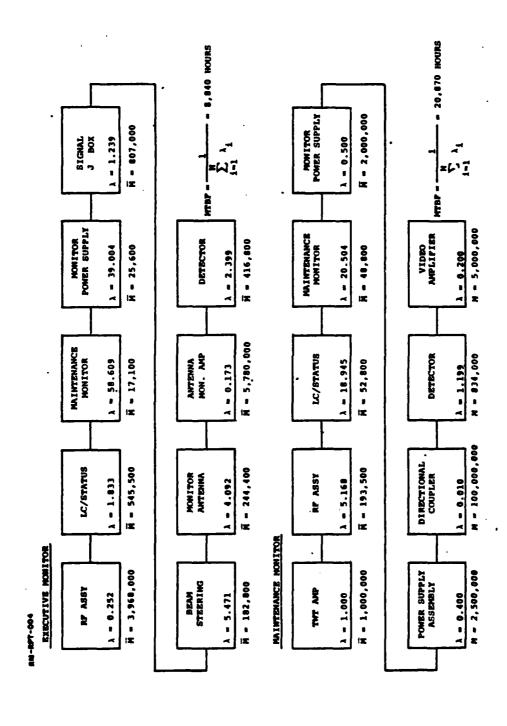


FIGURE C.4. BASIC NARROW EL MONITOR RELIABILITY MODELS

ASSEMBLY	SUBASSEMALY	POARD	(F.R.1)
ACTIVE EQUIP	TUT AMP ATATAT	CHASSIS (Q= 1)	4.03096
ACTIVE EQUIP	TATAMP ATATAT	PCB (Q= 1)	4.26836
ACTIVE EQUIP	THT AMP A1A1A1	H/V BOX (9= 1)	1.59270
ACTIVE EQUIP	THE AMP ATATAT	RF COMPONENTS (Q= 1)	50.02470
ACTIVE EQUIP	RF ASSY ATATAZ	(9= 1)	1.84141
ACTIVE EQUIP	RF ASSY ATATAZ	EXCITER ATATAZAT (Q= 1)	11.64571
ACTIVE EQUIP	RF ASSY A1A1A2	DPSK ASSY A1A1A2A2 (Q= 1)	2.67856
ACTIVE EQUIP	RF ASSY A1A1A2	AMP MOD ATATAZAS (Q= 1)	9.02338
ACTIVE EQUIP	RF ASSY A1A1A2 RF ASSY A1A1A2	ISOLATOR P/O A1A1A2(Q= 1) ATTEN, VAR P/O A1A1A2(Q= 1)	0.76745 0.85252
ACTIVE EQUIP	LC/STATUS ATATAS	(Q= 1)	6.79174
ACTIVE EQUIP	LC/STATUS ATATAS	SYST SYNC ATATASAS (Q= 1)	0.65755
ACTIVE EQUIP	LC/STATUS ATATAS	DATA LINK ATATASA4 (R= 1)	1.83593
ACTIVE FOUIP	LC/STATUS A1A143	DAT LK AUXATATASA6 (Q= 1)	1.76248
ACTIVE EQUIP	LC/STATUS ATATAS	VAP AUX A1A1A3A10 (Q= 1)	1.70685
ACTIVE EQUIP	LC/STATUS A1A1A3	FIX AUY 2 ATATASATT (Q= T)	2.12219
ACTIVE EQUIF	LC/STATUS A1A1A3	FIX AUX 1 A1A1A3A12 (Q= 1)	2.12219
ACTIVE EQUIP	LC/STATUS A1A1A3	AUX DS/WV A1A1A3A13 (Q= 1)	1.31403
ACTIVE EQUIP	LC/STATUS A1A143	AU/AD/PAR A1A1A3A14 (Q= 1)	1.60242
ACTIVE EGHIP	LC/STATUS A1A1A3	MORSE COD A1A1A3A15 (G= 1)	1.36476
ACTIVE EQUIP	LC/STATUS A1A1A3	ID/80/DPS A1A1A3A16 (Q= 1)	1.65630
ACTIVE EQUIP	LC/STATUS A1A1A3	SYS TIM GEATATA3A17 (Q= 1)	2.13297
ACTIVE EQUIP	LC/STATUS A1A1A3	TIM CHTRL A1A1A3A18 (9= 1)	5.54339
ACTIVE EQUIP	LC/STATUS A1A1A3	10 MHZ DR A1A1A3A19 (Q= 1)	0.05236
ACTIVE EQUIP	LC/STATUS A1A1A3	(1 =P) TYEATATADZO SHM OT	3.39331
ACTIVE EQUIP	PS ASSY A1A1A6	(Q= 1)	1.61052
ACTIVE EQUIP	PS ASSY A1A1A6	20v p.suppalala6ps1 (q= 1)	0.75369
ACTIVE EQUIP	PS ASSY A1A1A6	15V P.SUPPATATA6PS2 (9= 1)	1.29561
ACTIVE EQUIP	PS ASSY ATATA6	5V P.SUPP A1A1A6PS3 (Q= 1)	0.60455
ACTIVE EQUIP	COOL FAN A1A191	(9= 1)	6.00519
ACTIVE EQUIP	ANTENNA	SCAN SWIT A251-16 (9=16)	38.10316
ACTIVE EQUIP	ANTENNA	SCAN MOD. AZAZ (Q= 1)	8.84140
ACTIVE EUUIP	ANTENNA	ANT.SEL.SWATATST (9= 1)	1.21734
ACTIVE EQUIP	PUR.DIST AIN1	(Q= 1)	6.68013
ACTIVE EQUIP	SMIA XOU L DIZ Smia xou l diz	i PB NO1 (9= 1)	1.79791
ACTIVE EQUIP	SIG J BOX AINZ	LPB NO1 (Q= 1) LPB NO4 (Q= 1)	1.79791
ACTIVE EQUIP	DM STEER. AZAT	LPB NO4 (9= 1) (9= 1)	4.83352 4.04673
ACTIVE FOULE	BM STEER. AZA1	SCAN CHTR AZATAT (Q= 1)	2.51020
ACTIVE EQUIP	PM STEER. AZA1	SC.CH.COMPAZATAZ (Q= 1)	1.94641
ACTIVE EQUIP	BM STEER. AZA1	SC.SW.DRIVAZATA4 (Q= 1)	1.53663
ACTIVE EQUIP	AM STEER. AZA1	SS DR. INT. AZA1A5 (Q= 1)	2.07627
ACTIVE ECUIP	RM STEER. AZAT	10 MHZ OSCAZATY1 (9= 1)	2.64071
ACTIVE ENUIP	ANT.PS.ASYAZA4	(Q= 1)	0.08207
ACTIVE EQUIP	ANT.PS.ASYAZA4	5V P.SUPP AZA4PS1 (9= 1)	0.60696
ACTIVE EQUIP	ANT.PS.ASYAZA4	24V P.SUPPAZA4PSZ (Q= 1)	0.62664
ACTIVE FQUIP	ANT.PS.ASYAZA4	4UV P.SUPPAZA4PS3 (Q= 1)	0.72043
ACTIVE EQUIP	L.P.ASSY AZAS	LPB NOT AZASAT (Q# 1)	1.79791
ACTIVE FOUIP	L.P.ASSY AZAS	LPB NO5 AZASAZ (Q= 1)	5.28136
ACTIVE EAUTP	APPER ASY AZET	(Q= 1)	0.01000
OVERALL FAILURE R	ATES FOR THIS EQUIPMENT		218.20727
OVERALL TIBE FOR	THIS EQUIPMENT		4582.79981

FIGURE C.5. BASIC NARROW AZ ACTIVE RELIABILITY PREDICTIONS

ASSEMBLY	SUBASSEMBLY	BOARD	(f.R.1)
EXEC MON EQUIP	RF ASSY A1A1A2	DET AMP A1A1A2AP1 (0= 1)	0.25219
EXEC MON EQUIP	LC/STATUS A1A1A3	SEQ/TIMER A1A1A3A2 (Q= 1)	1.83305
EXEC MON EQUIP	MAINT.HON ATATA4	EXEC INT. P/O A1A1A4(Q# 4)	9.20685
EXEC MON EQUIP	MAINT.MON ATATA4	MON CHTRL A1A1A4A6 (Q= 1)	1.11803
EXEC MON EQUIP	MAINT.MON ATATA4	MORSE COD ATATAGA? (9= 1)	1.57129
EXEC MON EQUIP	MAINT.PON A1A1A4	DPSK DECO A1A1A4A8 (Q= 1) DPSK DECI A1A1A4A9 (Q= 1)	1.06563
EXEC MON EQUIP	AATATA NOM.THIAM AATATA NOW.THIAM	DPSK DECI ATA1A4A9 (Q= 1) DISC DATA A1A1A4A10 (Q= 1)	3.05165 0.97163
EXEC MON EQUIP	MAINT, MON A1A1A4	RECLOCK DRATATA4A73 (Q= 1)	0.53102
EXFC MON FQUIP	MAINT, MON A1A1A4	ID/BD/DPS A1A1A4A25 (Q= 1)	1.65630
EXEC PON EQUIP	MAINT.MON A1A1A4	SYS TIM GEATATAGAZ6 (Q= 1)	2.34612
EXEC MON EQUIP	PATATA NOM.THIAM	MON TIM A1A1A4A28 (Q= 1)	1.22542
EXEC MON EQUIP	MAINT.MON ATATA4	SCAN TIM A1A1A4A29 (Q= 1)	16.59309
EXEC MON EQUIP	MAINT, MON ATATA4	AN.COM.#1 A1A1A4A3D (Q= 1)	2.35163
EXEC MON EQUIP	MAINT.MON A1A1A4	DET/COMP A1A1A4A31 (Q= 1)	0.89428
EXEC MON EQUIP	MAINT.MON ATATA4	BE ACC CO A1A1A4A32 (Q= 1)	5.18528
EXEC MON EQUIP	MAINT.MON ATATA4 Maint.mon atata4	DIG COMP. A1A1A4A33 (Q= 1) FREQ MON. A1A1A4A34 (Q= 1)	10.43492
EXEC MON EQUIP	MON PS ASYATATAS	(Q= 1)	3.44774 3.13538
EXEC MON EQUIP	MON PS ASYATATAS	C BAND LO ATATASATAT(G= 1)	11.64572
EXEC MON EQUIP	MON PS ASYATATAS	RF MODULE A1A1A5A1A2(Q= 1)	19.97954
EXEC PON EQUIP	MON PS ASYATATAS	REG/BUFFERATATASATA3(Q= 1)	0.87728
EXEC MON EQUIP	MON PS ASYATATAS	MIXER A1A1A5A1Z1(Q= 1)	0.90727
EXEC MON EQUIP	MON PS ASYATATAS	PWR DIV. A1A1A5A1ZZ(Q= 1)	1.17393
EXEC MON EQUIP	MON PS ASYATATAS	50 OHM TERATATASATT (Q= 1)	2,94888
EXEC MON EQUIP	MON PS ASYATATAS	SV P.SUPP ATATASP1/2(9= 2)	1.19760
EXEC MON EQUIP	MON PS ASYATATAS	TSV P.SUP ATATASPS3 (R= 1)	1.29357
EXEC MON EQUIP	VIDEO AMP P/O A1AR Detector P/O A1CR	(Q= 3)	0.53227
EXEC MON EQUIP	DETECTOR P/O A1CR SIG J BOX A1N2 ·	(9= 3) LPB NO2 (9= 1)	3.59824 1.23940
EXEC MON EQUIP	BM STEER AZA1	SC.CN.MON.AZATA3 (Q= 1)	2.66057
EXEC MON EQUIP	DM STEER AZAT	SS MONITORAZATA6 (Q= 1)	2.81032
EXEC MON EQUIP	BM STEER AZA1	SS MON EXPAZATAT/A8 (Q= 2)	4.33291
EXEC MON EQUIP	BM STEER AZA1	SS MON INTAZATA9 (Q= 1)	2.03421
EXEC MON EQUIP	MON ANT A3	PWR DIST A3N1 (Q= 1)	0.26955
EXEC MON EQUIP	MON ANT A3	LPB NO 3 (9= 1)	0.91843
EXEC MON EQUIP	MON ANT A3	VIDEO AMP A3NZAR1 (Q= 1)	0.23044
EXEC MON EQUIP	MON ANT A3	RF DET A3N2CR1 (Q= 1)	1.10134
EXEC MON EQUIP	MON ANT A3	BAND FILT AJN2FL1 (9= 1)	0.62870
EXEC MON EQUIP	MON ANT A3 TWT AMP A1A1A1	PWR DIV A3NZZ1 (Q= 1) CHASSIS (Q= 1)	0.94305 1.00000
MAINT MON EQUIP	RF ASSY A1A1A2	TERMIN. P/O A1A1A2(0= 3)	2.55757
MAINT MON FOUIP	RF ASSY A1A1AZ	DETECTOR P/O A1A1A2(Q= 2)	2.61000
MAINT MON EQUIP	LC/STATUS A1A1A3	(Q= 1)	13.75825
MAINT MON EQUIP	LC/STATUS A1A1A3	LT DR/ALM A1A1A3A1 (9= 1)	1.86031
MAINT MON EQUIP	LC/STATUS A1A1A3	LC/ST.IND.A1A1A3A20 (Q= 1)	1.99999
MAINT MON EQUIP	MAINT.MON ATATA4	(0= 1)	5.09181
MAINT MON EQUIP	MAINT.MON A1A1A4	MAINT INT.P/O A1A1A4(Q= 3)	6.59881
MAINT MON EQUIP	MAINT.MON A1A1A4	MAIN.MO.INATATATATAT	8.39999
MAINT MON EQUIP	MAINT.MON A1A1A4	AN.COM.#3 A1A1A4A11 (Q= 1)	2.34427
MAINT MON EQUIP	MAINT.MON A1A1A4 Maint.mon a1a1a4	AN.COM.#2 A1A1A4A13 (Q= 1) AU/AD/PAR A1A1A4A24 (Q= 1)	2.28655 1.61664
MAINT MON EQUIP	MON PS ASYATATAS	(Q= 1)	0.50000
MAINT MON EQUIP	PS ASSY A1A1A6	(9= 1)	0.40000
MAINT MON EQUIP	DIR CPLR A1A1DC1	(Q= 1)	0.01000
MAINT MON EQUIP	DETECTOR ATATERT	(9= 1)	1.19941
MAINT MON EGUIP	VIDEO AMP ATATART	(0= 1)	0.17742
OVERALL FAILURE RAT	TES FOR THIS EQUIPMENT	:	181.21548
OVERALL MIBF FOR TH	IIS EQUIPMENT		5518.29395

FIGURE C.6. BASIC NARROW AZ MONITOR RELIABILITY PREDICTIONS

ASSEMPLY	SUBASSEMBLY	POARD	(F.R.1)
ACTIVE FRUIP	TUT AMP ATATAT	CHASSIS (Q= 1)	4.03096
ACTIVE EQUIP	THE ARE THE	PCB (Q= 1)	4.26836
ACTIVE EQUIP	TUT AMP A1A1A1	H/V BOX (Q≈ 1)	1.59270
ACTIVE EQUIP	THT AMP ATATAT	RF COMPONENTS (Q= 1)	50.02470
ACTIVE EQUIP	RF ASSY ATATAZ	· (Q= 1)	1.84141
ACTIVE ECUIP	RF ASSY ATATAZ	EXCITER ATATAZAT (9= 1)	11.64571
ACTIVE EQUIP	RF ASSY ATATAZ	DPSK ASSY A1A1AZAZ (Q= 1)	2.67856
ACTIVE FOULP	RF ASSY ATATAZ	AMP MOD ATATAZAS (Q= 1)	9.02338
ACTIVE EQUIF	RF ASSY ATATAZ	ISOLATOR P/O A1A1A2(G= 1)	0.76745
ACTIVE EQUIP	RF ASSY A1A1A2	ATTEN, VAR P/O A1A1A?(Q= 1)	0.85252
ACTIVE EQUIP	LC/STATUS A1A1A3	(Q= 1)	1.43000
ACTIVE EQUIP	LC/STATUS A1A1A3	SYST SYNC A1A1A3A3 (Q# 1)	1.58504
ACTIVE EQUIP	LC/STATUS A1A1A3	DATA LINK A1A1A3A4 (Q≈ 1)	1.83593
ACTIVE EGUIP	LC/STATUS ATATAS	ID/BD/DPS A1A1A3A16 (9≈ 1)	1.65630
ACTIVE EQUIP	LC/STATUS A1A1A3	SYS TIM GEATATABATT (Q= 1)	2.12854
ACTIVE EQUIP	LC/STATUS A1A1A3	TIM CNTRL A1A1A3A18 (Q= 1)	7.35032
ACTIVE EUUIP	LC/STATUS A1A1A3	10 MHZ DR A1A1A3A19 (Q≈ 1)	0.05236
ACTIVE FQUIP	LC/STATUS A1A1A3	10 MHZ OSCA1A1A3Y1 (Q= 1)	3.39331
ACTIVE EQUIP	PS ASSY A1A1A6	(0* 1)	1.60052
ACTIVE EQUIP	PS ASSY ATATA6	20v p.suppata1A6PS1 (Q# 1)	0.75369
ACTIVE EQUIP	PS ASSY A1A1A6	15V P.SUPPA1A1A6PSZ (Q= 1)	1.29561
ACTIVE EQUIP	PS ASSY ATATA6	SV P.SUPP A1A1A6PS3 (Q= 1)	0.60455
ACTIVE EQUIP	COOL FAN A1A131	(Q= 1)	6.00519
ACTIVE EQUIP	ANTENNA	SCAN SWIT AZS1-4 (Q= 4)	9.52579
ACTIVE FOUIP	ANTENNA	SEAN MOD. AZAZ (Q= 1)	8.84140
ACTIVE EQUIP	ANTENNA	ANT SEL SWA2S5 (Q= 1)	1.05603
ACTIVE EQUIP	PWR.DIST ATM1	(Q= 1)	6.68013
ACTIVE FOUIP	SIG J BOX A1N2	LPB N01 (Q= 1)	1.85694
ACTIVE ERUIF	SIG J BOX A1N2	LPB N01 (Q= 1)	2.99655
ACTIVE EQUIP	SIG J BOX ATNZ	LP8 NO2 (Q= 1)	1.42505
ACTIVE EQUIP	SIG J BOX ATMZ	£PB N04 (Q≈ 1)	4.33284
ACTIVE EQUIP	SIG J BOX A1M2	LFB N01 (Q= 1)	0.61897
ACTIVE FUUIP	BM STEER. AZA1	(Q= 1)	6.82475
ACTIVE EQUIP	BM STEER. AZA1	SCAM CNTR AZA1A1 49× 1)	2.51020
ACTIVE EQUIP	BM STEER. AZA1	SC.CN.COMPAPATAZ (R= 1)	1.94641
ACTIVE EQUIP	BM STEER. AZA1	10 MHZ OSCAZATY1 (Q= 1)	2.64071
ACTIVE EQUIP	ANT.PS.ASYAZA4	(Q≈ 1)	0.08207
ACTIVE EQUIP	ANT.PS.ASYAZA4	5V P.SUPP AZA4PS1 (Q= 1)	0.60696
ACTIVE EQUIP	ANT.PS.ASYAZA4	24V P.SUPPAZA4PSZ (Q= 1)	0.62664
ACTIVE EQUIP	ANT.PS.ASYAZA4	40V P.SUPPAZA4PS3 (9= 1)	0.72043
ACTIVE EGUIP	L.P.ASSY AZAS	LPB NO1 AZA5A1 (Q= 1.)	3.09486
ACTIVE EQUIP	L.P.ASSY AZAS	LPB NOZ AZASAZ (Q= 1)	1.31941
ACTIVE EQUIP	L.P.ASSY AZAS	LP8 NO5 A?A5A3 (9≈ 1)	5.26907
OVERALL FAILURE	RATES FOR THIS EQUIPMENT		179.39212
OVERALL MIPF FOR	THIS EQUIPMENT		5574.38184

FIGURE C.7. BASIC NARROW EL ACTIVE RELIABILITY PREDICTIONS

ASSEMBLY	SUBASSEMBLY	BOARD	(F.R.1)
EXEC MON EQUIP	RF ASSY A1A1A2	DET AMP A1A1A2AR1 (Q= 1)	0.25219
EXEC MON EQUIP	LC/STATUS A1A1A3	SEQ/TIMER A1A1A3A2 (Q= 1)	1.83305
EXEC MON EQUIP	MAINT.MON ATATA4	EXEC INT. P/O A1A1A4(Q= 3)	6.90514
EXEC MON EQUIR	MAINT.MON A1A1A4	MON CNTRL A1A1A4A6 (Q= 1)	1.11803
EXEC MON EQUIP	MAINT.MON ATATA4	DPSK DECO ATATA4A8 (9= 1)	1.06563
EXEC MON EQUIP	MAINT.MON A1A1A4	DPSK DECI A1A1A4A9 (G= 1)	3.05165
EXEC MON EQUIP	MAINT.MON ATATA4	DISC DATA A1A1A4A10 (Q= 1)	0.97163
EXEC MON EQUIP	MAINT.MON ATATA4	RECLOCK DRATA1A4A23 (Q= 1)	0.53102
EXEC MON EQUIP	MAINT.MON A1A1A4 Maint.mon a1a1a4	1D/BD/DPS A1A1A4A25 (Q= 1) STS TIM GEA1A1A4A26 (Q= 1)	1.65630 2.34612
EXEC MON EQUIP	MAINT.MON ATATA4	MON TIM A1A1A4A28 (Q= 1)	1.82542
EXEC MON EQUIP	MAINT.MON A1A1A4	SCAN TIM A1A1A4A29 (Q= 1)	16.59309
EXEC MON EQUIP	MAINT.MON ATATA4	AN.COM.#1 A1A1A4A3D (Q= 1)	2.35163
EXEC MON EQUIP	MAINT MON ATATA4	DET/COMP A1A1A4A31 (Q= 1)	0.89428
EXEC MON EQUIP	MAINT.MON ATATA4	BE ACC CO A1A1A4A32 (Q= 1)	4.65752
EXEC MON EQUIP	MAINT.MON A1A1A4	DIG COMP. A1A1A4A33 (Q= 1)	10.43492
EXEC MON EQUIP	MAINT.HOW ATATA4	FREQ MON. A1A1A4A34 (Q= 1)	3.44774
EXEC FON EQUIP	HAINT MON ATATA4	TIMING REFATATAGA27 (Q= 1)	0.75948
EXEC MON EQUIP	MON PS ASYATATAS	(0= 1)	3.10278
EXEC MON EQUIP	MON PS ASYATATAS	C BAND LO ATATASATAT(Q= 1)	11.64572
EXEC MON EQUIP	MON PS ASYATATAS	RF MODULE A1A1A5A1A2(Q= 1)	19.97954
EXEC MON EQUIP	MON PS ASTATATAS	REG/BUFFERATATA5A1A3(Q= 1)	0.87728
EXEC MON EQUIP	MON PS ASYATATAS	MIXER A1A1A5A1Z1(G= 1)	0.90727
EXEC MON EQUIP	MON PS ASYATATAS	SV P.SUPP A1A1A5P1/2(Q= 2)	1.19760
EXEC MON EQUIP	MON PS ASYATATAS	15V P.SUP A1A1A5PS3 (0= 1)	1.29357
EXEC MON EQUIP	SIG J BOX A1N2	LPB NO2 (0= 1)	1.23940
EXEC MON EQUIP	DM STEER AZA1	SC.CH.MON.AZA1A3 (Q= 1)	2.66057
EXEC MON EQUIP	BM STEER AZAT	SS MONITORAZATA4 (Q= 1)	2.81032
EXEC MON EQUIP	ANT MO AMPAZAR	(Q= 1)	0.17314
EXEC MON EQUIP	DETECTOR A2CR1-2	(Q= 2)	2.39882
EXEC MON EQUIP	MON ANT A3	PWR DIST A3N1 (Q= 1)	0.26955
EXEC MON EQUIP	MON ANT A3	LPB NO 3 (Q= 1)	0.91843
EXEC MON EQUIP	MON ANT A3	VIDEO AMP A3N2AR1 (Q= 1)	0.23044
EXEC MON EQUIP	MON ANT A3	RF DET A3N2CR1 (Q= 1)	1.10134
EXEC MON EQUIP	HON ANT A3	BAND FILT A3N2FL1 (Q= 1)	0.62870
EXEC MON EQUIP	MON ANT A3	PWR DIV A3N2Z1 (9= 1)	0.94305
MAINT MON EQUIP	THT AMP A1A1A1	CHASSIS (0= 1)	1.00000
MAINT MON EQUIP	RF ASSY A1A1A2	TERMIN P/O A1A1A2(9= 3)	2.55757
MAINT MON EQUIP	RF ASSY A1A1A2	DETECTOR P/O A1A1A2(Q= 2)	2.61000
MAINT MON EQUIP	LC/STATUS A1A1A3	(Q= 1) LT DR/ALM A1A1A3A1 (G= 1)	15.08483
MAINT MON EQUIP MAINT MON EQUIP	LC/STATUS A1A1A3 LC/STATUS A1A1A3	LT DR/ALM ATATASAT (G= 1) LC/ST.1ND.ATATASA20 (G= 1)	1.86031 1.99999
MAINT MON EQUIP	MAINT.MUN ATATA4	(9= 1)	1.45489
MAINT MON EQUIP	MAINT.SON ATATA4	MAINT INT.P/O A1A1A4(Q= 3)	6.59881
MAINT MON EQUIP	MAINT.MON ATATA4	MAIN. NO. INATATA4A35 (Q= 1)	7.80000
MAINT MON EQUIP	MAINT.MON ATATA4	AN.COM.#3 ATATA4ATT (R= 1)	2.36420
MAINT FON EQUIP	MAINT.MON A1A1A4	AN.COM.#2 A1A1A4A13 (0= 1)	2.28655
MAINT MON EQUIP	MON PS ASYATATAS	(0= 1)	0.50000
MAINT MON EQUIP	PS ASSY A1A1A6	(9× 1)	0.40000
MAINT MON EQUIP	DIR CPLR ATAIDCT	(0= 1)	0.01000
MAINT MON EQUIP	DETECTOR ATATOR1	(Q= 1)	1.19941
MAINT MON EQUIP	VIDEO AMP ATATART	(9= 1)	0.20009
	ES FOR THIS EQUIPMENT		160.99881
OVERALL MIBF FOR TH	IS EQUIPPENT		6211.22755

FIGURE C.8. BASIC NARROW EL MONITOR RELIABILITY PREDICTIONS

C.3.1.3.2 Small Community Configuration - The reliability prediction for the Small Community Configuration yields an MTBF of 4,350 hours for the active azimuth equipment and 4,470 hours for the active elevation equipment at 25°C. The MTBF's for the executive monitoring functions are 4,250 hours for azimuth and 5,070 hours for elevation. The maintenance monitor predictions are, azimuth - 11,300 hours, elevation - 12,620 hours. Figure C.9 thru C.12 give the reliability block diagrams for the Small Community Configuration. Figures C.13 thru C.16 show the computer summaries of the reliability prediction for this configuration. Further details of the prediction are maintained at Bendix and will be made available for customer review upon request.

The reliability prediction for the Small Community Configuration is based on a best commercial practice design. making the prediction, the lowest quality levels of failure rates given in MIL-HDBK-217B were used for commercial parts since no other commercial data is readily available. In Bendix experience, the calculation resulting from this assumption represents a bottom limit of the MTBF that can be expected since the type of equipment being designed and built for MLS is not of the type that is typically construed as commercial design, and is, therefore, not accurately represented by this prediction assumption. Factors which invalidate the prediction technique for commercial grade parts include the fact that the MLS equipment is designed to meet the full range of operational and environmental conditions specified. The MLS is not a high volume commercial production operation in which equipment is operated for only a few brief minutes, but in fact, the equipment will be fully tested to the same general criteria as the Basic Narrow. The parts used are not of the cheapest commercial grade available, but rather are high grade commercial, computer grade and, in many instances, MIL-spec parts. Additionally, Bendix has imposed its in-house "best commercial practice" specifications on vendors

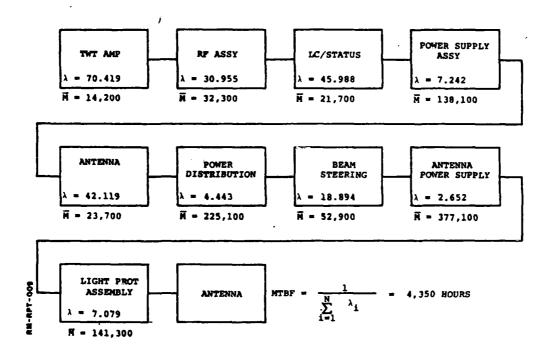
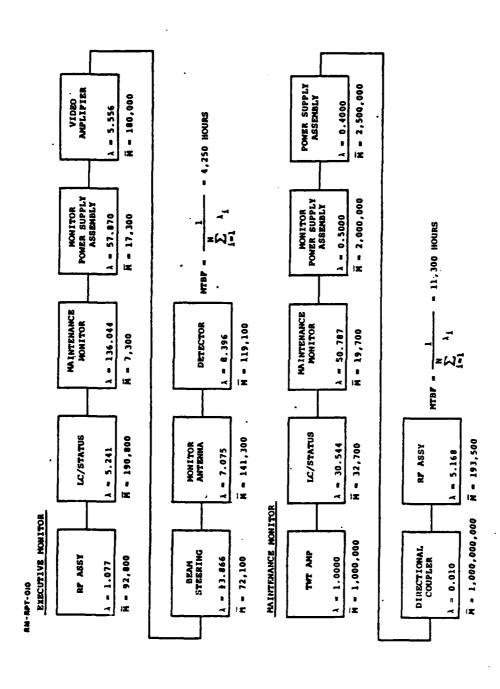


FIGURE C.9. SMALL COMMUNITY AZ ACTIVE RELIABILITY MODEL



SMALL COMMUNITY AZ MONITOR RELIABILITY MODEL FIGURE C.10.

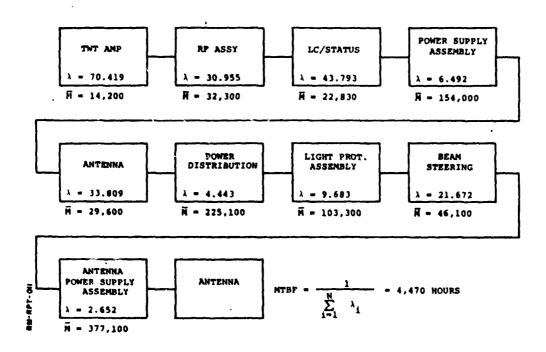


FIGURE C.11. SMALL COMMUNITY EL ACTIVE RELIABILITY MODEL

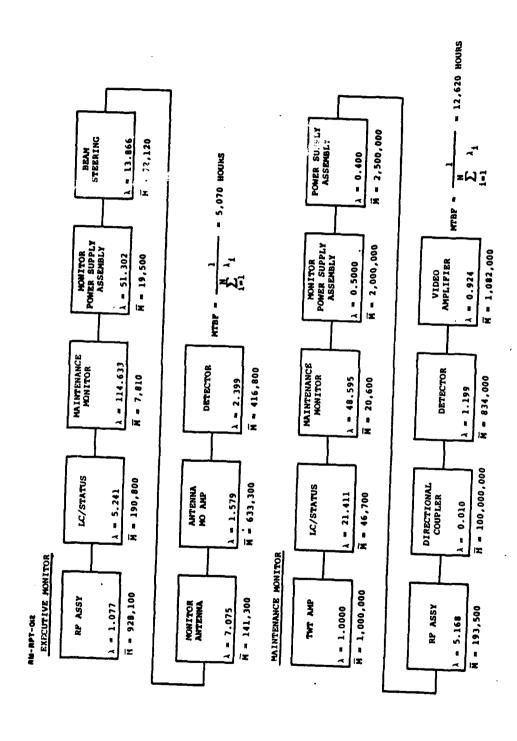


FIGURE C.12. SMALL COMMUNITY EL MONITOR RELIABILITY MODEL

And the second s

ASSEMBLY	SUBASSEMBLY	BOÁRD		(F.R.1)
ACTIVE EQUIP	TUT AMP A1A1	CHASSIS	(Q= 1)	10.02481
ACTIVE EQUIP	THT AMP A1A1	PCB	(0= 1)	8.73740
ACTIVE EQUIP	TUT AMP A1A1	H/V BOX	(0= 1)	1.63187
ACTIVE EQUIP	TUT AMP A1A1	RF COMPONE	(0= 1)	50.02470
ACTIVE EQUIP	RF ASSY A1A2		(Q= 1)	1.84141
ACTIVE EQUIP	RF ASSY A1A2	EXCITER ATAZAT	(Q= 1)	13.17267
ACTIVE EQUIP	RF ASSY A1A2	DPSK ASSY A1AZAZ Amp mod A1AZA3	(Q= 1) (Q= 1)	3.59803
ACTIVE EQUIP	RF ASSY A1A2			10.72309
ACTIVE EQUIP	RF ASSY A1A2	ISOLATOR ATAZATT ATTEN, RF ATAZATZ	(Q= 1) (Q= 1)	0.76745 0.85252
ACTIVE EQUIP	RF ASSY A1AZ	ALIENA RE RINCALZ		8.70997
ACTIVE EQUIP	LC/STATUS A1A3	SYST SYNC A1A3A3	(Q= 1) (Q= 1)	2.25647
ACTIVE EQUIP	LC/STATUS A1A3	DATA LINK ATABAS	(Q= 1)	5.80521
ACTIVE EQUIP	LC/STATUS A1A3	MORSE COD ATASATS	(Q= 1)	4.09130
ACTIVE EQUIP	LC/STATUS A1A3 LC/STATUS A1A3	ID/BD/DPS A1A3A16	(Q= 1)	4.54739
ACTIVE EQUIP	LC/STATUS ATAS	SYS TIM GEATASATT	(0= 1)	6.71834
ACTIVE EQUIP	LC/STATUS ATAS	TIM CNTRL ATASATS	(Q= 1)	10.18422
ACTIVE EQUIP	LC/STATUS ATAS	10 MHZ DR A1A3A19	(Q= 1)	0.28188
ACTIVE EQUIP	LC/STATUS ATAS	10 MHZ DK ATASKIY	(Q= 1)	3.39331
ACTIVE EQUIP	PS ASSY A1A6	IU MHZ USCATASTI	(9= 1)	2.35052
ACTIVE EQUIP		20V P.SUPPATA6PS5	(Q= 1)	1.19403
ACTIVE EQUIP	PS ASSY A1A6 PS ASSY A1A6	15V P.SUPPATA6PS2	(Q= 1)	2.49364
ACTIVE EQUIP		5V P.SUPP A1A6PS1	(Q= 1)	1.20357
ACTIVE EQUIP	PS ASSY A1A6 Antenna	SCAN SWIT ATST-4	(9= 4)	9.52579
ACTIVE EQUIP	ANTENNA	SCAN MOD. A1A8	(Q= 1)	30.15826
ACTIVE EQUIP	ANTENNA	ANT.SEL.SWA155-6	(9= 2)	2.43469
ACTIVE EQUIP	PWR.DIST A1N1	MII.3EL.3WII33-0	(Q= 1)	4.44293
ACTIVE EQUIP	BM STEER. A1A7		(Q= 1)	5.34173
ACTIVE EQUIP	BM STEER. A1A7	SCAN CNTR A1A7A1	(Q= 1)	7.29437
ACTIVE EQUIP	BM STEER. A1A7	SC.CN.COMPA1A7A2	(Q= 1)	3.61681
ACTIVE EQUIP	BM STEER. A1A7	10 MHZ OSCATATVI	(q= 1)	2.64071
ACTIVE EQUIP	ANT.PS.ASYATA6	TO HAL OSCATATO	(9= 1)	0.08207
ACTIVE EQUIP	ANT.PS.ASYA1A6	24V P.SUPPATA6PS4	(Q= 1)	1.10738
ACTIVE EQUIP	ANT.PS.ASYA1A6	40V P.SUPPATA6PS3	(Q= 1)	1.46212
ACTIVE EQUIP	L.P.ASSY A1A10	LPB NOT ATATOAT	(Q= 1)	1.79791
ACTIVE EQUIP	L.P.ASSY A1A10	LPB NOS ATATOAZ	(q= 1)	5.28136
ACTIVE EQUIP	Car cassir Araro	CIO NOS AINIGAE	(0= 1)	0.00000
MCITAL ENOTE			(4- 1)	
OVERALL FAILURE RA	ATES FOR THIS EQUIPMEN	T		229.78973
OVERALL MISF FOR	THIS EQUIPMENT			4351.80567

FIGURE C.13. SMALL COMMUNITY AZ ACTIVE RELIABILITY PREDICTIONS

ASSEMBLY	SUBASSEMBLY	BOARD		(F.R.1)
EXEC MON EQUIP EXEC MON EQUIP	RF ASSY A1A1 LC/STATUS A1A3	DET AMP A1AZAR Seg/timer A1A3A2	(Q= 1) (Q= 1)	1.07747 5.24076
EXEC MON EQUIP	MAINT.MON ATA4	EXEC INT. P/O A1A4	(Q= 5)	35.84455
EXEC MON EQUIP	MAINT.MON A1A4 Maint.mon A1A4	MON CNTRL A1A4A6 Morse Cod A1A4A7	(Q= 1) (Q= 1)	2.60450 4.55980
EXEC MON EQUIP	MAINT.MON A1A4	DPSK DECO A1A4A8	(Q= 1)	3.06096
EXEC MON EQUIP	MAINT_MON ATA4	DPSK DECI A1A4A9	(Q= 1)	5.88183
EXEC MON EQUIP	MAINT.MON A1A4	DISC DATA A1A4A10	(Q= 1)	2.11019
EXEC MON EQUIP	MAINT.MON A1A4	RECL. DR. A1A4A23	(Q= 1)	1.79492
EXEC MON EQUIP	MAINT.MON A1A4	ID/BD/DPS A1A4A25	(Q= 1)	4.54739
EXEC MON EQUIP	MAINT.MON A1A4	SYS TIM GEA1A4A26	(0= 1)	7.40043
EXEC MON EQUIP	MAINT.MON A1A4 Maint.mon A1A4	MON TIM A1A4A28 Scan tim A1A4A29	(Q= 1) (Q= 1)	5.57079 19.70799
EXEC MON EQUIP	MAINT.HON A1A4	AN.COM.#1 A1A4A30	(9= 1)	7.33790
EXEC MON EQUIP	MAINT.HON A1A4	DET/COMP A1A4A31	(Q= 1)	2.94232
EXEC MON EQUIP	MAINT.MON ATA4	BE ACC CO A1A4A32	(0= 1)	9.24046
EXEC MON EQUIP	MAINT.MON ATA4	DIG COMP. A1A4A33	(Q= 1)	12.90176
EXEC MON EQUIP	MAINT.MON A1A4	FREG MON. A1A4A34	(Q= 1)	7.87391
EXEC MON EQUIP	MAINT.MON A1A4	TIMING REFA1A4A27	(Q= 1)	2.66390
EXEC MON EQUIP	MON PS ASYATAS		(Q= 1)	6.28778
EXEC MON EQUIP	MON PS ASYATAS	C BAND LO ATASATAT	(Q= 1)	13.17267
EXEC MON EQUIP	MON PS ASYATAS	RF MODULE A1A5A1A2	(Q= 1)	27.43653
EXEC MON EQUIP	MON PS ASYA1A5 Mon PS ASYA1A5	REG/BUFFERA1A5A1A3 Mixer A1A5A1Z1	(Q= 1) (Q= 1)	1.05550 0.90727
EXEC MON EQUIP	MON PS ASYATAS	PWR DIV.	(Q= 1)	1.17393
EXEC MON EQUIP	MON PS ASYATAS	50 OHM TER	(0= 1)	2.94888
EXEC MON EQUIP	MON PS ASYATAS	5V P.SUPP A1A5PS1/2	•	2.39564
EXEC MON EQUIP	MON PS ASYATAS	15V P.SUP A1A5PS3	(q = 1)	2.49160
EXEC MON EQUIP	VIDEO AMP ATAR		(Q= 7)	5.35569
EXEC MON EQUIP	DETECTOR A1CR		(Q= 7)	8.39589
EXEC MON EQUIP	BM STEER ATA7 .	SC.CN.MON.A1A7A3	(Q= 1)	7.63475
EXEC MON EQUIP	BM STEER A1A7	SS MONITORATA7A4	(9= 1)	6.23126
EXEC MON EQUIP	MON ANT A2 Mon ant a2	BOX ASSY A2N1 Light protazn2a1	(Q= 1) (Q= 1)	2.48955 0.91843
EXEC MON EQUIP	MON ANT AZ	VIDEO AMP AZNZARIA1	(Q= 1)	0.91843
EXEC MON EQUIP	MON ANT AZ	RF DET AZNZCR1	(0= 1)	1.10134
EXEC MON EQUIP	MON ANT AZ	BAND FILT AZNZFL1	(Q= 1)	0.62870
EXEC MON EQUIP	MON ANT AZ	PWR DIV AZNZZ1	(Q= 1)	0.94305
MAINT MON EQUIP	TWT AMP A1A1	CHASSIS	(Q= 1)	1.00000
MAINT MON EQUIP	RF ASSY A1A2	TERMIN. A1A2A3-5	(Q= 3)	2.55757
MAINT MON EQUIP	RF ASSY A1AZ	DETECTOR A1A2CR1/2		2.61000
MAINT MON EQUIP	LC/STATUS A1A3	1 7 AD / 11 M 44 17 14	(Q= 1) (Q= 1)	24.21739
MAINT MON EQUIP	LC/STATUS A1A3 LC/STATUS A1A3	LT DR/ALM A1A3A1 LC/ST.IND.A1A3A20	(9= 1)	4.32637 1.99999
MAINT MON EQUIP	MAINT.MON A1A4	CC/31.1AD.RIAJREO	(0= 1)	7.85681
MAINT MON EQUIP	MAINT.MON A1A4	MAINT INT.P/O A1A4	(q= 3)	19.33687
MAINT HON EQUIP	HAINT.FON A1A4	MAIN.MO.INA1A4A35	(9= 1)	8.39999
MAINT MON EQUIP	MAINT.MON A1A4	AN. COM. #3 A1A4A11	(Q= 1)	7.59948
MAINT MON EQUIP	MAINT.MON A1A4	AN.COM.#2 A1A4A13	(0= 1)	7.59394
MAINT MON EQUIP	MON PS ASYATAS		(Q= 1)	0.50000
MAINT MON EQUIP	PS ASSY A1A6		(Q= 1)	0.40000
MAINT MON EQUIP	DIR CPLR A18C1		(Q= 1)	0.01000
OVERALL FAILURE RAT	ES FOR THIS EQUIPMENT			323.53180
OVERALL MIBF FOR TH	IS EQUIPMENT			3090.88721

FIGURE C.14. SMALL COMMUNITY AZ MONITOR RELIABILITY PREDICTIONS

ASSEMBLY	SUBASSEMBLY	BOARD		(f.R.1)
ACTIVE EQUIP	THT AMP A1A1	CHASSIS	(Q= 1)	10.02481
ACTIVE EQUIP	TWT AMP A1A1	PCB	(Q= 1)	8.73740
ACTIVE EQUIP	TWT AMP ATAT	H/V BOX	(9= 1)	1.63187
ACTIVE EQUIP .	TWT AMP ASAS	RF COMPONE	(9= 1)	50.02470
ACTIVE EQUIP	RF ASSY A1AZ		(Q= 1)	1.84141
ACTIVE EQUIP	RF ASSY A1AZ	EXCITER ATAZAT	(Q= 1)	13.17267
ACTIVE EQUIP	RF ASSY A1A2	DPSK ASSY A1AZAZ .	(Q= 1)	3.59803
ACTIVE EQUIP	RF ASSY A1A2	AMP MOD ATAZAS	(0= 1)	10.72309
ACTIVE EQUIP	RF ASSY A1A2	ISOLATOR ATAZATT	(Q= 1)	0.76745
ACTIVE EQUIP	RF ASSY A1A2	ATTEN, RF A1A2AT2	(0= 1)	0.85252
ACTIVE EQUIP	LC/STATUS A1A3		(Q= 1)	6.61000
ACTIVE EQUIP	LC/STATUS A1A3	SYST SYNC A1A3A3	(Q= 1)	5.13866
ACTIVE EQUIP	LC/STATUS A1A3	BATA LINK A1A3A4	(B= 1)	5.80521
ACTIVE EQUIP	LC/STATUS A1A3	ID/BD/DPS A1A3A16	(0= 1)	4.54739
ACTIVE EQUIP	LC/STATUS A1A3	SYS TIM GEA1A3A17	(9= 1)	6.61203
ACTIVE EQUIP	LC/STATUS A1A3	TIM CHTRL A1A3A18	(0= 1)	11-40408
ACTIVE EQUIP	LC/STATUS ATA3	10 MHZ DR A1A3A19	(Q= 1)	0.28188
ACTIVE EQUIP	LC/STATUS A1A3	10 MHZ OSCA1A3Y1	(Q= 1)	3.39331
ACTIVE EQUIP	PS ASSY A1A6		(Q=1)	1.60052
ACTIVE EQUIP	PS ASSY ATA6	20v P.SUPPA1A6PS5	(Q= 1)	1.19403
ACTIVE EQUIP	PS ASSY A1A6	15V P.SUPPA1A6PS2	(Q= 1)	2.49364
ACTIVE EQUIP	PS ASSY A1A6	5V P.SUPP A1A6PS1	(Q=1)	1.20357
ACTIVE EQUIP	ANTENNA	SCAN SWIT A151-54	(0= 1)	2.38144
ACTIVE EQUIP	ANTENNA	SCAN MOD. A1A8	(Q=1)	30.15826
ACTIVE EQUIP	ANTENNA	ANT SEL SWA1S5	(Q= 1)	1.26945
ACTIVE EQUIP	PWR.DIST A1N1		(0= 1)	4.44293
ACTIVE EQUIP	BM STEER. ATA?		(Q=1)	8.11975
ACTIVE EQUIP	BM STEER. A1A7	SCAN CNTP A1A7A1	(Q= 1)	7.29437
ACTIVE EQUIP	BM STEER. A1A7	SC.CN.COMPA1A7AZ	(0=1)	3.61681
ACTIVE EQUIP	BM STEER. A1A7	10 MHZ OSCATA7Y1	(q=1)	2.64071
ACTIVE EQUIP	ANT.PS.ASYA1A6		(e= 1)	0.08207
ACTIVE EQUIP	ANT.PS.ASYA1A6	24V P.SUPPA1A6PS4	(e= 1)	1.10738
ACTIVE EQUIP	ANT.PS.ASYA1A6	40V P.SUPPA1A6PS3	(Q= 1)	1.46212
ACTIVE EQUIP	L.P.ASSY A1A10	LPB NOT ATATOAT	(9=1)	3.09486
ACTIVE EQUIP	L.P.ASSY A1A10	LPB NOZ ATATOAZ	(Q= 1)	1.31941
ACTIVE EQUIP	L.P.ASSY ATATO	LPB NOS ATATOAS	(Q= 1)	5.26907
OVERALL FAILURE	RATES FOR THIS EQUIPMENT			223.91665
OVERALL MTBF FOR	THIS EQUIPMENT			4465.94825

FIGURE C.15. SMALL COMMUNITY AZ ACTIVE RELIABILITY PREDICTIONS

ASSEMBLY	SUBASSEMBLY	BOARD		(F.R.1)
EXEC MON EQUIP	RF ASSY ATAZ	DET AMP ATAZART	(Q= 1)	1.07747
EXEC MON EQUIP	LC/STATUS A1A3	SEG/TIMER A1A3A2	(Q= 1)	5.24076
EXEC MON EQUIP	MAINT.MON A1A4 Maint.mon A1A4	EXEC INT. P/O A1A4 MON CNTRL A1A4A6	(Q= 3) (Q= 1)	21.50672 2.60450
EXEC MON EQUIP	MAINT.BON A1A4	DPSK DECO A1A4A8	(9= 1)	3.06096
EXEC MON EQUIP	MAINT.MON A1A4	DPSK DECI A1A4A9	(q= 1)	5.88183
EXEC MON EQUIP	MAINT.MON A1A4	DISC DATA ATAGATO	(0= 1)	2.11019
EXEC MON EQUIP	MAINT.MON ATA4	RECL DR A1A4A23	(Q= 1)	1.79492
EXEC MON EQUIP	MAINT.MON A1A4	ID/BD/DPS A1A4A25	(9= 1)	4.54739
EXEC MON EQUIP	MAINT.MON A1A4	SYS TIM GEATA4A26	(Q= 1)	7.40043
EXEC MON EQUIP	MAINT_MON A1A4	MON TIM A1A4A28	(Q= 1)	5.57079
EXEC MON EQUIP	MAINT.MON A1A4	SCAN TIN A1A4A29	(Q= 1)	19.70799
EXEC MON EQUIP	MAINT.MON A1A4	AN.COM.#1 A1A4A30	(0= 1)	7.33790
EXEC MON EQUIP	MAINT.MON A1A4	DET/COMP ATA4A31	(Q= 1)	2.94232
EXEC MON EQUIP	MAINT.MON A1A4	BE ACC CO A1A4A32	(Q= 1)	6.88211
EXEC MON EQUIP	MAINT. MON A1A4	DIG COMP. A1A4A33	(Q= 1)	12.90176
EXEC MON EQUIP	MAINT.MON A1A4	FREG MON. A1A4A34	(Q= 1)	7.87391
EXEC MON EQUIP	MAINT.HON A1A4 Mon PS ASYATAS	TIMING REFATA4A27	(Q= 1) (Q= 1)	2.50953 3.84278
EXEC MON EQUIP	MON PS ASYATAS	C BAND LO ATASATAT	(Q= 1)	13.17267
EXEC MON EQUIP	MON PS ASYATAS	RF MODULE ATASATA2	(0= 1)	27.43653
EXEC MON EQUIP	MON PS ASYATAS	REG/BUFFERATASA1A3	(9= 1)	1.05550
EXEC MON EQUIP	MON PS ASYATAS	MIXER ATASATZT	(Q= 1)	0.90727
EXEC MON EQUIP	MON PS ASYATAS	SV P.SUPP ATASPST	(q= 2)	2.39564
EXEC MON EQUIP	MON PS ASYATAS	15V P.SUP ATASPS3	(0= 1)	2.49160
EXEC MON EQUIP	BM STEER ATAT	SC.CN.MON.A1A7A3	(Q= 1)	7.63475
EXEC MON EQUIP	BM STEER A1A7	SS MONITORATA7A4	(Q= 1)	6.23126
EXEC MON EQUIP	ANT MO AMPA1E1AR1/2		(Q= 2)	1.57877
EXEC MON EQUIP	RF DETEC A1E1CR1/2		(0= 2)	2.39882
EXEC MON EQUIP	MON ANY AZ	BOX ASSY AZNI	(Q= 1)	2.48955
EXEC MON EQUIP	SA THA HOM	LPB NO 3 AZNZAT	(Q= 1)	0.91843
EXEC MON EQUIP	MON ANT A2	VIDEO AMP AZNZARI	(0= 1)	0.99372
EXEC MON EQUIP	MON ANT AZ	RF DET AZNZER1	(Q= 1)	1.10134
EXEC PON EQUIP	SA THA NOM	BAND FILT A2N2FL1 PWR DIV A2N2Z1	(Q= 1) (Q= 1)	0.62870 0.94305
MAINT MON EQUIP	TWT AMP ATAT	CHASSIS	(q= 1)	1.00000
MAINT MON EQUIP	RF ASSY A1A2	TERM ATAZAT3-5		2.55757
MAINT MON EQUIP	RF ASSY ATAZ	DETECTOR ATAZER1-2	-	2.61000
MAINT MON EQUIP	LC/STATUS A1A3		(Q= 1)	15.08483
MAINT MON EQUIP	LC/STATUS A1A3	LT DR/ALM A1A3A1	(Q= 1)	4.32637
MAINT MON EQUIP	LC/STATUS A1A3	LC/ST.IND.A1A3A20	(Q= 1)	1.99999
MAINT MON EQUIP	MAINT.MON A1A4		(Q= 1)	6.26489
MAINT MON EQUIP	MAINT.MON A1A4	MAINT INT.P/O A1A4	(Q= 3)	19.33687
MAINT MON EQUIP	MAINT.MON A1A4	MAIN.MO.INA1A4A35	(Q= 1)	7.80000
MAINT MON EQUIP	MAINT.MON A1A4	AN.COM.#3 A1A4A11	(0= 1)	7.59941
HAINT MON EQUIP	MAINT.MON A1A4	AN.COM.#2 A1A4A13	(0= 1)	7.59394
MAINT MON EQUIP	MON PS ASYATAS		(Q= 1)	0.50000
MAINT MON EQUIP	PS ASSY A1A6 DIR CPLR A1DC1		(Q= 1) (Q= 1)	0.40000
MAINT MON EQUIP	RF DETECTOATCR3		(u= 1) (u= 1)	1.19941
MAINT MON EQUIP	VIDEO AMP ATATART		(0= 1)	0.92415
OVERALL FAILURE RATE			,,	276.37878
OVERALL MIBF FOR THI	2 FAMILWENT			3618.22363

FIGURE C.16. SMALL COMMUNITY AZ MONITOR RELIABILITY PREDICTIONS

supplying hardware. In view of these factors, and based on Bendix experience on other contracts for "best commercial practice" equipment, it is fully expected that the MTBF's that will be achieved in the field will lie closer to the MTBF of a full FAA-2100 design than it will to the bottom limit predicted.

C.3.2 MAINTAINABILITY

The results of the maintainability predictions yield an MTTR of 0.42 hours for the Basic Narrow Configuration and 0.41 hours for the Small Community Configuration.

MIL-HDBK-472, procedure III was used to make the predictions.

Figure C.17 gives a functional level diagram for the ground subsystem and indicates the levels of localization to the LRU by means of built-in front panel and internal indicators. From this functional level diagram, seven general categories of maintenance action were identified. The checklist scoring technique of procedure III was applied to these seven types of actions and a corrective maintenance time determined for each. These individual maintenance times were then weighted by the probability of occurrence (ratio of individual item failure rate to the total system failure rate) to arrive at the overall MTTR

The checklist scores and details of the maintainability calculations by individual item are given in Supplement A.

C.3.3 FAILURE MODES AND EFFECTS ANALYSIS

A Failure Modes and Effects Analysis was performed to determine the effectiveness of the monitor equipment to detect all failures and to identify the effect of hardware failures on system performance.

C.3.3.1 Analysis Method

A series of matrices were developed which define the effect of hardware failures on the functional operation of the

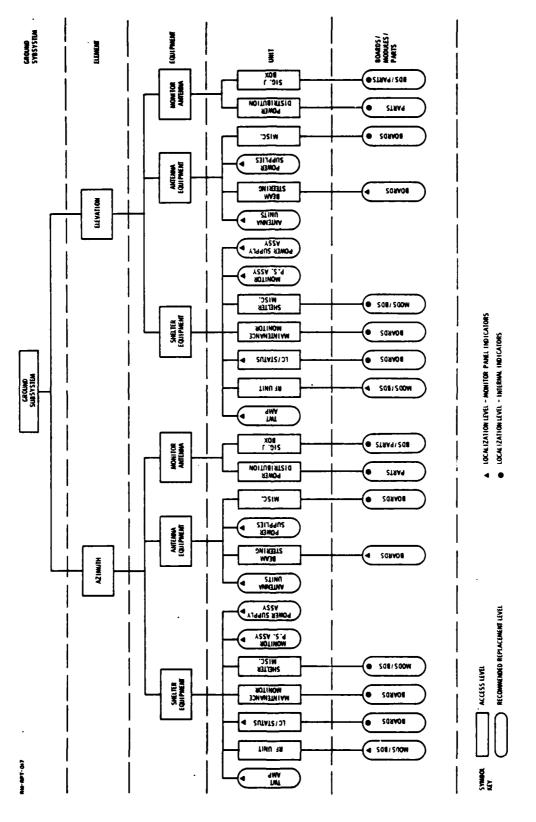


FIGURE C.17. MAINTAINABILITY FUNCTIONAL LEVEL DIAGRAM

وقائلتك فلتكم الكائمة وتتكافئ والمستفاول والمدعومون سيال فالتراكي وماء والاستفادات

system, and also define the monitor function which detects the failure and downgrades the system.

The analysis was performed starting at the board functional interface level, establishing the functional relationships between circuit boards. These relationships were then traced until the ultimate effect on the system output was established. The system output effects were categorized into four aspects of the radiated signal:

- a. Carrier Frequency
- b. Carrier Phase Timing
- c. Power ON/OFF and Antenna Selection Timing
- d. Carrier Amplitude versus Steering Position

The above analysis was then used as the criteria for determining criticality of hardware items in evaluating the executive monitor's ability to detect all failures, and perform the executive downgrading function.

C.3.3.2 Analysis Results

Figure C.18 is the composite matrix which shows the cause/ effect relationships of the various hardware failures (cause) on the four critical aspects of the radiated signal (effect). The numbers in the body of the table indicate the estimated ratios of the particular hardware items which will cause the indicated effect on the system output signal.

An additional matrix is shown in Figure C.19. This matrix illustrates the maintenance monitor panel indications (effect) upon the occurrence of particular hardware failures (cause), and is intended as a maintenance aid in troubleshooting the hardware. The numbers in the body of the table are approximate ratio of the hardware failures for a particular equipment which will result in the indicated symptom.

STG FAIL. (TIMING) O MNZ FAIL. (TIMING) MORSE CODE GEN. (TIMING) MATA LINK FAILURE (L.C.) PE MSEC DRIV. FAIL E.C.)	•	0.6		POSITION
NORSE CODE GEN. (TIMING) DATA LINK FAILURE (L.C.)) •	1	0.6	0.8
DATA LINK FAILURE (L. C.)		L.O	1.0	1.0
	•	L.O	1.0	1.0
42 MSEC DOLV. FALL II C. 1	0	1.0	1.0	1.0
		1.0	1.6	1.0
SECYTIMER FAIL (L.C.)	1 •	L0	1.0	1.0
IGHT DRIVER (L.C.)	0	0	0	0
O MHZ OSC. FAIL (B.S.)	0	0	0	1.0
SCAN CONTROL LOGIC (8. S.)	•	0	0	1.0
CAN CONTROL MONL COMP. (B. S.)	0	0	0	0
SCAN CONTROL MONL (B, S,)	0	0	0	0
CAN SWITCH DRIVER (8.5.)	0	•	0	0.3
NT. SCAN SWITCH DRIVER (B.S.)	0	0	0	0.3
SCAN SWITCH MON. 18.S.)	0	0	0	0
D/BASIC DATA/DPSK GEN, (TIMING)	0	0.8	€6	0
IMING CONTROL (TIMING)	0	0.9	0.9	0
IUX. DATA - 5 CARDS (TIMING)	0	۵,9	0.1	0
DICITER FAILURE (XMTR-EXC.)	1.0	0	1.0	0
MODULATOR CONTR-EXC.)	•	1.0	1.0	0
PSK DRIVER (XMFR-EXC.)	0	1.0	0	0
SOL (XMTR-EXC.)	0	[0	1.0	0
MP MOD OUNTR-EXC.)	0	0	1.0	0
/AR. ATTEN (XMTR-EXC.)	0	0	1.0	0
WTA	•	0	1.0	0
AONITOR ROVE AND PEAK DETECTOR (THI MONITOR)		0	0	0
D/BASIC DATA/DPSK GENERATOR (TM MONITOR)	0	0	0	0
SYSTEM TIMING GENERATOR (TM MONITOR)) 0) 0	0	0
AORSE CODE GENERATOR (TM MONITOR)	0	0	. 0	0
IUX/ID/ADD/PARITY GENERATOR (THI MONITOR)	0		0	0
AONITOR DECODE (THI MONITOR)	0	0	0	0
IONITOR DECISION (TM MONITOR)		8	0	0
AONITOR CONTROL (ROLLO)	0	0	0	0
AONITOR TIMING SD IROLLOI	0	0	0	0
SCAN TIMING BD (ROLLO)	0	0	0	0
DIEC. INT. BO IROLLOS	1 0	1 0	0	0
MAINT, INT. 80 (ROLLO)		0	0	0
ANAL. COMP. 80 IROLLOS	0	0	0	0
DIGITAL COMP. BO (ROLLO)	0	0	0	0
DISC. : ATA 80 (ROLLO)	1 0	0	0	0
FAR FY_LD ANTENNA (RF MONL)		0	0	0
OMMIN DET IRF MONL)	0	0	0	0
PSLS DET (RF MONL)			0	0
SLS DET (RF MONL)	•	0	0	0
TEST PULSE LOGIC (RF MONL)	•	0	0	0
ANGLE LOGIC (RF MONL)	0	0	ò	0
SCAN SWITCH (ANT.)			o	1.0
SCAN MOD. (ANT.)	0	0	0	1.0
ENS FAILURE	0	١	1.0	1.0
DMMI ANT, FAIL (ANT,)		1.0	1.0	0
	1	0	0	1,0
ISLS ANT. FAIL (ANT.)	1	,	i	1.0
ISLS ANT. FAIL (ANT.) .SLS ANT. FAIL (ANT.)	1 0			

FIGURE C.18. BASIC NARROW FAILURE MATRIX

			-7	7	7	7	7	7	7	7	7	7	_	-7	7	7	7	7	7	7	7	7	7	-	-,	7	77
			Ι.	/.	/	Ι.	Ι.	/	/	Ι.	Ι.	Ι.	/	Ι.	Ι.	/.,	/,	/ ,	Ζ,	Ι.	/	Ι.	200	/	Ι.		/ , / , ,
		//	./.			a /	Ι.			\mathcal{J}	/.	\mathcal{I}		ړ/ خ	./.		<u>``</u>		}/s	\mathcal{I}		8/8	* /		/\$	*/	
	,		/\$	Ζ.		/ŝ	الخوا	Ζ,		/\$	2	1	/8			/3	Ζ,) \$ /	/ § 3	/3	3				
	/3	*/*			? /:				!	3/		3/		8		a /		5/3			•//		.]			* /.	• /
	/ *	<u> </u>	<u> </u>	<u> Z</u>	<u> </u>	<u> </u>	<u> </u>	۷,	<u> </u>	\angle	Ζ,	/3	<u>/</u>	\mathbb{Z}^{9}	<u> </u>	\$ 2	<u> </u>	<u> </u>	/₹	۷.	/*	Ζ.	~	<u> </u>	Ζ.	<u>/:</u>	7
STG (TIMERE)	4.	4.	4.1	٠.	4.	41	4.		6.0	0.4	4.1	۰		4.5		0.8	4.0	۰			0.6	0	٠	۵.	8.0	4.0	Į
(Canada Canada)	9	10	1.0	1.0	1.0	1.0	1.0	•	1.0	1.0	1.0	۰	1.0	1.0	1.0	1.0	1.0	•	0	10	1.0	0		1.0	1.0	10	j
MORSE CODE GEN (THRING)	1:1	•	۰	٠			1.0	•	۰	:	0		:			١		•		1.9	10	0	0	٥	10	10	i
DATA LINE U. C.) SEE MS DELV. G. C.:	١.١	ů		,	ľ	,				,					٠	١		٠			ľ	,		10		1.0	
SEQ/TIMER N. C)	;		٥	,			j			·		۰		6.2						01	a.	,	٠	۵,	4.5	4.1	
LIGHT DRIV. IL.C.	0	,	0		۰			•		0		0		٥					0			0	۰	0		0	
10 1042 OSC 18.5 1	10	,	1.0	0	0	0	0	٠	1.0	1.0	10	0	٥	0	0	٥	0	0	٥	3	٥	0	۰	٥	: 0	٥]
SCAN CHIRL LOGIC (8 S.)	10	٥	: 0	0	0	•	٥	۰	1.0	LO.	1.0	٥	٥	0	0	3	0	۰	۰	0	۰	0	٥	٥	1.0	3	
SCAN CHIRL MON COMP ID 5 -	٥	0	۰	٥	۰			۰	1.0	1.0	1.0	١٠	۰	[•	•	۰	٥	٥	٥	٥	٥	(0	3	0	1.3	1	l
SCAN CHITIC MOR (8.5.)	l.º	0	•	3	<u> </u>	•	ů		10	1.0	1.0	٥	°	0	0	0	•	°	0	0	l °	0	0		1.0	0	1
SCAN SIR DRIV (BLS.)	10	١٥١	1.0) 0	٩		٥	0	1.0	0	10	0	0	٥	٥	٥	٥	۱	8	ů	0	l °	0		1.0	1 0	ţ .
ENT SCAN SW. DRIV (B.S.) SCAN SW. MON (B.S.) (3 CARDS)		0	1.0	,			,		1.0			,	۰	,				٠	0			,	i	0	1.0	,	1
ID BASIC DATA DPSK GEN (TIMING)		,					0.1	Ĭ		0		٥			2.5	0.2			۵		a.s	0	0		4.6	3 8	1
TIMENG CHINE ITMENGS	2.0	4.0	0.1	0.8	4.8	2.1	4.5	0	1.0	1.0	1.0	0	6	0	43	2.3	0.5	۰	0	٥	4.0		٥	ı	3 5	0.0	l
AUX DATA -TIMING	1 • 1		٥	•		٠			٥	6	٥	٥		0	2	10	•	0	۰	٥	0	0		٥	٥	1.0	į
EXCITER IEXC-MODI			10	1.0	10	10	L.O	1.0	10	1.0	0	٥	٥	0	1.0	1.0	1.0	1.0	۰	0	0		0	0	1.0	10	i
# MODULATOR (CIC-MOD)	l • l	•	10	L0	۱۰	0	1.0	•	۱ ه ا	0	0	0	۰	(•	10	LO	10	•		0	•	0	۰	٥	1.0	10	1
DPSE DRIVER «DIC-MODI	٥	٥	1.0	1.0	۰	٩	10		٥	۰	0	0	0	8	1.0	1.0	1.0	٥	0	1.0	0		0	0	1.0	10	ł
ISOLATOR EXC MODI	•	۰	1.0	1.0	L.O	1.0	1.6	•	L.O	10	8	۰	•	l° l	1.0	1.0	1.0	0	:	۰			0	0	1.0	1.0	
AMP 400 EXC-4001		10	1.0	1.0	1.0	LO LO	1.0 1.0		1.0	1.0 1.0	0	٥		l °	10	1.0	1.0	3	0	0	1.0		٥	0	1.0	1.0]
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KFER SW. (MATR)	•		1.0	1.0	1.0	1.0	1.0	٠	10	1.0	0				1.0	1.0		0	Q.		a	اها	a	0	10	10	ļ
MONITOR REVR & PEAK DET ITIME MONE	ի եթի	1.0	۰	•		•	LO		•	0	۰	٥	۰	١.,	1.0	1.0		ا ه	0	0	٥	0	٥	0	10	1.0	
PPSK CHITEL ITHE MORL!	0	0	٥	۰	٥	٥	1.0	۰		٥	0	0	٥	0	0.5	0.2	0	٥	٥	0	٥	ه ا	0	0	1.0	Q.5	
SYST TIMING GEN. (TIM. MON.)	•	٥	0	0	١٠	(• i	1.0	٠	0	•	0	٥		0	10	10	9	٥	0	٥	٥	٥	٥	٩	1.0	10	1
WORSE CODE GEN (TIM. MON.)	l °	٥	e	٥	٥	۰	1.0	0	۰	0	١٥	0		1.0	0		٥	°	٥	٥		0	0	٥	1.0	1.0	İ
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MONITOR CHIRL MOLLO	اره ا	4.5	4.5	a.5	a,	۵,	0.5	4,5	۵,	45	0.5	۵,	0.2	4.5	43	۵,	4.5	0.5	0.5	۵,	0.5	انه	0.1	0.5	a٠	a.	ļ
MONITOR TIMING SO MOLLO	10	1.0	1.0		10	10	L.	1.0	1.0	1.6	1.0	1.0	Le	1.0	1.6	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	10	1
SCAN TIMING BO INCLIDE	1.0	1.0	1.0	1.0	10	1.0	1.0	1.0	1.0	1.0	1.0	1.0	10	10	1.0	1.0	10	1.0	10	1.0	1.0	10	1.0	10	1.0	1.0	ł
ENEC INT. BD IROLLO	01	0.1	Ø 1	a 1	Q.I	Q .1	a.ı	0.1	6 1	0.i	Q.i	6.1	0.1	Q.I	۰	0	0	۰	۰	0	٥	0	0	٥	t. a	0	1
WAIRE INF. \$5 HOLD	0	٥	٩	٩	٩	9	0		•	•	0	0	0	0	81	61	0.1	Q. 1	4.1	9.1	9.1	0.1	0.1	0.1	0	10	1
ANAL COMP. 80 HOLLO			g I	0.1	9.1	41		0	ů		٥			ا ۽ ا	:	0	3	0.1	ů	۰	0	G 1	8.1	٠	1.0	1.0	l
DIG. COMP BO MOLLON DISC. DATA BO MOLLON	3	۵,	۵	0	0	٥	91	4)	91	81	انها	4,1	81	0 1	41	4.1		:		Q.I	O Q i	١،	0	0	10	10	}
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CHANN DET 451 MONE				1.0		•													١		٥		0	0	1.0		
RISLS DET & AME HE HADE	٥			0	•	10	0	0			0	•		0	• }	0	c	0	0	0	0	0	0	0	1.0	٥	}
LSLS DET & ANT INF MON	ا • ا	•	•	٠	l.0	•	۰	0	•		۰	۰	•	•	•	١٠	0	۰	۰	0	۰	٥	0	0	1.0	۰	
TEST PULSE LOGIC OF MORE	ا ۱	1.0	۰	٥	۰	۰	0	•	۰	٠	٥	•	•		۰	٥	٥	0	٥	0	0	0	0	۰	1.0	٥	[
WHERE FORMS THE MOST	10	0	•	•	•	•	0	٩		•		•			•		•	۰	°	0	•	0	٥		1.0		
SCAR SMITCH IAME)		10	10		۱۹۱		0	•	1.0	0	٥	٥	۰	l º	:	۰	١٠١	٥	١	٥	•	١	0	8	10	3]
SCAN MOS. HARF !	1.0	1.0	1.0	0	١	•	0	•	1.0	1.6 0	ů			1:					å	0		0	0	0	1.0	٥	1
TERS OWN				1,0	١.,		1.0	١		٠				8	1.6	1.0	١	١	ï	٠		١	0		1.0	10	
AUR DATA INPUT			٠			١	8			٠	٥		٠	;		1.0		ا				١	0	0		10	l

FIGURE C.19. MONITOR EFFECT MATRIX

C.3.3.3 Analysis Conclusions

The overall conclusion of the analysis is that the monitor hardware is adequate for detecting the vast majority of system failures. During the analysis one undetectable failure was defined. This is a scan switch failure, whereby a failure of a port to close will not be detected. The effect of this failure is transmission of erroneous angle data. The discovery of this undetected failure mode will precipitate an investigation during the next contract phase.

C.3.4 HUMAN FACTORS AND SAFETY EVALUATION

A human factors and safety evaluation was performed on the MLS ground equipment to verify adherence to the design criteria in MIL-STD-1472A and the safety and grounding requirements of FAA-G-21001/b and amendment B. A checklist procedure had previously been established for performing the evaluation; a copy of the procedure is contained in Supplement B of this document.

The checklist sheets in Supplement B show the results of the evaluation. Both the Basic Narrow and the Small Community Configurations were considered in the evaluation. The checklist sheets are applicable to both systems with the exception of the Facility-Shelter-Work Station Checklist for the electronic shelter. The latter is applicable only to the Basic Narrow Configuration.

C.3.4.1 Human Factor/Safety Analysis Results

The results of the analysis indicate a system and equipment design with a close adherence to the program Human Factors and Safety criteria. A minimum amount of deviations were discovered, all minor in nature, which are described in the individual checklist sheets.

SUPPLEMENT A

of	Isolation Monitor Panel Isolates malfunction to the LRU
_	
	MAINTENANCE ANALYSIS
	Check monitor panel to isolate to LRU
	Open Unit - open drawer, remove rfi cover
•	Remove and replace LRU
l.	Check monitor to verify that problem is corrected
i.	Close Unit - replace rfi cover, close drawer
	•
	•
	•

CHECKLIST SCORES

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	Total
A	4	0	4	4	4	4	4	4	4	4	4	· 2	0	4	4	50
В	4	4	4	4	4	4	4									28
C	4	4	4	4	4	4	4	4	4	4						40

Predicted downtime

10 Min.

	Isolation Monitor Panel Localizes to Unit: Internal lights and/or Test points ize to board.
	MAINTENANCE ANALYSIS
1.	Check monitor panel to Localize to unit
2.	Open Unit - open drawer, remove rfi cover
3.	Localize to board group with internal lights (groups - 1 to 6 boards)
1	a) Isolate to individual board with test points, if desired
4.	Remove and replace board(s)
5.	Check monitor to verify that problem is corrected
6.	Close Unit - replace rfi cover, close drawer
1	
	•
1	

CHECKLIST SCORES

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	Total
A	4	0	4	4	4	4	2	2	2	4	4	2	0	4	4	44
В	2	4	4	4	4	4	4									26
С	4	4	4	4	2	2	2	4	4	4						34

Predicted downtime

19 Min.

Task Clas	sification3
Equipment	Group Shelter Electronics Unit/Part Chassis Parts
Method of	Isolation Monitor panel localizes to unit; test point isolates to chassis;
detaile	troubleshooting to faulty part.
	MAINTENANCE ANALYSIS
1.	Check monitor to localize to unit
2.	Open Unit - open drawer, remove rfi cover
3.	Check board test points
	a) All board test points good - begin chassis troubleshooting
	b) One or more board test points show faulty - remove and replace boards. If problem isn't corrected - begin chassis troubleshooting.
4.	Troubleshoot to find part
5.	Remove and replace part - mechanical and soldering operations
6.	Check monitor to verify that problem is rectified
7.	Close Unit - replace rfi cover, close drawer
3	

CHECKLIST SCORES

	1	2	3	4	5	6	7	8	9.	10	11	12	13	14	15	Total
A	4	0	4	0	0	0	2	2	0	0	4	4	0	4	4	28
В	1	4	4	4	4	4	4									25
С	4	4	2	4	0	2	1	3	0	2						22

Predicted downtime

70 Min.

 Check monitor to isolate to the LRU Go to antenna enclosure and remove cover (snap locks) Check power supply test point to verify failure is not in the line 	
• • •	
. Check power supply test point to verify failure is not in the line	
. Remove and replace LRU	
. Check test point to verify failure removed	
. Close cover	
. Return to shelter - check monitor to verify problem has been con	rrecte

CHECKLIST SCORES

	1	2	3	4	5	6	7	8	9.	10	11	12	13	14	15	Total
A	4	4	4	4	4	0	4	4	4	4	4	4	4	4	4	56
В	4	.4	4	4	4	4	4									28
C	2	4	4	4	4	4	4	4	4	4						38

Predicted downtime

_8 Min.

Plus 2 minutes to walk to antenna enclosure and back 10 Min.

MAINTAINABILITY PREDICTION FORM

	MAINTENANCE ANALYSIS
1.	Check monitor to localize to unit
2.	Go to antenna enclosure and remove cover (snap locks)
3.	Check local monitor and/or test points to isolate to LRU
4.	Remove and replace LRU
5.	Check test points and/or local monitor to verify failure removed
6.	Close enclosure cover
	Return to shelter - check monitor to verify problem has been corrected

CHECKLIST SCORES

	1	2	3	4	5	6	7	3	9.	10	11	12	13	14	15	Total
A	4	4	4	4	4	2	2	2	2	4	4	2	0	4_	4	46
В	2	4	4	4	4	4	4									26
C	2	4	4	4	2	2	2	4	4	4						32

Predicted downtime

18 Min.

Plus 2 minutes to walk to antenna enclosure and back 20 Min.

MAINTAINABILITY PREDICTION FORM

	Isolation Monitor panel localizes to antenna equipment; local monitoric points isolates to r.f. cables
	MAINTENANCE ANALYSIS
1.	Check monitor to localize to unit - no switches show malfunction
2.	Go to antenna enclosure and remove cover (snap locks)
3.	Check local monitor and test points to verify it's not one of the boards or switches
4.	Isolate to faulty cable
5.	Remove and replace cable
6.	Check local monitor to verify failure removed
7.	Go to shelter to verify field monitor indicates failure removed
8.	Return to antenna enclosure and close cover

CHECKLIST SCORES

	1	2	3	4	5	6	7	8	9.	10	11	12	13	14	15	Total
A	4	4	4	0	4	2	0	0	0	0	0	4	0	4	4	30
В	1	4	4	4	4	4	4									25
C	2	4	2	4	0	2	1	3	0	2						20

Predicted downtime

65 Min.

Plus 3 minutes walking between shelter and enclosure 68 Min.

MAINTAINABILITY PREDICTION FORM

Task Classification	
Equipment Group	Shelter Electronics Unit/Part Cooling Fan
Method of Isolation	Hear that fan motor is inoperating.

MAINTENANCE ANALYSIS

- Check power to motor presence of power shows motor is bad
- 2. Turn off power
- 3. Remove and replace cooling fan assembly
- 4. Restore power

CHECKLIST SCORES

\cdot	1	2	3	4	5	6	7	8	9.	10	11	12	13	14	15	Total
A	.4	0	4	2	2	2	4	2	3	0	4	4	4	0	4	39
В	2	4	4	4	4	4	4									26
C	3	4	2	3	3	4	4	4	4	4						35

Predicted downtime

24 Min.

DASIC NARROW

UNIT	FAILURE RATE (FAIL/10 ⁶ HRS)	QTY.	PERCENT OF TOTAL FR	TASK	MTTR CONTRIBUTION (MIN.)
TWT AMP	61.917	2	. 16.62	1	1.66
RF ASSY CHASSIS PARTS	3.682	-	0.49	m	0.34
EXCITER	11.646	7	3.13	7	0.59
ISOLATOR	0.767	7	0.21	m	0.15
DPSK ASSY	2.679	7	0.72	-1	0.07
VAR. ATTEN.	0.852	7	0.23	М	0.16
AMPLITUDE MODULATOR	9.023	7	2.42	1	0.24
C/STATUS CHASSIS PARTS	37.065	-	4.98	м	3.49
SYSTEM SYNC AZ	0.658	г	60.0	7	0.02
SYSTEM SYNC EL	1.585	7	0.21	7	0.04
DATA LINK BOARD	1.836	7	0.49	7	60.0
DATA LINK AUX DATA	1.762	٦	0.24	7	0.05
VARIABLE AUX DATA GEN	1.707	~	0.23	7	0.04
FIXED AUX DATA #2	.2.122	~	0.29	7	90.0
FIXED AUX DATA #1	2.122	-	0.29	. 8	90.0
AUX DATA SEL/WORD VER.	1.314	Н	0.18	7	0.03
AUX ID/ADDRESS/PARITY GEN	1.616	7	0.43	7	80.0
MORSE CODE GEN.	1.365	7	0.37	7	0.07
ID/BASIC DATA/DPSK	1.656	4	0.89	7	0.17
SYSTEM TIMING GEN, AZ	2.133	7	0.57	7	0.11
SYSTEM TIMING GEN, EL	2.128	2	0.57	7	0.11
SEQUENCE TIMER	1.833	7	0.49	7	60.0

TINU	FAILURE RATE (FAIL/10 ⁶ HRS)	QTY.	PERCENT OF TOTAL FR	TASK	MTTR CONTRIBUTION
TIMING CONTROL, AZ	5.543	-	0.75	2	0.14
TIMING CONTROL, EL	7.350	-	66.0	7	0.19
LC/STATUS INDICATOR	2.000	7	0.54	м	0.38
10 MHz DRIVER	0.052	7	0.01	7	0.01
10 MHz OSCILLATOR A	3,393	7	0.91	2	0.17
LIGHT DRIVER/ALARM	1.860	8	. 05.0	7	60.0
EXECUTIVE INTEGRATOR	2.302	7	2.16	7	0.41
MONITOR CONTROL	1:118	7	0.30	7	90.0
DPSK DECODER	1.065	7	0.29	7	90.0
DPSK DECISION	.3.052	7	0.82	7	0.16
DISCRETE DATA BOARD	0.972	7	0.26	7	0.05
ANALOG COMP. #3	2.364	7	0.64	7	0.12
ANALOG COMP. #2	2.287	7	0.61	7	0.12
MAINTENANCE INTEGRATOR	2.200	9	1.77	7	0.34
MAINTENANCE MONITOR INDICATOR	7.800	7	2.09	7	0.40
RECLOCK DRIVER	0.531	7	0.14	7	0.03
MONITOR TIMING	1.825	2	0.49	7	60.0
SCAN TIMING	16.593	7	4.46	7	0,85
ANALOG COMP. #1	2.352	2	0.63	7	0.12
DETECTOR COMPARATOR	0.894	7	0.24	7	0.05
BEAM ACCURACY COUNTER AZ	5.185	-	69.0	7	0.14
BEAM ACCURACY COUNTER EL	4.657	1	0.63	7	0.13

BASIC NARROW

FIND	FAILURE	λωO	PERCENT OF		
	RATE (FAIL/10 ⁶ HRS)		TOTAL FR	TASK	MTTR CONTRIBUTION (MIN.)
DIGITAL COMPARATOR	10.435	2	2.80	2	0.53
FREQ MONITOR	3.448	2	0.93	7	0.18
TIMING REFERENCE	0.759	-	0.10	7	0.02
MAINT. MON. CHASSIS PARTS	6.537	7	0.88	m	0.62
MONITOR PWR SUPPLY CHASSIS PARTS	11.361	7	1.53	e	1.07
C-BAND L.O.	11.646	7	3.13	7	0.59
RF MODULE	19.979	8	5.36	7	1.02
regulator/bupper	0.877	7	0.24	7	0.05
MIXER	0.907	7	0.24	7	. 50.0
5 V, 10 A PWR. SUPPLY	1.198	ហ	08.0	н	80.0
15 V, 1.5 A PWR. SUPPLY	1.293	4	0.70	1	0.07
20 V, 1 A PWR. SUPPLY	0.754	7	0.20	1	0.02
5 V, 5 A PWR. SUPPLY	0.604	• m	0.24	1	0.02
PWR SUPPLY ASSY, CHASSIS PARTS	4.011	· ~	0.54	m	0.38
COOLING FAN	6.005	7	1.61		0.39
SCAN SWITCH	2.381	20	6.39	ហ	1.28
SCAN MODULATOR	8.841	7	2.37	4	0.24
ANT. SELECTOR SWITCH AZ	1.056	н	0.14	2	0.03
ANT. SELECTOR SWITCH EL	1.217	7	0.16	7	0.03
PWR DIST. BOX PARTS	13.360	ч	1.79	ю	1.25
LIGHTNING PROTECTOR BD #1 A	1.798	н	0.24	2	0.05
LIGHTNING PROTECTOR BD #1 B	1.798	2	0.48	7	60.0

TINU	FAILURE RATE (FAIL/10 ⁶ HRS)	QTY.	PERCENT OF TOTAL FR	TASK CLASS	MTTR CONTRIBUTION (MIN.)
LIGHTNING PROTECTOR BD #1 C	1.857	-	0.25	7	0.05
LIGHTNING PROTECTOR BD #1 D	2.997	7	0.80	8	0.15
LIGHTNING PROTECTOR BD #1 E	0.619	н	0.08	7	0.02
LIGHTNING PROTECTOR BD #2 A	1.239	8	0.33	7	90.0
LIGHTNING PROTECTOR BD #2 B	1.425	-г	0.19	7	0.04
LIGHTNING PROTECTOR BD #2 C	1.319	-	0.18	ហ	0.04
LIGHTNING PROTECTOR BD #4 A	4.833	ä	0.65	7	0.12
LIGHTNING PROTECTOR BD #4 B	4.333	-	0.58	7	0.11
LIGHTNING PROTECTOR BD #5 A	5.281	7	17.0	ស	0.14
LIGHTNING PROTECTOR BD #5 B	5.269	Н	0.71	S	0.14
LIGHTNING PROTECTOR BD #3	0.918	7	0.25	7	0.05
BEAM STEERING CHASSIS PARTS	10.871	-	1.46	9	66.0
SCAN CONTROL	2.510	7	0.67	2	0.13
SCAN CONTROL COMPARATOR	1.946	7	0.52	ស	0.10
SCAN SWITCH DRIVER	1.537	ч	0.21	5	0.04
SCAN SWITCH DRIVER INTERMEDIATE	2.076	-	0.28	2	90.0
10 MHz OSCILLATOR B	2.641	7	0.71	2	0.14
SCAN CONTROL MONITOR	2.661	7	0.72	S	0.14
SCAN SWITCH MONITOR	2.810.	7	0.75	S	0.15
SCAN SWITCH MONITOR EXPANDER	4.333	1	0.58	5	0.12
SCAN SWITCH MONITOR INTERMEDIATE	2.034	-	0.27	ر د	0.05
ANT. P.S. ASSY CHASSIS PARTS	0.164	7	0.02	9	0.01

BASIC NARROW

			£		
UNIT	FAILURE RATE (FAIL/10 ⁶ HRS)	QTY.	PERCENT OF TOTAL FR	TASK CLASS	MTTR CONTRIBUTION (MIN.)
24 V, 1.0 A POWER SUPPLY	0.627	2	0.17	4	0.02
40 V, 0.5 A POWER SUPPLY	0.720	7	0.19	4	0.02
AZIMUTH APERTURE ASSY PARTS	0.010	ч	0.01	9	0.01
VIDEO AMP A	0.177	9	0.14	8	0.03
VIDEO AMP B	0.230	7	90.0	S	0.01
DETECTOR	1.199	14	2.25	м	1.58
TERMINATION	0.852	9	69.0	м	0.48
DIRECTION CPLR	0.010	7	0.01	٣	0.01
BANDPASS FILTER	0.629	7	0.17	٣	0.12
PWR DIV.	0.943	8	0.25	m	0.18
MON ANT MISC PARTS	0.539	7	0.07	9	0.05
			100.00		25.25
					•
				•	

UNIT	FAILURE RATE	QTY.	PERCENT OF TOTAL FR	TASK	MTTR
	- 1				
TWT AMP	71.419	7	13.55	1	1,36
RF ASSY CHASSIS PARTS	3.682	7	0.35	м	0.25
EXCITER	13.173	7	2.50		0.48
DPSK ASSEMBLY	3.598	7	0.68	1	0.07
AMPLITUDE MODULATOR	10.723	7	2.03	ч	0.20
ISOLATOR	0.767	7	0.15	m	0.11
RF ATTENUATOR	0.852	8	0.16	М	0.11
TERMINATION	2.558	7	0.49	m	0.34
DETECTOR	1.294	1.5	1.84	m	1.29
LC/STATUS CHASSIS PARTS	54.622	н	5.18	м	3.63
SYSTEM SYNC, AZ	2.256	7	0.21	7	0.04
SYSTEM SYNC, EL	5.139	н	0.49	7	0.09
DATA LINK	5.805	7	1.10	8	0.21.
MORSE CODE GENERATOR	4.326	7	0.82	7	0.16
ID/BD/DPSK	4.547	4	1.73	7	0.33
SYSTEM TIMING GEN, AZ	7.059	7	1.34	7	0.25
SYSTEM TIMING GEN, EL	7.006	7	1.33	, N	0.25
TIMING CONTROL, AZ	10.184	-	0.97	7	0.18
TIMING CONTROL, EL	11.404	П	1.08	7	0.21
10 MHz DRIVER	0.282	2	0.05	7	0.01
10 MHz OSCILLATOR	3.393	7	0.64	7	0.12
SEQUENCE TIMER	5.241	2	66.0	8	0.19

SMALL COMMUNITY

UNIT	FAILURE RATE (FAIL/10 ⁶ HRS)	QTY.	PERCENT OF TOTAL FR	TASK	MTTR
LIGHT DRIVER/ALARM	4.326	2	0.82	2	0.16
LC/STATUS INDICATOR	2.000	7	0.38	æ	0.27
MAINTENANCE MONITOR CHASSIS PARTS	14.122		1.34	m .	0.94
EXECUTIVE INTEGRATOR	7.169	&	5.44	2	1.03
MONITOR CONTROL	2.604	7	0.49	2	0.09
DPSK DECODE	3.061	7	0.58	2	0.11
DPSK DECISION	5.882	7	1.12	2	0.21
O DPSK DATA	2.110	7	0.40	8	0.08
RECLOCK DRIVER	1.795	7	0.34	7	90.0
MONITOR TIMING	5.571	7	1.06	7	0.20
SCAN TIMING	19.708	7	3.74	7	0.71
ANALOG COMPARATOR #3	7.599	7	1.44	7	0.27
ANALOG COMPARATOR #1	7.338	7	1.39	7	0.26
ANALOG COMPARATOR #2	7,594	7	1.44	7	0.27
DETECTOR/COMPARATOR	2.942	7	0.56	7	0.11
BEAM ACCURACY COUNTER AZ	9.240	-	0.88	2	0.17
BEAM ACCURACY COUNTER EL	6.882	7	0.65	7	0.12
DIGITAL COMPARATOR	12.902	8	2.45	7	0.47
FREQUENCY MONITOR	7.874	7	1.49	2	0.28
TIMING REFERENCE	2.509	7	0.48	7	60.0
MONITOR PWR. SUPPLY CHASSIS PARTS	11.131	H	1.06	က	0.74
C-BAND LO	13.173	7	2.50	7	0.48

SMALL COMMUNITY

UNIT	FAILURE RATE (FAIL/10 ⁶ HRS)	QTY.	PERCENT OF TOTAL FR	TASK CLASS	MTTR CONTRIBUTION
RF MODULE	27.436	7	5.21	2	66.0
REGULATOR/BUFFER	1.055	2	0.20	7	0.04
MIXER	0.907	2	0.17	7	0.03
MON. PWR SUPPLY PWR DIVIDER	1.174	Н	0.11	ĸ	0.08
MON. PWR SUPPLY TERMINATION	2.949	1	0.28	m	0.20
5 V, 9 A POWER SUPPLY	1.197	4	0.45	1	0.05
+15 V, 2 A POWER SUPPLY	2.492	7	0.47	ч	0.05
5 V, 12 A POWER SUPPLY	1.204	7	0.23	ı	0.02
+15 V, 0.7 A POWER SUPPLY	2.494	8	0.47	1	0.05
40 V, 0.35 A POWER SUPPLY	1.462	7	0.28	τ	0.03
24 V, 0.7 A POWER SUPPLY	1.107	7	0.21	1	0.02
20 V, 0.9 A POWER SUPPLY	1.194	8	0.23	т	0.02
PWR SUPPLY ASSY CHASSIS PARTS	4.750	1	0.45	m	0.32
BEAM STEERING CHASSIS PARTS	13.462	-	1.28	m	06.0
SCAN CONTROL	7.294	7	1.38	7	0.26
SCAN CONTROL COMPARATOR	3.617	7	69.0	Ю.	0.13
SCAN CONTROL MONITOR	7.635	8	1.45	7	0.28
SCAN SWITCH MONITOR	6.231	7	1.18	. 7	0.22
B.S. 10 MHZ OSCILLATOR	2.641	7	05.0	7	0.10
SCAN SWITCH	1.488	8	1.13	ហ	0.23
SCAN MODULATOR	30.158	7	5.72	4	0.57
ANT. SELECT SWITCH	1.269	m	0.36	ស	0.07
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SMALL COMMUNITY

UNIT	FAILURE RATE (FAIL/10 ⁶ HRS)	QTY.	PERCENT OF TOTAL FR	TASK	MTTR
ANT. PWR SUPPLY CHASSIS PARTS	0.164	1	0.02	3	0.01
PWR DIST. ASSY PARTS	8.886	-	0.84	, M	0.59
MAINTENANCE INTEGRATOR	6.446	9	3.67	2	0.70
MAINTENANCE MONITOR INTEGRATOR	8.400	7	1.59	2	0.30
MON. ANT BOX ASSY, PARTS	4.979	1	0.47	ĸ	0.33
LIGHTNING PROT. BOARD #1 A	1.798	7	0.17	2	0.03
LIGHTNING PROT. BOARD #1 B	3.095	H	0.29	2	90.0
LIGHTNING PROT. BOARD #2	1.319	-	0.13	2	0.02
LIGHTNING PROT. BOARD #5 A	5.269	Ħ	05.0	2	0.10
LIGHTNING PROT. BOARD #5 B	5.281	п	0.50	2	0.10
LIGHTNING PROT. ASSY	0.918	7	0.17	7	0.03
VIDEO AMP A	0.807	6	69.0	2	0.13
VIDEO AMP B	0.987	S	0.47	7	. 60.0
MON. ANT BANDPASS FILTER	0.629	7	0.12	ĸ	0.08
MON. ANT. DIVIDER	0.943	7	0.18	m	0.13
DIRECTION COUPLER	0.010	~	0.01	m	0.01
			100.00		24.37
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SUPPLEMENT B

HUMAN FACTORS AND SAFETY
EVALUATION CHECKLISTS
FOR
MLS GROUND EQUIPMENT

1.0 INTRODUCTION

This document describes a method for evaluating the extent to which Human Factors and Safety Engineering criteria have been designed into the equipment. The method described utilizes a series of checklists which have been prepared, to digest and summarize the design criteria given in MIL-STD-1472A. Specifically for the MLS application, two additional checklists have been prepared for the safety and grounding requirements given in FAA-G-2100 1/b and amendment B, attachment I.

Tabulation forms are also provided so that the numerous factors involved can be systematically applied in the evaluation of the hardware. The forms also provide a written record of the results of the evaluation, including specific comments and recommendations.

2.0 DESCRIPTION OF CHECKLISTS

So that the user may have an overview of the evaluation procedure, an outline of the checklists, showing their organization into groups, is provided and described.

The checklists are grouped into three major categories according to their applicability to specific hardware features. The first group of checklists relates to the evaluation of control and display panel layout. The second group is to be used for the evaluation of workspace and environment related criteria. The third group relates to hardware factors other than panel layout and workstation design.

Some of the factors are duplicated in several of the checklists (e.g. under labeling or safety). However, there is no duplication in the evaluation procedure itself, since the duplicated factors apply to different aspects of the hardware design, which should be evaluated separately and independently.

There is duplication, however, between some of the factors in the safety checklist R (MIL-STD-1472A) and checklist S (FAA-G-2100 1/b). Rather than merge the two checklists, they are kept separated so that the FAA-G-2100 requirements can be independently identified, and can be deleted from evaluations for which they are not applicable.

Group I - Panel Layout Checklists

- A. Control Display Integration
- B. Visual Displays (general criteria)
- C. Transilluminated Displays
- D. Scale Indicators
- E. Other Visual Displays
- F. Auditory Displays
- G. Controls
- H. Labeling

Group II - Facility, Shelter, Workstation Checklists

- I. Anthropometry
- J. Workspace
- K. Console Design
- L. Stairs, Ramps, Ladders, Doors, Hatches
- M. Environment
- N. Trailers, Vans, Enclosures
- O. Safety

Group III - Equipment Checklists

- P. Maintainability
- Q. Labeling
- R. Safety
- S. Safety (FAA-G-2100 1/b)
- T. Grounding (FAA-G-2100 1/b)

3.0 USE OF CHECKLISTS AND TABULATION FORMS

A separate tabulation form is provided for each of the three checklist groups so that each may be evaluated independently as is applicable to the specific hardware and/or hardware level.

In using the various forms, a separate form should be completed for each item under evaluation, as applicable. For example, in an equipment console with five unit drawers, a separate panel form should be completed for each unit front panel that has controls or displays in sufficient number to warrant a detailed human factors evaluation. Similarly, each of the drawers might warrant separate evaluation for the Group III criteria (especially if each drawer is designed by a different subcontractor). Where uniform design criteria have been employed throughout all drawers, one Group III form might be applicable for the entire console. Separate Group II forms should be prepared for each work station (whether seated or standing) and for the general work area, facility and/or shelter.

In all of the checklists, each of the factors is expressed as a question. If the answer to the question is a yes, a "check" is placed into the appropriate box. This check implies that the human factors/safety criterion expressed by the factor is satisfied without qualifications.

If the criterion is not satisfied, or if the criterion is satisfied with certain qualifications, then a "C" (for comments) is placed into the appropriate box. The evaluation of all factors scored with a "C" should be elaborated upon under the comments section. Where the criterion is evaluated as satisfied with qualifications, such qualifications should be delineated. Where the criterion is evaluated as not being satisfied, the comments should indicate the specific reasons for the evaluation along with suggested recommendations. (Note: such recommendations might include "no change." Where such a recommendation

is given, the reasons why this recommendation is made should be given.)

If the factor is not applicable to the particular design, an "N" is placed into the appropriate box. Placing an N into the box, instead of leaving it blank, provides a positive record of all of the factors that were included in the evaluation and states that, in the evaluator's opinion, these factors were not applicable.

GROUP I - PANEL LAYOUT CHECKLISTS

CHECKLIST A - CONTROL-DISPLAY INTEGRATION

- 1. Relationship is the relationship between a control and its associated display apparent from the use of proximity, grouping, coding, framing, labeling or similar design techniques?
- 2. <u>Precision</u> is the precision of control manipulation consistent with the precision required by the display? Conversely, is the precision of the display presentation consistent with the range of control movement?
- 3. Feedback adequate feedback provided on control response?
- 4. <u>Functional Grouping</u> are functionally related controls and displays located in proximity to one another, arranged in groups by sequence, frequency of use or importance?
- 5. <u>Borders</u> where appropriate, are borders used to designate functional groups?
- 6. Movement are the movement of display indicators sufficiently clear and unambiguously direct to guide the appropriate control response?
- 7. <u>Time Lag</u> has time lag or inertia between control movement and display presentation been eliminated or minimized?
- 8. <u>Direction</u> in both controls and displays, do movements which are clockwise, forward, up or to-the-right represent an increase in setting magnitude?
- 9. Control-Display Ratio has the control-display ratio been selected to minimize the total time required to make the desired control movement?

CHECKLIST B - VISUAL DISPLAYS

1. <u>Information Content</u> - is the displayed information limited in content to that which is required to perform specific actions or to make decisions?

- 2. <u>Precision</u> is the information displayed only to the degree of precision required for a specific action or decision?
- 3. Format is the information displayed in directly usable form (no transposing, interpolating, computing, etc.)?
- 4. <u>Display Failures</u> are display failures immediately apparent as display failures?
- 5. Failsafe are display circuits designed so that display failures do not cause equipment failures?
- 6. <u>Unrelated Markings</u> are markings, such as trademarks or company names, which are not related to the panel function eliminated from the panel face?
- 7. <u>Location</u> are displays located so that they may be read to the precision required by personnel in the normal operating position?
- 8. Access can displays be read without the use of ladders, supplementary lighting, or other special equipment?
- 9. Orientation are display faces perpendicular to the operator's normal line of sight, wherever feasible? If not normal, is the display face greater than the minimum 45° from the normal line of sight?
- 10. <u>Reflectance</u> are displays constructed, arranged and mounted to minimize the reflectance of ambient illumination?
- 11. <u>Vibration</u> has display vibration been eliminated so that operator performance is not degraded below required levels?
- 12. Grouping are displays logically grouped according to their sequence of use, functional relations, frequency of use and importance?
- 13. <u>Importance</u> are critical displays placed in privileged positions in optimum visual zones or otherwise highlighted?

- 14. Minimum Viewing Distance is the minimum viewing distance greater or equal to 13 inches?
- 15. Maximum Viewing Distance for displays associated with local controls, is the viewing distance within the maximum reach distance of 28 inches?

CHECKLIST C - TRANSILLUMINATED DISPLAYS

- 1. Equipment Response do lights display equipment response and not merely control position?
- 2. Positive Feedback is the "lamp on" position used to denote a positive indication of the condition sought? (e.g. go-ahead, ready, malfunction.)
- 3. Grouping are master caution, master warning, and summation lights set apart from component status lights?
- 4. <u>Location</u> are critical function indicators located within 15° of the operator's normal line of sight?
- 5. Maintenance Displays on units having operator displays, are maintenance displays located behind access doors?
- 6. <u>Brightness</u> are displays within the range of 10% to 300% brighter than the surrounding brightness?
- 7. Reflections are provisions made to prevent direct or reflected sunlight from making indicators appear illuminated?
- 8. <u>Brightness Control</u> for applications with varied ambient brightness, is a variable control provided?
- 9. <u>Lamp Redundancy</u> except for airborne applications, are incandescent bulbs redundant?
- 10. <u>Lamp Test</u> is a lamp test provided on panels with greater than three bulbs?
- 11. Lamp Removal where possible, are provisions made to remove incandescent bulbs from the front of the display without tools and while power is applied?

- 12. Color Coding do colors conform to applicable specifications? (Where unspecified, do they conform to MIL-C-25050?)
- 13. <u>Legend Lights</u> are legend lights used in preference to simple indicator lights to the maximum extent practical?
- 14. <u>Transilluminated Panel Assemblies</u> are panel assemblies which present whole patterns of information applicable? (Suitable for presentation of data flow and complicated data organization.)

CHECKLIST D - SCALE INDICATORS

- 1. <u>Selection</u> except where necessitated by operational restrictions, are moving-pointer, fixed-scale indicators selected in preference to fixed-pointer, moving scale indicators?
- 2. <u>Linearity</u> are non-linear scales avoided except where system requirements dictate nonlinearity?
- 3. Scale Markings are scale graduations multiples of 1, 2, or 5? Is the number of intermediate markings less than nine?
- 4. Contrast is the contrast between the scale face and the markings at least 50%.
- 5. <u>Coding</u> is the face of the scale coded (pattern and/or color) to indicate ranges, zones, operating levels, etc?
- 6. <u>Numerical Progression</u> does the numerical progression increase as the scale is read clockwise, from left to right or from bottom to top?
- 7. Orientation are scale numerals upright when in the reading position?
- 8. Zero Position in Fixed Circular Scales when positive and negative values are displayed around a zero or a null position, is the null point located at either 12 o'clock or at 9 o'clock? Are positive values represented by clockwise pointer motion?

- 9. <u>Null Indicators</u> is the circuit designed so that, if power fails, the indicator will NOT rest in the in-tolerance position?
- 10. Fixed-Pointer, Moving-Scale Indicators should be avoided. Where required, is the unused portion of the dial face covered in applications requiring the setting of a value? For tracking applications, is the whole dial face exposed?

CHECKLIST E - OTHER VISUAL DISPLAYS

- 1. <u>CRT Size</u> are the signal size and CRT display size consistent with the computations resulting from the requirements of 20 minutes of visual angle?
- 2. CRT Viewing Distance is a 16 inch viewing distance provided? Does the design permit the observer to view the scope from as close as he may wish? Are displays which must be viewed from distances greater than 16 inches appropriately modified?
- 3. CRT Brightness does ambient illumination contribute less than 25% of screen brightness?
- 4. Faint Signals are hoods or shields provided for CRT when the ambient illumination is above 0.25 FT-C?
- 5. Reflected Glare is the scope placement, relative to light sources, selected to minimize reflected glare?
- 6. Adjacent Surfaces are surfaces adjacent to the scope of a dull matte finish? Do they have a brightness range between 10% and 100% of the screen background brightness?
- 7. Counter Mounting are mechanical counters mounted as close as possible to the panel surface to minimize parallax?
- 8. Counter Movement is the movement of mechanical counters snap action rather than continuous? Does a clockwise rotation of the reset knob increase the indication?

- 9. Printer Format is printed information presented in directly usable form?
- 10. <u>Printer Supplies</u> are printers designed for quick insertion and removal of printing materials? Is a take-up device provided? Is there a positive indication of remaining supply?
- 11. <u>Annotation</u> are printers mounted so that tapes may be annotated easily while still in the recorder?
- 12. Plotter Contrast where plotters are used is a minimum of 50% contrast provided between the plotted function and the background?
- 13. <u>Job Aids</u> are aids (e.g. graphic overlays) provided when an operator is required to interpret graphic data?
- 14. Flags is the use of flags restricted to non-emergency conditions? Do they operate by snap action? Is a minimum of 50% contrast provided between the flag and its background? Does a malfunction flag at least partially obscure the operator's view of the normal display? Is a flag test provided?

CHECKLIST F - AUDITORY DISPLAYS

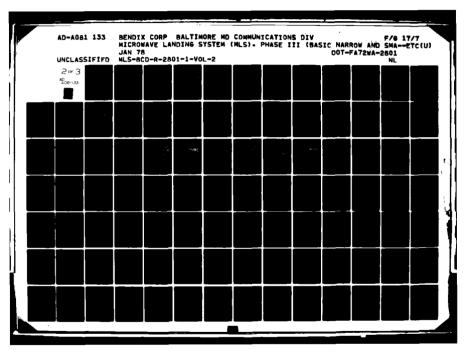
- 1. Application are auditory displays provided in situations with any of the following conditions?
 - a. The information is short, simple and transitory and requies immediate or time-based response.
 - b. Visual display is restricted by overburdening, illumination, operator mobility, degradation of vision by reason of vibration, high g-forces, hypoxia, or other environmental factors; or anticipated operator inattention.
 - c. To warn, alert or cue the operator to subsequent additional response, or the criticality of response.
 - d. Custom or usage has created anticipation of display.
 - e. Voice communication is necessary or desirable.

- 2. Type are the application of tones and non-periodic complex sounds restricted to status indication?
- 3. <u>False Alarms</u> are false alarms minimized or precluded in the design?
- 4. Circuit Test are circuitry test devices provided?
- 5. <u>Caution Signals</u> are caution signals readily distinguishable from warning signals?
- 6. Relation to Visual Displays when used with visual displays, are auditory signals used to supplement or support the visual display?
- 7. Frequency is the frequency of the tone between 250 and 2500 hertz?
- 8. <u>Intensity</u> is the sound pressure level at least 20 dB above the maximum ambient noise level?
- 9. <u>Headsets</u> are headsets provided where ambient noise will exceed 100 dB?
- 10. Discriminability where several different auditory signals are used, are they readily discriminable through the use of differences in pitch, intensity, beats, harmonics and/or coding?
- 11. Prohibited Types of Signals are prohibited types of signals avoided? (Prohibited signals are those which might be confused with sounds or noises which are likely to occur under normal operating conditions. These signals include tones resembling navigation signals or coded radio transmissions, static, electrical interference, bfo glissandi, cross modulation, random noise, bagpipes, etc.)
- 12. <u>Compatibility</u> is the meaning of the audio warning signal compatible with established meanings?
- 13. <u>Masking</u> are means provided to prevent audio warning signals from interfering with other critical functions or warning signals?

- 14. Verbal Warnings is the voice used distinctive and mature? Is the delivery formal, impersonal and calm? Is the message content intelligible, apt and concise?
- 15. Controls for Auditory Warning Devices are persistent signals provided with a shut-off (automatic or manual) control, and a volume control? Is automatic reset provided? Are volume controls restricted to prevent reducing the volume to an inaudible level?

CHECKLIST G - CONTROLS

- 1. Selection has the selection of types of controls considered, as applicable, distribution of load (overburdening of operator's limbs), multirotation for precision over wide ranges, detents for discrete functions?
- 2. Sequential Operations where sequential operations follow a fixed pattern, are the controls arranged to facilitate the operation?
- 3. <u>Coding</u> where applicable, are controls coded by labeling, location, shape, size and/or color for differentiation?
- 4. Accidental Activation are controls designed and located to minimize their susceptibility to accidental activation without precluding normal operation within the required time?
- 5. <u>Dead Man Controls</u> are dead man controls utilized wherever operator incapacity can produce a critical condition?
- 6. Concentric Shafts for concentric shaft vernier controls is the larger diameter knob used for the fine adjustment? Are the knobs adequately coded to avoid confusion?
- 7. Spacing are minimum separation requirements between controls met?



- 8. Rotary Controls do rotary switches have a moving pointer and a fixed scale? Except where shape coding is used and torque is light, are the knobs bar shaped? Do blind switches have no more than 12 positions? Are visible switches limited to 24 positions? Are stops provided where ranges are applicable?
- 9. Thumb Wheels is color coding used to facilitate checking of off and normal positions? Can the readout be viewed from all operator positions? In non-detented switches is a resistance provided?
- 10. <u>Knobs</u> are knobs used where little force is required and precise adjustments of a continuous variable are required? Is a moving knob with fixed scale employed?
- 11. Pushbuttons are pushbuttons used for momentary contact or for locking circuitry? Is the button surface either concave or a nonslip surface? Is there a positive indication of activation (tactual, click, lamp, etc.)?
- 12. <u>Toggle Switches</u> are toggle switches of three or more positions avoided? Are the switches oriented vertically with down representing "off"?
- 13. Legend Switches is there a positive indication of switch activation? Is the legend legible with only one lamp operating? Are the lamps replaceable from the front? Is there a maximum of three lines of lettering on the legend plate?
- 14. Other Controls are cranks, handwheels, levers or pedals provided, as applicable, for tasks requiring many rotations, large forces, multidimensional movements or large displacement?

CHECKLIST H - PANEL LABELING

1. <u>Label Characteristics</u> - do the labels provide for accurate identification of required functions at the

- working distance required with the available illumination in the time available for recognition and reponse? Is the criticality of the function labeled or coded?
- 2. Orientation are labels oriented horizontally so that they may be read quickly and easily? Where the use of vertical labeling cannot be avoided because of space limitations, is its use restricted to non-critical functions?
- 3. Abbreviations are standard abbreviations employed?
- 4. Qualities are the labels brief, visible, legible, unobscured, of high contrast? Do they use words familiar to the operator?
- 5. <u>Label Characters</u> do the characters conform to MIL-M-18012? Is the ratio of letters to reading distance between 0.4% and 1.0% (For illumination levels below 1 foot lambert the ratio shall be increased by 50%). Is a 5/3 aspect ratio used? Is the stroke width 1/6 of the height?
- 6. <u>Functional Labeling</u> is each control and display labeled according to function, avoiding similar names for different controls and displays? Does the label reflect the function being measured or controlled? Does the label indicate the functional result of control movement (e.g. increase)? Where control and displays are used together, do the labels indicate their functional relationship?
- 7. Location does the location of the label give priority to ease of operation over label visibility? Are labels located above the control and displays they describe? (Except where visibility will be enhanced by locating the label below the control...e.g. eye level or higher.) Are the units of measurement located on the panel? Are labels identifying functionally grouped controls and/or displays provided? Are such labels located above the functional group identified and centered?

8. Size Graduation - to reduce confusion and search time, are labels graduated in size with group controls labeled with larger characters than individual controls, and with size graduations decreasing down to individual control position labels? Has the size of the smallest characters been determined by the viewing distance criteria? Is each size graduation approximately 25% larger than the next smaller size?

HUMAN FACTORS ENGINEERING PANEL LAYOUT CHECKLIST

EQUIPMENT	SHELTER ———	CABINET
IINIT	EVALUATOR	DATE

CHECKLIST	FACTOR														
CHECKLIST	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
A															
B															
С															
מ															
E															
Ŧ															
G															
H															

(√- SATISFACTORY; C - REFER TO COMMENTS; N - NOT APPLICABLE)								
CHECKLIST ITEM	COMMENTS	RECOMMENDATIONS						
	•							
•		·						
	C-60							

GROUP II - FACILITY, SHELTER, WORK STATION CHECKLISTS

CHECKLIST I - ANTHROPOMETRY

- 1. Gross Dimensions do gross dimensions of passageways, accesses, clearances, etc. permit the passage of the body or parts of the body based upon the 95th percentile values of applicable body dimensions?
- 2. <u>Limiting Dimensions</u> are limiting dimensions (such as reach distance, control movements, etc.) which restrict or are limited by body extension based upon the 5th percentile values of applicable body dimensions?
- 3. Adjustable Dimensions do the dimensions of adjustable devices (seats, safety belts, goggles, etc.) span a range sufficient to accommodate the 5th through the 95th percentile values of applicable body dimensions?
- 4. <u>Use of Dimension Data</u> in selecting the design-critical dimensions, does the design allow for the nature, frequency and difficulty of the tasks?
- 5. <u>Body Position</u> has the position of the body during performance of the task been allowed for in the design dimensions?
- 6. <u>Flexibility</u> has mobility and flexibility requirements imposed by required tasks been included in designcritical dimensions?
- 7. Obstacles have increments in design-critical dimensions been included to account for the need to compensate for obstacles, projections, garments, packages, lines, padding, etc?

CHECKLIST J - WORK SPACE CHECKLIST

1. <u>Kick Space</u> - do all cabinets, consoles and work surfaces that require an operator to stand or sit close to the front surface contain a minimum kickspace of 4 inches deep and 4 inches high?

- 2. <u>Handles</u> are handles on cabinets and consoles either recessed to eliminate projections or designed so they will neither injure personnel nor entangle clothing or equipment?
- 3. Work Space a free floor space of at least 4 feet in front of each console is desirable. Where maintenance is required, are the following minimum work spaces provided?
 - a. Depth of work area 42 inches minimum between the rack and the opposite surface or obstacle.
 - b. Lateral work space (for racks with drawers) -
 - 1. Drawers weighing less than 45 pounds 18 inches on one side, 4 inches on the other.
 - 2. Drawers weighing over 45 pounds 18 inches on each side.
 - c. Storage space adequate and suitable for manuals, worksheets, and other operational or maintenance materials.
- 4. Work Surfaces (standing) are work surfaces for standing operations 36 inches above the standing surface? (unless otherwise specified in the contract).
- 5. Display Placement (standing) for standing operations, are displays mounted on vertical panels placed in an area between 41 and 74 inches above the floor? Are displays requiring frequent and/or precise readings placed in an area between 50 and 69 inches above the standing surface?
- 6. Control Placement (standing) for standing operations, are controls mounted on vertical panels located in an area between 34 and 74 inches above the standing surface? Are controls requiring frequent, and/or precise operation and emergency controls located in an area between 34 and 57 inches above the standing surface and no further than 22 inches laterally from the centerline?

- 7. Work Surfaces (seated) for seated operations, are work surfaces at least 30 inches wide by 16 inches deep? Are desk tops and writing tables placed 30 inches above the floor? Are writing surfaces on equipment consoles at least 16 inches deep by 23 inches wide?
- 8. Seating are seats adjustable, vertically, from 16 to 23 inches in increments of no more than one inch? Is a backrest provided that reclines between 103° and 115°? Where applicable, is at least one inch of cushioning provided on both the seat and the backrest? Are 2 x 8 inch armrests provided?
- 9. <u>Knee Room</u> for seated operations, is knee and foot room provided that equals or exceeds 25 inches in height, 20 inches in width and 18 inches in depth?
- 10. Display Placement (seated) for seated operations, are displays mounted on vertical panels located between 6 and 48 inches above the sitting surface? Are displays requiring frequent and/or precise readings placed between 14 and 37 inches above the sitting surface and no further than 22 inches laterally from the centerline? Are critical warning displays mounted at least 22.5 inches above the sitting surface on consoles requiring horizontal vision over the top?
- 11. Control Placement (seated) for seated operations, are controls mounted on vertical panels located between 8 and 35 inches above the sitting surface? Are controls requiring frequent and/or precise operation mounted between 8 and 30 inches above the sitting surface.
- 12. <u>Unusual Positions</u> does the work space design for work to be accomplished in unusual positions (squatting, stooping, kneeling, crawling, or prone) conform to the appropriate preferred dimension? Do all clearance dimensions provide no less than the minimum values specified?

CHECKLIST K - CONSOLE DESIGN

- Dimensions do the dimensions of standard console designs conform to the dimensions given in Table VII of MIL-STD-1472A?
- 2. <u>Configurations</u> are standardized console configurations employed wherever feasible?
- 3. <u>Variables</u> have the following variables been considered in choosing the most appropriate console design?
 - a. visibility over the top of the console.
 - b. operator mobility requirements.
 - c. panel space requirements.
 - d. volume required below the writing surface.

Where special purpose console designs are required, the following checklist items apply:

- 4. <u>Panel width</u> for panel widths exceeding 44 inches, is a flat-surface, segmented, wrap-around console provided so that all controls are within the reach of a 5th percentile operator?
- 5. <u>Dimensions</u> where vision over the top is not required, is the width of the control segment kept to within 34 inches? Are the left and right segments no more than 24 inches wide?
- 6. <u>Viewing Angle</u> is the total left-to-right viewing angle kept to below 190°?
- 7. Vertical Panel Division where forward vision is not required and lateral space is limited, is the panel divided into three vertical/stacked segments with surfaces perpendicular to the operator's line of sight with little or no head movement?
- 8. Vertical Segment Height where vertical/stacked segments are used, is the center of the central segment 31.5 inches above the seat reference point? Is the height of this segment limited to 21 inches?

CHECKLIST L - STAIRS, LADDERS, RAMPS, DOORS, HATCHES

- 1. <u>Selection</u> does the selection of stairs, stair-ladders, fixed ladders or ramps conform to the angle of ascent requirements of MIL-STD-1472A?
- 2. Hand-carrying of Equipment are ramps or elevators provided when equipment weighing more than 40 pounds must be hand carried? Are stairs or steps provided rather than ladders in any application requiring hand-carrying of equipment under 40 pounds?
- 3. <u>Handrails and Guardrails</u> are handrails provided on each side of stairs, stair-ladders, fixed ladders and ramps? Where one or both sides are open, are intermediate guardrails provided?
- 4. Stairs are stair dimensions within the maxima or minima specified in Figure 26?
- 5. Stair Ladders are stair ladder dimensions within the minima or maxima of Figure 27? Is the tread rise open at the rear? Are landings provided every tenth or twelth tread? Is the tread surface either of open grating material or treated with nonskid material? Are they of metal construction? Do handrails have non-slip surfaces?
- 6. Fixed Ladders are ladder dimensions within the maxima or minima of Figure 28? Are ladders providing access to multiple levels offset at each level? Is a guardrail provided at the opening at the top of each fixed ladder? Is safety caging provided on fixed ladders more than 20 feet high?
- 7. Ramps where cleating is required for pedestrian ramps, are the cleats spaced 14 inches apart? Do they extend from handrail to handrail at right angles to the line of traffic? Where vehicular and pedestrian traffic must be mixed on one ramp, is the vehicular surface located in the center of the ramp, with pedestrian traffic next to the handrails?

- 8. Platforms are platform surfaces constructed of open metal grating or treated with non-skid material? Do open sides have guardrails not less than 42 inches high (with intermediate rails) and a toeboard or guard screen not less than 3 inches high? Are hand holds provided where needed.
- 9. Elevators, Inclinators, Hydraulic Platforms are the following items and devices provided?
 - a. maximum load signs.
 - b. control guards to prevent accidental operation.
 - c. limit stops.
 - d. a fail-safe brake or other self-locking device.
 - e. provision for manually lowering the platform, where feasible.
 - f. for open platforms see the factors under platforms.
- 10. Doors when a sliding door is used, is a separate hinged door in the sliding door provided for personnel exit? Is fixed equipment at least 3 inches from the swept area of hinged doors?
- 11. <u>Hatches</u> are wall hatches flush with the floor, where possible? Do hatches open with a single hand or foot motion? Is the unlocking force for handles less than 20 pounds? Can overhead hatches be opened with less than 50 pounds force?
- 12. Hatch Dimensions do hatches accommodate limiting dimensions for location and operability and gross dimensions for size and passage? (Including any requirements for carrying equipment through the hatch.) Do rectangular hatches conform to Figure 29 of MIL-STD-1472A? Is the minimum diameter of circular hatches 30 inches? Are appropriate foot rests or steps provided where a step-down through a top access exceeds 27 inches?

CHECKLIST M- ENVIRONMENT

- 1. <u>Heating</u> is heating provided in mobile personnel enclosures capable of at least 50°F? For semi-permanent facilities, is the heater capable of at least 68°F?
- 2. Ventilation does the ventilation system provide a minimum of 30 cfm per man? Is approximately 2/3 of the ventilation from outside air? Is the air flow moving past the man kept below 100 cfm (65 cfm preferred)?
- 3. Air Conditioning is air conditioning provided for enclosures with effective temperatures exceeding 85°F?

 Is the air conditioning system designed so that coldair discharge is not directed on personnel?
- 4. <u>Humidity</u> is the humidity value approximately 45% @ 70°F? Are provisions made to prevent the humidity from decreasing below 15%?
- 5. Temperature Uniformity is the difference in air temperature from floor to ceiling within 10°F?
- 6. Thermal Tolerance is the combined temperature-humidity exposure within the prescribed tolerance limits (when corrected for air flow rates)?
- 7. <u>Illumination</u> is the illumination at the prescribed levels for the required tasks? Is the illumination distributed to reduce glare and specular reflection?
- 8. Hazardous Noise is noise generated by equipment kept below the maximum allowable levels prescribed by applicable specifications? Is noise generation and penetration controlled to the extent that acoustic energy will not cause personnel injury, interfere with voice or other communications, cause fatigure or in any other way degrade over-all system effectiveness?
- 9. Speech Interference are the facility and equipment noise controlled to levels that will permit the necessary voice communications as determined by applicable measures? (Articulation index, speech interference levels, and/or noise criteria).

- 10. Facility Design does the design of the facility control the noise level to the optimum extent feasible through effective sound reduction and attenuation techniques?
 - a. Attenuation sound absorbing materials for floors, walls, ceilings; staggered walls, staggered doors, double-paned windows, baffles.
 - b. Reverberation time is reverberation time reduced to the limits given in Figure 35 of MIL-STD-1472A?
 - c. Absorption Coefficient is the sound absorption coefficient at least 0.2, but less than 0.5?
- 11. Vibration are the facility and equipment designed to control the transmission of whole body vibrations to levels consistent with comfort, proficiency and safety limits? Are equipment vibrations below levels which impair control manipulation or display readability?

CHECKLIST N- TRAILERS, VANS AND TRANSPORTABLE ENCLOSURES

- 1. Brake Controls are trailer brake controls located so that an operator can reach them while restraining or positioning the trailer manually? Are the controls located on the side away from road traffic?
- 2. <u>Positioning Controls</u> are trailers equipped with precise positioning controls when the trailer must mate parts?
- 3. Landing Gear Lock can the landing gear lock and release be operated by either the hand or the foot?
- 4. <u>Vans and Enclosures</u> do vans and transportable enclosures which serve as shelters for men and equipment and which require recurring occupany in excess of one hour meet the following criteria?
 - a. ceiling height minimum of 78 inches.
 - b. personnel access (doors) minimum of 76 inches high
 by 30 inches wide.

- c. equipment access openings as appropriate and convenient.
- d. steps, stairs or ladders provided for van floors more than 18 inches above ground level.
- e. access doors capable of being locked in open as well as closed positions, and provided with inner releases.

CHECKLIST O - SAFETY

- 1. Safety Labels and Placards are conspicuous placards mounted adjacent to any hazardous equipment? Are jacking and hoisting points labeled? Are areas requiring special protective clothing specifically identified? Are "NO-STEP" markings provided? Are receptacles marked, as appropriate, with voltage, phase and frequency characteristics? Are pipe, hose and tube lines clearly labeled or coded? Are floor openings properly marked?
- 2. Fire Extinguishers are fire extinguishers of the correct type readily accessible? Are they located where fires will not block access to them?
- 3. <u>Alerting Devices</u> is a hazard alerting device provided? Is the sound distinctly recognizable and unlikely to be masked by other noises?
- 4. Emergency Exits are emergency exits readily accessible, unobstructed and quick opening (5 seconds or less)?
- 5. Obstructions are walkways, steps and work areas well designed and free of dangerous projections and/or obstructions?
- 6. <u>Illumination</u> is adequate illumination provided in all areas? Are warning placards, stairways and all hazardous areas particularly well illuminated?
- 7. Energy Sources are energy sources isolated?
- 8. Antenna Range is there an antenna microwave radiation hazard zone? Is it clearly marked and guarded?

9. Safety Mesh - is a screen or safety mesh installed on the underside of open gratings, platforms or flooring surfaces where there is a possibility that small tools or parts may fall through on workers or equipment beneath the grating?

HUMAN FACTORS ENGINEERING FACILITY-SHELTER-WORK STATION CHECKLIST

EQUIPMENT		_	CABINET AREA					<u></u>							
EVALUATOR				_							DA	TE _			
	CHECKLIST						FAC	TOR						•	
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CHECKLIST	COMMENTS									R	ECO	MME	NDAT	ONS	
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GROUP III - EQUIPMENT/UNIT CHECKLISTS

CHECKLIST P - MAINTAINABILITY

- 1. <u>Special Tools</u> are special tools, required for operational adjustments, securely mounted in a readily accessible location within the equipment?
- 2. Clothing Constraints where applicable, does the design permit installation, removal and maintenance by personnel wearing required special purpose clothing or equipment?
- 3. Mounting of Parts are parts mounted on a two-dimensional surface rather than stacked? Are similarly formed components mounted in a standard orientation? Are delicate components either located or guarded to reduce damage susceptibility?
- 4. Adjustments Controls are knobs, rather than screw-driver adjustments employed for frequently adjusted controls? Are reference scales or other feedback provided for all adjustments? Are limit stops on calibration or adjustment controls provided, where required? Are sensitive adjustments located or guarded to avoid inadvertent disturbance? Are screwdriver shaft guides provided where adjustments must be made without the aid of vision?
- 5. Accessibility are structural members located so that parts, components and replaceable items can be removed without difficulty? Are sliding, rotating or hinged units, to which rear access is required, free to open or rotate to their full distance? Are braces, gravity or other means provided to hold hinged assemblies open or in the "out" position while being worked on?
- 6. <u>Lubrication</u> can mechanical components requiring it, be lubricated without disassembly? Are extended fittings provided to lubricate parts not readily visible or accessible? Are labels provided which specify lubrication type and frequency?

- 7. Cases and Covers are edges and corners rounded or otherwise finished to prevent injury? Are cases designed to be lifted from units rather than units lifted from cases? Is the case size large enough to avoid damage to wire or parts when cases are put on or removed? Are guides, tracks, slides or stops provided, as necessary, to prevent injury to personnel or damage to units? Is it obvious when a cover, which is in place, is not secured? Can covers be removed without interference from bulkheads, brackets or other units?
- 8. Access Openings are covers for access openings either completely removable or self-supporting in the open position? Are labels provided identifying accessible items, recommended procedures, and/or hazards? Are arm and hand access openings large enough to not only permit the required operation but, where possible, provide an adequate view of the manipulated parts? Is an interlock provided on the access cover where hazardous voltages exist?
- 9. <u>Fasteners</u> are captive bolts and nuts used in situations where dropped items might cause damage to equipment or create a difficult or hazardous removal problem? Are captive fasteners provided for access covers requiring periodic removal?
- 10. Unit Handling are rests or stands provided, where feasible? (Including space for tools and test equipment.) Are irregular, fragile, or awkward extensions (cables, wave guides, hoses, etc.) designed for easy removal before handling?
- 11. Weight are the unit weight vs height requirements within the maximum limits of Table XVII of MIL-STD-1472A? Are labels provided for items weighing more than the one-man lift values? Where mechanical or power lift is required are hoist and lift points provided and clearly labeled?

- 12. Handles and Grasp Areas are all removable units provided with handles or other suitable means for grasping, handling and carrying? Wherever possible, are handles located relative to the center of gravity of the unit to preclude swinging or tilting? Are handles located to provide at least 2 inches of clearance from obstructions during handling? Do foldout handles have a stop in open position? Can they be opened with one hand? Do handles meet the dimension requirements of Figure 30 of MIL-STD-1472A?
- 13. Mounting can units be removed along a straight line (or slightly curved line) rather than through an angle? Are rollout racks, slides or hinges provided on units frequently pulled out from installed positions? Are consoles or cabinets bolted down where rollout racks may cause the entire console to tip over? Are limit stops provided on racks and drawers? Are interlocks provided, where applicable? Are braces provided to hold hinged units in the "out" position?
- 14. Connector Spacing are connectors spaced far enough apart to permit firm grasping for connecting and disconnecting? Is a minimum of 1 inch spacing provided? (except where a line of connectors are always removed sequentially.)
- 15. <u>Test Points</u> are test points located close enough to associated controls so that the displayed signals can be read?
- 16. Test Equipment does portable test equipment weigh under 25 pounds if it is to be carried by one man? Does the test equipment have built-in storage space for leads, probes, manuals and/or special tools?
- 17. Failure Indication is an indication of prime power failure provided? Are labels provided indicating fuse ratings? Can fuses be readily replaced? Are displays

provided to indicate if equipment has failed? Is an auditory alarm provided (where applicable) to indicate a critical malfunction?

CHECKLIST Q - LABELING

- 1. Label Characteristics do the labels provide for accurate item identification at the required working distance, with the available illumination in the time available for recognition? Is there consistency in label design within and between systems?
- 2. <u>Label Characters</u> do the characters conform to MIL-M-18012? Is the ratio of height of letters to reading distance between 0.4% and 1.0%? (For illumination levels below 1 foot lambert the ratio shall be increased by 50%). Is a 5/3 aspect ratio used? Is the stroke width 1/6 of the height?
- 3. Assemblies, Components, Parts is each assembly, component and part labeled clearly and visibly with a readable, meaningful name, number or symbol?
- 4. Location are the gross identifying labels on assemblies or major components located externally in position not obscured by adjacent assemblies or components? Are they located on the flattest, most uncluttered surface available? Are they located on the main equipment chassis?
- 5. <u>Life</u> are labels located in a way to minimize wear or obscurement by grease, grime or dirt? Is accidental removal, obstruction or handling damage precluded?
- 6. Terms are components, circuits or assemblies labeled with terms descriptive of the test or measurement applicable to their test points? (e.g. demodulator rather than crystal detector.)

CHECKLIST R - SAFETY

- 1. Warning Placards are conspicuous placards mounted adjacent to any equipment which presents a hazard to personnel? (e.g. high voltage, high frequency, hot equipment, where mechanical components (linkages, springs, etc.) are under constant load or strain, noxious gases, moving parts, jacking and hoisting points, liquid, gas and steam pipelines, and radiation.) Are the center of gravity and/or the weight distinctly marked on equipment, as applicable?
- 2. <u>Hazardous Locations</u> is the placement of internal controls near hazardous locations avoided? (e.g. high voltages, rotating machinery or hot parts.) Where such location cannot be avoided, are appropriate shields and labels provided?
- 3. <u>Interlocks and Alarms</u> does the operation of a switch or control which initiates a hazardous operation (e.g. movement of a crane) require the prior operation of a related or locking control? Where practical, is a visual or auditory warning device activated?
- 4. Access are parts which retain heat or electrical potential after equipment is turned off located so that they will not be touched during normal maintenance? Are discharge or bleeder devices provided for high-energy capacitors? Are covers, structural members, etc., either grounded or protected? Are struts and latches provided to keep hinged and sliding components from shifting? Do drawers and fold-out assemblies have limit stops? Are safety interlocks used in high voltage distribution circuitry?
- 5. Edge Rounding are exposed edges rounded to a minimum radius of 0.04 inches, and exposed corners to a minimum of 0.5 inches? if not rounded, are they protected by rubber, fiber or plastic?

- 6. General Electrical Hazards are wires routed so that removal of a plug or connector will not expose "hot" leads? Are tools and test leads adequately insulated? Are plugs and receptacles designed to preclude the insertion of a plug or one voltage into the receptacle of another voltage? Are all external parts (except antennas and transmission lines) grounded? Do electrical hand-tools have three-wire power cords or double insulation?
- 7. Mechanical Hazards are guards provided on all moving parts of machinery including pulleys, belts, gears, blades, etc., on which personnel may become injured or entangled? Are all mechanical components with heavy springs designed so the spring cannot come loose? Is adequate clearance for fingers provided in the design of telescoping steps or ladders?
- 8. <u>Toxic Hazards</u> are personnel exposed to toxic hazards in excess of established threshold limit values?

CHECKLIST S - FAA-G-2100/1b SAFETY REQUIREMENTS

- 1. <u>Line-input Terminals</u> do all ac line-input terminals (120V ac or higher) have covers, barriers or guards?
- 2. <u>Interlocks</u> are interlocks provided for all voltages of 150V or higher which would otherwise be accessible while primary doors, covers, or shields are removed? Are assemblies or chassis at voltages of 500V and higher completely enclosed and separately interlocked?
- 3. Interlock Switches are interlock switches normally open, momentary on, with a manual latch for on position? Does the switch automatically return to momentary-on upon reclosing the cover? (Cutler-Hammer Part 8909, Type Kl28, DPST, 6A/250V, 12A/125V; Cutler-Hammer #91820X1F1, DPST, 10A/250V, 15A/125V; or equiv.) Are interlock bypass switches provided? (A combination interlock/bypass switch may be used.)

- 4. X-RAY is x-radiation from high power tubes, radars, transmitters, CRT's, kept within the exposure limit of 2 mil-roentgens per hour through the use of shields, interlocks, etc?
- 5. <u>Discharging Devices</u> are automatic protective methods and/or devices provided to discharge high voltage circuits and capacitors to 30 volts or less, within 2 seconds after power is removed or an interlock opened?
- 6. Cathode Ray Tubes are provisions incorporated to protect personnel from CRT implosion? (safety glass, laminated face plates, reinforecement, warning signs.)
- 7. Radioactive Material have radioactive luminescent markings and paints been prohibited?
- 8. Warning Signs are all contacts, terminals, parts, etc., having voltages in excess of 500 volts clearly marked? Are exposed dangerous rotating and reciprocating mechanical parts provided with warning signs? Are the signs located conspicuously, and as close as possible to the point of danger?
- 9. Test Points & Controls are test points and controls located so as to preclude accidental shock? (In no case shall they be located in compartments with voltage points of 500 volts or higher.)
- 10. Noise Levels are the noise levels generated by the equipment within the limits specified in paragraph 1-3.5.11 of FAA-G-2100/lb?

CHECKLIST T - FAA-G-2100/1b GROUNDING REQUIREMENTS

- 1. Grounding Practices are at least four separate grounding networks, each isolated from each other, provided? (AC ground, chassis/cabinet ground, signal ground, trunk circuit ground.)
- 2. Power Supply Returns are metallic circuits (wires) used for power supply returns? Are power supply returns as close as physically possible to the "hot" wire to reduce ground loops? Are power supply outputs isolated from each other? Are common returns avoided?

- 3. Single Point Grounding where electronic loads are referenced to ground, are power supply outputs left ungrounded so that reference to ground is at the load termination only? (For multiple loads ground only once at the point of maximum use.) Are d.c. distribution systems grounded only at the source (generator) with ungrounded return circuits provided for all distribution?
- 4. Shielded Wire are outer conductors of shielded wire avoided as signal or power returns?
- 5. Ground Impedance is the ground impedance between any two points within a cabinet kept below one milli-ohm?
- 6. Splices & Connectors are splices in copper ground busses either welded or brazed? (Bolted bus splices are not be be solely relied on.) In making ground connections, is the joining of dissimilar metals avoided? Is adequate environmental protection provided to minimize accelerated joint corrosion?
- 7. RF Grounds are copper sheets or straps used for R.F. grounds? (Braided or stranded conductor shall not be used.) To minimize RF impedance, are the ground conductors kept as short as is physically possible?
- 8. Cabinet Bus are all chassis, nests, racks, panels and cabinet subassemblies positively grounded to the cabinet bus with a minimum wire size of AWG #16?
- 9. Primary Power are the grounding systems for primary power kept separate from equipment ground systems? (A single point reference of the two ground systems is permissible.)
- 10. <u>Building Structures</u> is the equipment grounding system kept isolated from building structures except for bonding at one point only? (Where metal frames or enclosures require grounding for safety reasons, direct equipment ground connections to building structures are permitted.)

- 11. Conduits are conduits properly bonded to the equipment services by either bond strap or brazing, etc.?
- 12. Air Ducts are all air ducts (and sections) electrically bonded to building ground?
- 13. Cable Trays are all cable trays bonded to an appropriate ground by either bond strap, welding, brazing, etc.?
- 14. Machinery is all rotating machinery (including electric motors, generators, fans, etc.) properly grounded with the necessary precautions taken to reduce interference.
- 15. <u>Unit Frames</u> does the unit frame ground system provide only a single path back to architectural ground for all points in each subsystem?

HUMAN FACTORS ENGINEERING EQUIPMENT/UNIT CHECKLISTS

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EQUIPMENT MLS AZ & EL	SHELTER	Elec. Shelter	CABINET Elec. Cab.
UNIT TWT AMP PANEL	EVALUATOR	Mihm	DATE 7/21/77

CHECKLIST	FACTOR														
CHECKLIST	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
A	1	1	1	1	1	N	1	N	1						
В	✓	1	1	С	1	1	>	1	1	1	N	1	1	1	✓
С	1	1	N	1	N	1	1	N	N	С	N	1	1	N	
מ	N	N	N	N	N	N	N	N	N	N					
E	N	N	N	N	N	N	N	N	N	N	N	N	N	N	
F	1	N	N	N	N	N	N	N	N	N	N	N	N	N	N
G	1	/	1.	1	N	N	1	N	N	N	N	1	1	N	
Н	1	1	1	1	1	1	1	1							

1	(√- SATISFACTORY; C - REFER TO COM	MENTS; N - NOT APPLICABLE)
CHECKLIST ITEM	COMMENTS	RECOMMENDATIONS
B4 & C10	Except for the two fault lights, it is obvious when the light is inoperable since the lights are related to an operational control. The fault light indications are remoted to the back of the unit allowing for future remoting to the maint. mon. panel.	Remote the fault indications to the maint. mon. panel for redundancy.
	C-82	

EQUIP	MENT !	MLS AZ 8	EL	SHELTER	Elec. Shelter	CABINET	T Elec. Cab.	
IINTT	Local	Cntrl/S	Status	Panel VALUATOR	Mihm	ከልጥድ .	7/22/77	

CHECKITET	FACTOR														
CHECKLIST	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
A	\	1	1	1	1	. 1	✓	1	1						
В	✓	1	1	1	1	1	1	✓	1	1	N	1	1	1	1
С	1	1	N	1	N	1	1	N	N	1	N	1	1	N	
D	1	N	N	✓	N	N	N	N	N	N					
E	N	N	N	N	N	N	N	N	N	N	N	N	N	N	
F	1	1	1	1	N.	N	1	1	N	N	✓	1	1	N	1
G	✓	✓	1.	1	1	N	1	1	N	1	N	✓	1	N	
Н	1.	1	1	1	1	1	1	1							

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HECKLIST ITEM	COMMENTS	RECOMMENDATIONS
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C-83

HUMAN FACTORS ENGINEERING FACILITY-SHELTER-WORK STATION CHECKLIST

		SHELTER Elec.	Shelter	CABINET AREA	All
	Basic Narrow	Outh		- · 7 /2	·
EVALUATOR	_ Mihm			DATE _ 7/2	.3/11

CHECKION						FAC	TOR					
CHECKLIST	1	2	3	4	5	6	7	8	9	10	11	12
I	✓	1	N	1	1	1	1					
J	>	✓	С	1	С	С	N	Ŋ	N	N	N	/_
K	N	N	N	N	N	N	N	N				
. L	1	N	1	1	1	N	N	N	N	N	N	N
M	>	1	1	1	1	1	1	N	N	N	N	
N	N	N	N	N								
0	✓	1	N	.1	1	1	1	N	N			

($\sqrt{-}$ SATISFACTORY; C - REFER TO COMMENTS; N - NOT APPLICABLE)

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CHECKLIST ITEM	COMMENTS	RECOMMENDATIONS					
J3	Only 3.1' have been provided for work area depth in the Basic Narrow Shelter instead of the recommended 3.5'.	No recommendations. The required shelter dimensions necessitate this exception. Also, the deviation is slight.					
J5-J6	Pwr supply panels, containing a minimum of lights and toggle controls are lower than 41" off the floor. This has been covered on checklist item B9 and C4 of the power supply panel layout checklist						
	C-84						

EQUIPMENT MLS AZ & EL	SHELTER	Elec. Shelter	CABINE	Elec. Cab.
UNIT Power Supply Panel	EVALUATOR	Mihm	ከልጥዮ	7/25/77

CHECKLIST							FAC	TOR							
CHECKLIST	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
A	→	1	1	1	1	✓	✓	1	1						
В	V	1	1	1	1	1	✓	1	С	1	N	1	1	1	1
C	1	1	1	С	N	1	1	N	N	N	1	1	✓	N	
ם	N	N	N	N	N	N	N	N	N	N					
E	N	N	N	N	N	N	N	N	N	N	N	N	N	N	
F	N	N	N	N	N	N	N	N	N	N	N	N	N	N	N
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Н	1	1	1	1	1	1	1	1							

· <u>L</u>	(√- SATISFACTORY; C - REFER TO COMMENTS; N - NOT APPLICA											
CHECKLIST	COMMENTS	RECOMME NDATIONS										
B9 & C4	The panel is located close to the floor and display is therefore >45° from line of sight. This is necessary since this chassis is heavy. Also, the quantity of controls and indicators is minimum on this panel. Lamp type indicators (no meters) only, are on this panel. This configuration is SOP for power supply panels.	This configuration is satisfactory and therefore no recommendations are in order. (Note that those panels containing the greatest quantity of controls and indicators are around eye level.)										

C-85

EQUIE	MENT MLS A	Z & EL	SHELTER	Elec. Shelter	CABINET	Elec. Cab.
IINIT	Maint. Mon	. Panel	EVALUATOR	Mihm	DATE	7/25/77

CHECKLIST		FACTOR														
CHECKLIST	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	
A	1	1	1	1	1	N	N	N	N							
В	1	1	1	1	1	1	1	1	1	1	N	1	N	1	1	
С	1	1	N	1	N	1	1	N	N	1	N	1	1	N		
מ	N	N	N	N	N	N	N	N	N	N						
E	N	N	N	N	N	N	N	N	N	N	N	N	N	N		
·	N	N	N	N	N	N	N	N	N	N	N	N	N	N	N	
G	1	N	1.	1	1	N	1	N	N	N	N	✓	✓	N		
H	1	1	1	1	1	1	1	С								

(\sqrt{satisfactory}; C - REFER TO COMMENTS: N - NOT APPLICABLE)

CHECKLIST	COMMENTS	RECOMMENDATIONS
н8	There are up to four levels of labeling. Due to this fact and the quantity of labels on this panel, it is impossible to comply with the size gradation rqmt. and at the same time make all labels large enough. This is not considered critical due to the non-critical nature of this panel.	This is an acceptable deviation.

EQUIPMENT MLS AZ & EL	SHELTER Elec. Shelter	CABINET Elec. Cab.
UNIT MON. PWR. SUPP. PANEL	EVALUATOR Mihm	DATE 7/25/77

CHECKLIST							FAC	TOR			•				
CHECKIESI	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
A	>	✓	1	1	1	N	. 1	1	1						
В	1	1	1	1	1	✓	✓	1	1	✓	N	1	N	1	1
С	✓	1	1	1	N	1	1	N	N	N	1	1	1	N	
D	N	N	N	N	N	N	N	N	N	N					
E	N	N	N	N	N	N	N	N	N	N	N	N	N	N	
F	N	N	N	N	N	N	N	N	N	N	N	N	N	N	N
G	1	N	1	1	1	N	1	N	N	N	N	1	N	N	
н	1	1	1	1	1	1	1	1							

(- SATISFACTORY; C - REFER TO COMMENTS; N - NOT APPLICABLE)

CHECKLIST ITEM	COMMENTS	RECOMMENDATIONS
		·
		·
		·
	C-87	

HUMAN FACTORS ENGINEERING EQUIPMENT/UNIT CHECKLISTS

EQ	UIPMENT ML	S AZ	&]	EL		S	HEL	rer :	Elec	. Sh	elte	er	C	ABIN	ET _	Elec	. Ca	b.
UN	IT All D	rawe	rs			_	EVA	LUA:	ror .	Mi	hm				DAT	E	/26/	77
									FAC	TOR								
•	CHECKLIST	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
	P	N	N	1	1	1	N	1	1	1	1	1	1	1	1	1	1	
	Q	1	✓	1	1	1	1											
	R	1	1	1	1	1	1	N	1									
	S	✓	1	1	1	✓	N	N	1	1	1							
	T	1	1	1	1	1	1	1	1	1	1	.1	N	N	N	1		

					Ľ		<u>L'</u>	M	I N										
-	T	•	1	1	/	1	1	1	✓	1	✓	1	1	N	N	N	1		
		(√.	- SAT	MSF.	CTO	RY;	C - R	EFE	R TO	COM	MEN	TS; I	N - N	OT A	PPL	CAB	LE)		
CHEC	KLIST EM				CO	MME	NTS							REC	OMM	END	ATIC	ons	
													•						
																			•
	}																		
											1					•			
	Ì																		,
																		•	
	-															٠			•.
									C-8	8						•			

EQUIPA	MENT MLS AZ & EL	SHELTER	Elec. Shelter	CABINET	Elec. Cab.
IINTT.	RF UNIT PANEL	TO STATE AT ATT ATT	Mihm	DAME	7/27/77

CHECKLIST							FAC	TOR			•				
CHECKLIST	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
٨	✓	1	1	1	✓	1	1	1	1						
В	N	N	N	N	N	N	N	N	N	N	N	N	N	N	N
С	N	N	N	N	N	N	N	N	N	N	N	N	N	N	
מ	N	N	N	N	N	N	N	N	N	N					
E	N	N	N	N	N	N	N	N	N	N	N	N	N	N	
F	N	N	N	N	N	N	N	N	N	N	N	N	N	N	N
G	1	N	√ .	1	N	N	1	N	N	1	N	N	N	N	
H	1	1	1	1	1	1	1	1							

(√- SATISFACTORY; C - REFER TO COMMENTS; N - NOT APPLICABLE)

CHECKLIST ITEM	COMMENTS	RECOMMENDATIONS
	•	

EQUIPMENT MLS AZ & EL	SHELTER Antenna Case	CABINET
TINT MAINT. PANEL	EVALUATOR Mihm	DATE

CHECKIET							FAC	TOR							
CHECKLIST	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
٨	√ .	1	1	1	N	1	1	1	1						
В	1	1	1	1	1	1	1	1	1	1	N	1	N	1	1
С	1	1	N	N	N	1	1	N	N	1	N	1	N	N	
מ	1	1	1	1	N	1	✓	N	1	N					
E	N	N	N	N	N	Ŋ	N	N	N	N	N	N	N	N	
F	N	N	N	N	N	N	N	N	N	N	N	N	N	N	N
G	1	1	1	1	1	N	1	1	N	1	N	1	N	N	
H	1	1	1	1	1	1	1	N							

(√- SATISFACTORY; C - REFER TO COMMENTS; N - NOT APPLICABLE)

CHECKLIST		
ITEM	COMMENTS	RECOMMENDATIONS

HUMAN FACTORS ENGINEERING FACILITY-SHELTER-WORK STATION CHECKLIST

EVALUATO	R Mihm		SHELTER ANTENNA CASE CABINET AREA												
	· · · · · · · · · · · · · · · · · · ·	<u> </u>	FACTOR												
	CHECKLIST	1	2	3	4	5	6	7	8	9	10	11	12		
	I	1	✓	1	1	1	✓	1							
	J	1	N	1	1	1	1	N	N	N	N	N	N		
	K	N	N	N	N	N	N	N	N						
	L	N	И	N	N	N	N	N	N	N	N	1	/		
	M	N	N	N	N	N	N	N	N	N	N	N			
	N	N	N	N	N										
	0	N	С	N	N	N	N	N	V	N					
	(√- SATISFAC	TOR	Y; C	- RE	FER	то	OMA	ÆNI	S; N	- NO	T AP	PLIC	ABLE)		
CKLIST TEM		сом	MEN	TS						R	ECO	MME:	MOITADM		
02	No fire extirenclosure. The fire hazard senter this should be shown in the fire extinction of the fire hazard senter this should be shown in the fire extinction.	her.	e is e pe	no	pers	sonn	-1	No	reco	omme	ndat	ion.			

HUMAN FACTORS ENGINEERING EQUIPMENT/UNIT CHECKLISTS

EQUIPMENT MLS AZ & EL SHELTER ANTEN							ENNA	CAS	E	C.	ABIN	ET _		<u> </u>					
UNIT										Mihm DATI					E				
	FACT						TOR												
	CHECKLIST	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	
	P	✓	N	1	√ .	✓	N	1	1	✓	1	1	1	1	1	1	1	1	
	Q	>	1	1	1	1	1												
	R	1	1	N	1	1	1	N	✓										
	S	1	1	N	N	N	N	N	N	✓	N								
•	T	✓	1	1	1	1	1	1	✓	✓	1	1	N	N	N	1			
	(√.	- SAT	TSF.A	CTO	RY;	C - R	EFE	R TO	COM	MEN	TS; 1	1 - N	OT A	PPLI	CAB	LE)			
	KLIST EM			CO	MME	NTS							REC	ОММ	ENDA	ATIO	NS		
															_				
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																,			
		•													_		•		
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APPENDIX D

MAINTAINABILITY

PLAN

FOR

MLS

GROUND SYSTEM

Prepared by

The Bendix Corporation Communications Division Towson, Maryland 21204

November 1977

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MAINTAINABILITY DEMONSTRATION PLAN FOR THE

MLS GROUND SUBSYSTEM

D.1 SCOPE

This document describes the test procedure that will be implemented to demonstrate that the MLS Ground Subsystem is designed to meet a mean-time-to-repair (MTTR) of no greater than 0.5 hours, as specified in Table 11-6B of FAA-ER-700-07. The test procedure conforms to MIL-STD-471A, Test Method 9, for mean-corrective-maintenance-time (μ_{C}) . The level of repair which will be demonstrated is the restoration of ground sub-system operation at the organization level of maintenance, accomplished through the replacement of line replaceable units (LRU's). Fault isolation and diagnostics are performed to a major degree using the existing monitoring circuitry and built-in-test-equipment.

D.2 APPLICABLE DOCUMENTS

The following documents of the issue in effect on the date of the contract, form a part of this test plan to the extent specified herein.

D.2.1 Standards

MIL-STD-280 Definitions of Item Levels
MIL-STD-470 Maintainability Program Requirements
MIL-STD-471 Maintainability Demonstration
MIL-STC-721 Definitions of Effectiveness Terms

D.2.2 Handbooks

MIL-HDBK-472 Maintainability Prediction

D.2.3 Other

Contract No. DOT FA72WA-2801

FAA-ER-700-07, Amendment 1, 2/25/75, revised 3/26/75.

MLS Functional Requirements Specification

MLS-RM-001-IN, 11/12/75 - Reliability and Maintainability
Predictions for Basic (Narrow) and Small
Community Ground Subsystems.

D.3 GENERAL TEST REQUIREMENTS

D.3.1 Description of the Equipment to be Tested

The Maintainability Test will be performed on a complete MLS Phase III Basic Narrow System, less the DME equipment. Both Azimuth and Elevation subsystems will be included.

D.3.2 Demonstration Site

The maintainability demonstration will be performed at the Bendix Communications Division facility in Towson, Maryland.

D.3.3 Number and Skill Level of Repair Personnel

All maintenance tasks can be performed with one technician. The technician assigned to the demonstration will have a skill level, in Bendix's opinion, equivalent to an FAA Technician.

D.3.4 Demonstration Test Team

A demonstration test team will be organized and assembled to assure appropriate representation of FAA and Bendix personnel for accomplishing the maintainability demonstration. A Bendix test conductor will be responsible for all test activities including the supervision of those technicians involved in the insertion of simulated failures as well as those involved in performing the maintenance tasks, timing and recording the data.

D.3.5 Task Selection Method

The sample size of 200 tasks has been derived in accordance with the procedure outlined in Appendix A of MIL-STD-471A. Appendix A provides specific procedures for assuring that the corrective maintenance (CM) tasks to be used in the demonstration constitute a representative sample of the total population of CM tasks. Of the 200 tasks identified, 50 will be selected at random by the FAA representative to be used in the demonstration.

Based on the procedures of Appendix A of MIL-STD-471A, a table has been constructed which gives the distribution of tasks

resulting from the sample size analyses. This table, which may be found in Supplement 1, contains items which are grouped by module in accordance with the level of maintenance to be demonstrated. The number of tasks assigned to each item was allocated by predicted frequency of occurrence; that is, percent contribution to the overall failure rate of the unit under demonstration.

Also given in Supplement 1 is the method which will be used to randomly select the 50 demonstration tasks.

D.3.6 Data Acquisition

During the Maintainability demonstration test, a data collection method will be implemented to measure and record the elapsed time required to repair each simulated fault. The format presented in Figure D.7-2 will be used to record in minutes the time required for such specific task elements as fault location, fault correction (module removal and replacement), and final adjustment, checkout and reassembly. Supply and administrative delay time and servicing time will be excluded from all calculations of maintenance downtime.

D.3.7 Analysis of Data and Method of Scoring

Following the completion of the 50 sample tasks, mean downtime of the sample (\bar{x}_c) will be calculated in accordance with Test Method 9 of Appendix B in MIL-STD-471A.

Data analysis will include all of the tasks which were randomly selected and performed from the Task Identification and Location Table found in Supplement 1.

Accept/reject criteria will be computed for the specified value of MTTR at a 10% consumer's risk using the following test: $_{\rm N}$

a) Mean of Sample
$$(\overline{x}_C) = i \frac{\sum_{i=1}^{\infty} X_{Ci}}{N_C}$$

b) Accept if MTTR_{specified}
$$\geq \overline{X}_{C} + \frac{g\sigma}{\sqrt{N_{C}}}$$

Reject if MTTR_{specified} $< \overline{X}_{C} + \frac{g\sigma}{\sqrt{N_{C}}}$

where σ = standard deviation of sample of corrective maintenance tasks

 $\emptyset = 1.28$ (consumer's risk (β) - 10%)

 $N_c = 50$ (number of demonstrated tasks)

D.4 TEST PROCEDURES

D.4.1 Periodic Checks

Prior to the insertion of each fault to be simulated, the equipment involved will be checked to assure that no real fault exists. These checks will be as indicated in paragraph D.4.2 below. After fault insertion, the equipment will be rechecked to determine that the malfunction has been properly installed and that no other malfunction exists. In addition, a check will be made after the fault has been removed to be sure that the equipment has been properly restored. Results of each check will be entered, as appropriate, in a General Test Log (See Figure D.7-1).

D.4.2 Check-Out Procedure

D.4.2.1 Unit Level Checks

Checks will be made on individual units prior to the insertion of a fault, and after its removal. These checks will be to simply determine that the unit is functioning properly.

D.4.2.2 Group and Equipment Level Checks

Check of operability of the equipment will be accomplished by reviewing the status lamp indicators on the Remote Control/ Status monitor panel. The following lamp checks will be made:

INDICATOR	MODE
STATUS ON	ОИ
CONTROL REM	ON
CONTROL LOC	OFF
STATUS OFF	OFF
MALF EXEC	OFF
MALF MAINT	OFF
MALF DL	OFF

D.4.2.3 Suggested Troubleshooting Procedures

The person assigned to perform the maintenance during the test will not be given strict procedures for troubleshooting the equipment. Instead, he will be familiarized with the MLS technical manuals prior to testing and during testing he will use these manuals, as needed, to isolate failures and effect the appropriate corrective actions.

D.4.3 Task Selection and Simulation

D.4.3.1 Selection of Tasks

The selection of tasks for the initial sample size of 200 simulations is based on the maintainability analysis referenced in paragraph D.2.3. For this analysis, units are grouped by similar function or nature (e.g., antenna, transmitter, timing, etc.) in accordance with the task selection procedure of Appendix A, MIL-STD-471.

As information regarding the selection and nature of the malfunctions must be concealed from the personnel performing the simulations, the detailed methods of selection and installation of malfunctions are described in Supplement 1 to this Maintainability Demonstration Plan. This Supplement is the Procedure for Fault Installation.

Supplement 1 itemizes the 200 tasks and describes the random methods of selecting the tasks and type of representative malfunctions.

D.4.3.2 Simulation of Failures

Supplement 1 gives the specific methods for simulating and installing failures. The methods to be used will be non-destructive to the equipment. Where several failures are required on the same type of equipment, several different failure modes have been specified. Selection of these modes will be on a random basis.

The procedure which will be followed for installing a malfunction is given below.

The personnel who will perform the maintenance task will be sent from the area. The personnel installing the malfunction will select the task per Attachment 1, and check out the equipment per paragraph D.4.2. The unit will be removed from the rack, if necessary, and the malfunction will be installed. The unit will be closed up, returned to its position and checked to determine that the malfunction is operating as predicted. The Group and Equipment Level checks will then be made to determine that no other fault exists. The required test equipment will then be removed from the circuitry and the equipment will be set in a condition which simulates the flight line checkout conditions.

D.4.3.3 Demonstration of Maintenance Tasks

The level of maintenance to be demonstrated is the repair of the MLS Ground Subsystem at the organizational level by LRU replacement. Demonstration of maintenance tasks will be timed, and will include the time for verifying a failure condition, patching in any necessary test equipment; checking out and localizing the fault to the appropriate LRU; removing and replacing the LRU; adjusting, closing, and final rechecking of the site equipment to be sure that the malfunction has been corrected. For this level of maintenance, failures simulated in case-mounted parts will be repaired by treating the case as a replaceable module.

After the malfunction has been installed, the maintenance personnel will be returned to the area for the start of the timed demonstration.

The appropriate check out procedures as outlined in paragraph D.4.2.3 will be used to localize to the faulty unit. Required auxiliary test equipment and built-in test equipment will be in the area and warmed up if required but will not be patched into the test set-up. In order to assist the maintenance personnel, available handbooks and/or troubleshooting aids (e.g., module identification charts, schematics, test point diagrams, etc.) will be provided.

Repairs will be made by unit, board or module replacement, with faulty items replaced with working spares. Where spares are unavailable, timing of the demonstration will be stopped after removal of the correct item. The test director will have the fault removed and demonstration time will then resume. The LRU will be replaced and the equipment will be adjusted, closed up and checked out. At this time, the demonstration task is completed and the elapsed time and manpower required will be recorded in the appropriate logs.

D.5 REQUIRED SUPPORT EQUIPMENT

The following equipment will be required to operate and support the Maintainability Demonstration. All test equipment will be subject to standard calibration requirements. In addition to the listed equipment, associated cabling and connectors are required.

Stop Watch (2 required)

(To read 60 seconds with one sweep, and record a minimum of 30 minutes.)

Gallet timer or

equivalent

HPG382A

HP435A

Variable Attenuator, RF Power Meter, RF Power Sensor, RF HP8481A
Oscilloscope Tektronix 545B

Dual Trace Amplifier Tektronix 1A2

Detector, RF HP420

Power Divider 4042652-0701

A-C Clamp Volt-Ammeter Weston 749

Coax to Waveguide Adaptors (4) HPG281A Signal Generator HP618B

Variable Attenuator, RF ARRA5804-20W

Phase Shifter HPJ885A

Dummy Load Narda 376NM

Test Probes Tektronix P6006
Assorted Test Cables RG214 and RG223

D.6 FAILURE PROCEDURES

If a real failure occurs, the failed module will be removed and replaced with a working spare. A defect tag will be completed for the failed unit, and it will be subject to the Bendix In-House Failure Analysis and Reporting procedure established for the MLS program. If a spare module is unavailable, the faulty one will be repaired for reuse in the test.

If the failure occurs while a task is in the process of demonstration, the demonstration will be aborted and appropriately logged. The demonstration personnel will leave the area while the radio set is being repaired. After the repair, the personnel will return and continue the task demonstration. Time recording for the task will again begin at this point.

D.7 TEST RECORDS

D.7.1 General Test Log

The General Test Log shown in Figure D.7-1 will provide a complete chronological record of all test activities and/or other actions performed on the equipment during the test period. It will contain a continuing history of equipment operation,

NLS HTTR DEMONSTRATION TEST GENERAL TEST LOG

ENTRY NO.	DATE	TIME	REMARKS (ACTIVITY, DEVIATIONS, INTERRUPTIONS, REPLACEMENTS, ETC. INITIALS
			·
·			
			·

FIGURE D.7-1

malfunctions, repairs, removals, etc. If the entry pertains to the performance of a demonstration task, appropriate columns have been provided to identify the task and record that the malfunction was properly installed.

D.7.2 MTTR Test Scoring Chart

Figure D.7-2 shows the chart on which the maintenance downtime per corrective maintenance task (x_c) for each task will be recorded. There are columns on the chart to measure the following task time segments: fault location, including diagnostic and module isolation activities such as opening unit cases to gain access to test points; module removal and replacement; and final checkout and reassembly. Final checkout and reassembly times include adjustment and calibration time; all of these are collectively incorporated in one column since checks may be made before and after the unit is closed up.

D.7.3 Test Equipment and Facility Logs

The log of Figure D.7-3a will be used to record the types of equipment or facilities used in the test set-ups. When an equipment is removed for replacement, the appropriate data will also be recorded. Calibration and Renewal Data will be recorded in the log shown in Figure D.7-3b by personnel performing the procedure.

MLS MITR DEMONSTRATION TEST SCORING CHART

TASK NO.	LOCALIZE TIME (MIN.)	REMOVE AND REPLACE TIME (MIN.)	FINAL UNIT CHECKOUT TIME (MIN.)	TOTAL RESTORATION TIME
			,	

FIGURE D.7-2

	OF-	
HEET		

MLS MAINTAINABILITY TEST TEST EQUIPMENT AND FACILITY LOG

- NOTES:
 1. ENTER MODEL, SERIAL NUMBER, AND DATE WHEN EQUIPMENTS OR FACILITIES ARE PUT INTO USE.
 2. WHEN EQUIPMENTS OR FACILITIES ARE REPLACED, ENTER THE NEW MODEL, SERIAL NUMBERS, AND THE DATE IN ADJACENT COLUMN.
 3. REFERENCE THE LINE AND COLUMN ON THE GENERAL TEST LOG.

rest sta	RTING DATE:	TES	T PINISH	ING DATE	:		
LINE NO.	EQUIPMENT OR FACILITY	1	2	3	4	5	6
İ						}	
			 - -			 	
-		ł					

FIGURE D.7-3a

TEST EQUIPMENT AND PACILITY CALIBRATION OR RENEWAL LOG MLS MAINTAINABILITY TEST

CALIBRATION OR RENEMAL PERSONNEL WILL ENTER DATE AND INITIALS UPON SATISFACTORY COMPLETION OF APPROPRIATE PROCEDURE. COMPLETE COLUMN 1 BEFORE STARTING COLUMN 2.

TESTING START DATE: TESTING FINISH DATE:

LINE NO.	1	2	3	4	5
				}	
		}			

FIGURE D.7-3b

MAINTAINABILITY

DEMONSTRATION PLAN

SUPPLEMENT 1

FAULT INSTALLATION PROCEDURE

FOR

MLS

GROUND SUBSYSTEM

Contract No.
DOT FA72WA-2801

Prepared by
The Bendix Corporation
Communication Division
Towson, Maryland 21204

November 1977

FAULT INSTALLATION PROCEDURE

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1.0 SCOPE

This document describes the procedure that will be used for the random selection of tasks to be demonstrated during the Maintainability test of the MLS Ground Subsystem. It further describes the methods for selecting specific malfunctions for each task. In addition, this attachment provides the procedures which will be used by the personnel installing the malfunctions to simulate faults in the equipment.

To maintain test integrity, the information contained in this document will be restricted and inaccessible to the personnel performing the task demonstrations.

2.0 REFERENCED DOCUMENTS

The following documents, of the issue in effect on the date of the contract, form a part of this procedure to the extent specified herein.

Maintainability Demonstration Plan for MLS Ground Subsystems

Reliability and Maintainability
Predictions for Basic (Narrow) and
Small Community Ground Subsystems

MIL-STD-471A

Maintainability Demonstration

Tables for Statisticians, Herbert Arkin and Raymond Colton, Barnes & Noble, 1963

3.0 SELECTION OF TASKS

A demonstration population of 200 corrective maintenance tasks for the MLS ground subsystem has been prepared in accordance with the Task Sampling Method given in Appendix A of MIL-STD-471A.

Table 1 gives the distribution of these tasks among the various replacement items. In constructing the table, the individual replaceable items were grouped by the major units (antenna, transmitter, timing, etc.) which comprise the equipment

Table 1. Corrective Maintenance Task Stratification

3	e	5	3	25	3	6	g	€	900	919
MA TR	BUNCTIONAL LEVEL	MAING	FST	EAITHOR	È	TASK	TOTAL	PETATIVE	DCMOR	DCM74
UNNTS	6	TASK	MAIN	RATE	AZ 6	GROUPING	FAILURE	E CO	POPULATION	SWAPE
	MAINTENANCE		TIME (MIN.)	FAOF HRS	ᇜ		RATE		ALLOCATION	SIZE
TWT AMP	TWT AMP	RR W	19	61.33	~	GRP. 1, TASK A	122.666	21.0	Z	1
RF UNNIT	DICITER	3 8 8	=	=	~	GRP. 2, TASK S	3	500	V-6.)	_
	57X	8/R 68)	-	2,965	~	A, B, C, D			71 \ 1-8	~
	AMPLIT. MODULATOR	3	=	19.110	~				_	
	DETECTOR AMP.	2 2	= 1	3 5	~ .		1		7 9	`
	CHASSIS FARIS	1 L	2	3	•	UKF. 3, IASK t	2	T T	9	•
LOCAL COMPROLISTATUS	SYSTEM SYNC	RR S	<u>=</u>	- 26	~	- A	E. 43	0.03	V-1)	
	DATA LINK	RAR GE	=	3,30	~	TASK, A-P			1-5	
	AUX DATALINK	SAR (C)	•	3.137	<u> </u>				- -	
	VARIABLE ALIX DATA	RR C)	<u>-</u>	3.174	_					
	FIXED AUX 2	R.R. E.	=	4.115	_					
	FIXED AUX 1	R.R. F.	<u>•</u>	4.115	_				Ξ	
	AUX / DS/MY	RAR (C)	=	2.35	_				6-1 / 1-9	
	AUX /AD/PAR	R. E.	<u>=</u>	50.7	_				_	`
	MORSE CODE	R/R (3)	<u>=</u>	2.58	_					_
	ID/BD/DPSK	RAR (D	<u>=</u>	7.886	~					
	SYS TUME GEN	RÆ CK)	=	3.88%	~				K-2	
	TIME CONTROL	8.8 5.0	=	£34	~				Ξ	
	10 MMtz DR IVER	R/R #	±	90.0	~				? X	
	10 MHz OSC	2. A. C.O	2	200	~					
	SEPITIMER	2 W CO	<u> </u>	3.23	~				2	
	LT DR.ML	RA G	•	2.2	7				-i-	_
	LCAST. TND	æ	R	2,000	~	GRP. 5, TASK Q	8	8	,-	•
		eg agn								
	RIM	2 W SE	Я	23.000	~	GRP. 6, TASK R	000 72	000	•	-
	CHASSIS PARTS	RP IS	2	5.53%	7	GRP. 7, TASK S	3	0.43	~	_
POWER SUPPLY DRWR	20 V PWR SUPPLY	3 8 8	2	200	~	GRP. 8	5.70	0.00	_	
	15 V PWR SUPPLY	R /R (B)	2	3	~	TASKS A, B, C				•
	S V PWR SUPPLY	RAR (C)	2	0.677	~				_	
	CHASSIS PARTS	8 E	e	2.006	~	CRP. 9, TASK D	4 012	8	_	•
				1		A			7	

Table 1. Corrective Maintenance Task Stratification (Cont)

8	8	6	3	63	3	6	8	ε	100	â
MAJOR	FUNCTIONAL LEVEL	MAINT	EST	FAILURE	Ě	TASK	TOTAL	RELATIVE	DEMON	DEMON
UNITS	5	TASK	MAIN	RATE	7 ZV	GROUPING	FAILURE	FREQ	POPULATION	SAMPLE
	MAINTENANCE		TIME (MIN.)	FAOO HRS	7		RATE		ALLOCATION	SIZE
MAINT MONITOR DRWR	EXECUTIVE INTEG	R/R (A.)	61	72.7	8	GRP, 10	209 602	0.242	(1-V	_
	MON. CMTRL	R/R (B)	62	1.671	7	TASKS A- T			1-9	
	MORSE CODE	R.R. (C)	2	2.865	_					
	DPSK DECODE	R.R. (D)	2	1.83	~				1-0	
	DPSK DECIDE	R/R (E)	61	4.234	7				£-2	
	DISC. DATA	R/R (F)	2	1.373	~				5	
	AN COMP. #3	(S) X/X	2	3.671	~				C-5	
	AN COMP. 12	2 % E	61	3.479	~				H-2	
	AU/AD/PAR	883	<u> </u>	2.733	_				Ξ	
	10/80/0PSK	2 KK C)	2	2886	~				=	
	SYS TIME GEN	R.R. (K)	61	4.34	~				K-2 > 48	~
	MON. TIME	RRC	\$	3,334	~				1-5	
	SCAN TIME	R/R (M)	19	17.731	~				*-¥	
	AN COMP. II	S & S	61	3.546	~				N-2	
	DETICOMP	R/R (0)	61	1.420	~				7-0	
	BEAM ACCUR.	R/R (P)	61	6.238	~	_			P-3	
	DIG. COMP.	R/R (Q	62	11.556	~				0-5	
	FREQ. MON.	R/R (R)	16	5.320	~				R-2	
	TIMING REFERENCE	RAR (S)	61	1.264					Q-S	
	MAINT INTEG.	2	61	3.889	•				1-5	_
	MAINT MON. INDIC.	R.R	8	8.400	2	GRP. 11, TASK U	16.800	0.019	-	_
		12 G3								
	CHASSIS PARTS	& &	8	3.268	~	GRP. 12, TASK V	6.536	3.007	-	0
MON. PWR SUPPLY DRWR	MONITOR RCVR	R/R /A)	2	40.611	2	GRP. 13, TASKS	292 297	6.100	A-18	
	S V PWR SUPPLY	RAR (B)	2	0.671	<u> </u>	A, B, C			8-1 \ 38	~
	15 V PWR SUPPLY	R.R. (C)	2	1.438	~					
	CHASSIS PARTS	RP (0)	2	5.680•	7	GRP. 14, TASK 0	11.360	0.013		~
COOLING FAN DRWR	CHASSIS PARTS	æ ₹	2	\$.00.9	~	GRP. 15, TASK A	12.010	0.014	•	

Corrective Maintenance Task Stratification (Cont) Table 1.

												_			_					_		_					_			\Box
8	DEMON	SIZE		-	-	_	_	· -	· -		_		_	-	•		•	,		س			` `	_		~		_	-	Я
-	3	TION		2		٠		:	2					~	_			-			7					•			3	82
1010	DEMON	ALLOCATION	L11-Y	~	3	V-7	~ 6	3 2	_ []	<u>-</u>	3	Ŧ	_ _						7		~ ::	35	•	(0- V	8-3	~	2-0	:3		
(6)	RELATIVE	נשנה	8/0.0			0.060								0.013	0.00			8	0.00					%					0.015	1.00
9	TOTAL	RATE	67.576			51. 680								10. 872	7,052			0.164	7. 906				95	60.00					13.370	864.876
	9	2	SKS				_		_	_				ASK J		ာ (၁		ASK D		w l			ASK F		u.				ASK F	
E	TASK	5	GRP. 16, TASKS	A, B, C		GRP. 18	TASKS A- I							GRP. 18, TASK	GRP. 19.	TASKS A, B, C		GRP. 20, TASK D	GRP. 21,	TASKS A-			CRP 27 TASK F		TASKS A-F				GRP. 24, TASK F	
3	€:	² 교	R		~	~	~	~		°	~	_	~	~	~	~	~	~	~	~	~	~ (, ,		` ^	-		. ~	. ~	П
ŝ	FAILURE	FAO HRS	2.30	8. 84L	1.137	\$	2.621	₹ 520	2.42	3.672	2 920	2.870	2.641	5.436	0. 679	0.627	0.720	0.083 0.093	1.10	0.629	3	0.362	2 2 2	24.0	• 700	36		ķ	. £	
3	EST.	TIME (MIN.)	R	8	2	ส	R	R	ล	8.8	2 8	8	R	3	2	2	2	3	я	8	R	R	2 3	3 8	2 8	2 8	2 8	2 8	2 2	
6	MAINT	YCY	R/R (A)	R./R (8)	RAR (C)	38.8	R/R (B)	R.R. (C)	8 6	8/8 60 60 60 60 60 60 60 60 60 60 60 60 60	(3) 8/8	R/R (H)	R.A.	RP (J)	R. S.	R.AR (B)	RAR (C)	8P (5)	R.R. (A)	R/R (B)	R/R (C)	R/R (D)			Z 6	0 8 8 9 0 5 9 9	2 6 6	E A CO (C)	E &	
S	FUNCTIONAL LEVEL	MAINTENANCE	SCAN SWITCH	SCAN MODULATOR	ANT. SEL. SW.	SCAN CMTRL	SCAN CNTR COMP	SCAN CNTR MON	SCAN SW DRIVE	S. S. DRIVE INT.	S S MON EXP	S S MON INT.	10 MHz 05C	CHASSIS PARTS	5 V PWR SUPPLY	24 V PWR SUPPLY	40 V PWR SUPPLY	CHASSIS PARTS	RF DETECTOR	BAND FILTER	PWR DIVIDER	VIDEO AMP	C. 20. 30. 30. 30. 30. 30. 30. 30. 30. 30. 3	ANT MON WINCO AND	AMI. MON. VIDEO ANT S	Lra ac. 1	7.04.60		PWR DISTRIB.	
a	MAJOR	STIMO	ALFERMIA			DEAM STERING								-	SHIPPIIFS				MONITOR HORN ASSY						MISCELLANEOUS					

level for which the demonstration is being conducted. Failure rates for each of the boards/modules were derived from the reliability prediction. Column 9 of Table 1 gives the relative frequency of occurrence of each of the maintenance tasks (or a percentage of the item failure rate to the total failure rate). These relative frequencies are then used to allocate the population of 200 tasks (column 10) among each of the maintenance tasks identified in columns 3 and 7. Column 11 presents the demonstration sample size of 50 tasks, from the population of 200 tasks, which have been allocated to each task group by relative frequency.

4.0 SELECTION OF MALFUNCTIONS

4.1 General Philosophy

The methods which will be used to simulate malfunctions were selected on the general basis of causing no electrical or mechanical damage or degradation to the equipment with respect to workmanship, overstress, or disruption of critical alignments or adjustments.

Applicable methods will include disconnecting leads from terminal pins and/or internal circuit elements, installing jumper wires, using faulty parts in place of good ones, adding certain parts to simulate faults, and misadjusting non-critical internal controls.

Disconnecting leads or attaching jumpers will be done internal to the LRU, where practical. For those tasks where internal simulation of a malfunction is impractical, the malfunction will be installed externally in a manner which will minimize the possibility of visual clues, e.g., from the back of the rack, or in the inter-connecting cabling. This procedure will correctly simulate a malfunction which would be internal to the box through isolation to the faulty unit, removal and replacement, up to rechecking the unit. At this time, the malfunction would be corrected if it were internal and the succeeding checkout would be favorable. To simulate this

condition, the following procedure will be adopted. The task will be conducted normally up to the point where the faulty unit has been isolated and removed. Time recording will then stop and the external fault will be repaired. Time recording will then resume for the replacement and checkout portions of the task. This procedure will accurately simulate the time required to perform the maintenance task.

4.2 Malfunction Installation Guide

Table 2 lists the specific malfunctions which will be installed in the various boards/modules. The table gives the symptom to be simulated, a description of the simulated failure and the method for simulating the symptom.

Where more than one task is to be demonstrated on a given board, several modes of failure are given to provide a variety of malfunctions. In selecting the various symptoms, consideration was given to typical modes of failure and comparative complexity of various functions within the module.

5.0 APPLICABILITY OF TASK DATA

The last column of Table 2 shows identifying task numbers for the two hundred malfunctions. To randomly select the task sequence for the 50 tasks to be demonstrated, chits will be prepared, one for each of the 200 task numbers. At the time of the demonstration, the chits will be placed in a container and mixed. At the start of each task demonstration, a chit will be drawn from the container, lottery fashion, and that task will be demonstrated.

As the test proceeds, a tally will be maintained of the demonstration sample, so that the number of tasks demonstrated for each individual maintenance task identified in column 3 of Table 1 does not exceed the sample size allocated to that task, as given in column 11 of the same table (as noted in paragraph

A.10.4.J of MIL-STD-471A). With this method of selection, the sequence in which the tasks are demonstrated is selected randomly while the appropriate weighting by frequency of occurrence is preserved.

TABLE 2. MALPUNCTION INSTALLATION GUIDE

MAJOR UNIT	MAINTENANCE LEVEL	SYMPTOM NO.	MOTAMYS	METHOD OF INSTALLATION	COMPITIONS OR NOTES	DENT.
TWT AMP	TWT AMP	7	NO LIGHTS ILLUMINATED ON TWT. SYSTEM SHUTDOWN. ERP AND/OR TWT MONITOR LIGHTS LIGHT (ON MONITOR PANEL).	BLOWN PUSE	BAD FUSE	-
		~	SYSTEM SHUTDOWN, ERP AND/OR TWT MONITOR LIGHTS LIGHT ON MONITOR PANEL	DISCONNECT COAX PROM TWT INPUT. (INSIDE TWTA)	SIMULATE BAD TWT INPUT CABLE OR BAD TWT INPUT CONNECTOR	
		м	SYSTEM SHUTDOWN. ERP AND TWT MONITOR LIGHTS LIGHT ON MONITOR PANEL. TWT OVER TEMPERATURE FAULT LIGHT LIGHTS. TWT WON'T RESET.	SHORT THERMO- STAT ON TWT HEAT SINK.	SIMULATE TWT OVER- TEMPERATURE	m
		~	SYSTEM SHUTDOWN. ERP AND/OR TWT MONIOR LIGHTS ON MONITOR PANEL LIGHT. NO INDICATORS ILLUMINATED ON TWT.	DISCONNECT SIMULATE BAD WIRE ON TWY AC AC PUR SWITCH POWER SWITCH	SIMULATE BAD AC PWR SWITCH	*
		v.	SYSTEM SHUTDOWN. TWT WILL NOT GO INTO "OPERATE" MODE (HV WILL NOT TURN ON).	SHORT A2U1-10 TO GND	SINULATE BAD A2U1	٠,
		9	SYSTEM SHUTDOWN. TWT WILL NOT GO INTO "OPERATE" MODE.	SHORT A3U2-7 TO GND	SIMULATE BAD A2U2	9
		^	SYSTEM SHUTDOWN, TWT "HELIX OVER- SHORT AZU3-11 LOAD" LIGHT ILLUMINATED, TWT WILL TO GND NOT GO INTO OPERATE MODE.	SHORT A2U3-11 TO GND	SINULATE BAD A2U3	~
•		6	SYSTEM SHUTDOWN. TWT HAS NORMAL INDICATIONS. (ERP AND/OR TWT LIGHTS ON MONITOR LIT.)	SHORT A2TP2 TO GND	SIMULATE BAD 09	œ
		٥	SYSTEM SHUTDOWN, NO TWT INDICATORS LIT EXCEPT FOR AC POWER.	DISCONNECT JUMPER BETWEEN El AND E2	SIMULATE BAD T1	•
•		01	SYSTEM SHUTDOWN, NO TWT INDICATORS LIT. (TWT AND/OR ERP LIGHTS LIT ON MONITOR PANEL.)	DISCONNECT WIRE FROM INTERLOCK SWITCH SA	SIMULATE BAD INTERLOCK SWITCH	9

TABLE 2. MALPUNCTION INSTALLATION GUIDE

MAJOR UNIT	MAINTENANCE LEVEL	SYMPTOM NO.	MOTAMYS	METHOD OF INSTALLATION	CONDITIONS OR NOTES	IDENT.
(CONT'D)	TWT AMP	11	SYSTEM SHUTDOWN. TWT INDICATORS OFF EXCEPT "AC POWER"	DISCONNECT WIRE FROM + TERMINAL OF RECTIFIER (QUAD) CR1.	SIMULATE BAD RECTIFIER (CR1)	n
		12	SYSTEM SHUTDOWN. TWT INDICATORS OFF EXCEPT AC POWER.	DISCONNECT WIRE BETWEEN ES AND E6.	SIMULATE BAD Q1	77
		13	SYSTEM SHUTDOWN. TWT INDICATORS NORMAL. (MONITOR TWT AND ERP LIGHTS ON.)	DISCONNECT J6 FROM A3.	SIMULATE BAD A3T1	13
		77	SYSTEM SHUTDOWN. TWT INDICATORS OFF EXCEPT AC POWER.	DISCONNECT J5 FROM A3.	SIMULATE BAD	7
		15	SYSTEM SHUTDOMN. TWT INDICATORS OFF.	DISCONNECT CABINET CABLE FROM J3 OF TWT.	SIMULATE BAD J3	25
		16	SYSTEM SHUTDOWN. TWT HELIX PAULT LIGHT LIT.	SHORT JUNCTION SIMULATE BAD OF A2R48 AND A2Q10 A2CR9 TO GROUND.	SIMULATE BAD A2Q10	16
		17	SYSTEM WILL NOT TRANSMIT, WILL NOT TURN ON WHEN "RESET"SWITCH ACTIVATED ON LOCAL CONTROL/STATUS PANEL. TWT "READY" AND "OPERATE" LIGHTS OFF.	SHORT A2C17 + TO GROUND.	SIMULATE BAD A2C17	17
		81	SYSTEM WILL NOT TRANSMIT, WILL NOT TURN ON WHEN "RESET" SWITCH ACTIVATED ON LOCAL CONTROL/STATUS PANEL TWT "READY" AND "OPERATE" LIGHTS OFF.	CONNECT JUMPER SIMULATE BAD ACROSS A2R45. Q8	SIMULATE BAD Q8	81
		19	SYSTEM SHUTDOWN. TWT HELIX FAULT LIGHT LIT.	SHORT A2U7-5 TO GROUND.	SIMULATE BAD U7	19

TABLE 2. MALPUNCTION INSTALLATION GUIDE

MAJOR UNIT	MAINTENANCE LEVEL	SYMPTOM NO.	SYMPTOM	METHOD OF INSTALLATION	CONDITIONS OR NOTES	BENT.
TWT AMP (CONT'D)	TWT AMP	20	SYSTEM SHUTDOWN, TWT INDICATORS NORMAL, SYSTEM WON'T RESTART.	DISCONNECT SIMULATE BAN WIRE PROM LINE LINE PILTER PILTER PL5	SIMULATE BAD LINE FILTER	07
		21	SYSTEM SHUTDOWN. TWT IN "READY" MODE, WON'T GO TO "OPERATE".	DISCONNECT SIMULATE WIRE FROM LINE CONTACTS	SIMULATE OPEN CONTACTS	12
		22	SYSTEM SHUTDOWN. TWT IN "READY" MODE, SYSTEM WON'T RESTART.	PLACE STANDBY, OPERATE SWITCH IN STANDBY POSITION	SIMULATE BAD SWITCH	22
		23	SYSTEM SHUTDOWN. ONLY TWT AC PWR LIGHT ON.	DISCONNECT R4 AND RT2 FROM COMMON TERMINAL	SIMULATE OPEN WIRE OR BAD R4 AND RT2	53
		34	SYSTEM SHUTDOWN. ONLY TWT AC PWR LIGHT ON.	DISCONNECT JUMPER BETWEEN E3 AND E4	SIMULATE OPEN PRIMARY WINDING ON TI	2
		25	SYSTEM SHUTDOWN. NO TWT INDICATORS ON.	DISCONNECT WIRE FROM FL2	SIMULATE OPEN AC LINE FILTER	52
		56	SYSTEM SHUTDOWN. TWT IN "READY" MODE. WON'T GO TO "OPERATE".	DISCONNECT WIRE FROM LINE FILTER FL4	SIMULATE BAD LINE FILTER FL4	56
		27	SYSTEM SHUTDOWN. TWT IN "READY" MODE. WON'T GO TO OPERATE.	DISCONNECT WIRE PROM LINE PILTER PL4	SIMULATE BAD A201.	23
		58	SYSTEM SHUTDOWN. NO TWT INDICATORS ON.	DISCONNECT WIRE FROM LINE FILTER FL3	SIMULATE OPEN CONTACT ON J3-N	88

TABLE 2. MALFUNCTION INSTALLATION GUIDE

MAJOR UNIT	N N	SYMPTOM	SYMPTOM		METHOD OF	CONDITIONS	DENT.
RP UNIT	EXCITER	1	SYSTEM SHUTDOWN. "FRE	*PREQ* LIGHT ON	24.8982	SIMULATE PREQUENCY ERROR	52
		~	SYSTEM SHUTDOWN. "FRE ON MONITOR PANEL.	"FREQ" LIGHT ON	DISCONNECT CABLE PROM "XTAL FREQ" CONNECTOR OF EXCITER	SIMULATE NO XTAL PREQ OUTPUT FROM EXCITER	8
		m	System shutdown.		DISCONNECT A2P1 FROM EXCITER POWER CONNECTOR	SIMULATE EXCITER FAILURE	£
		•	SYSTEM SHUTDOWN.		DISCONNECT CABLE FROM RF OUTPUT CONNECTOR ON EXCITER	SIMULATE EXCITER MULTIPLIER OR VCO FAILURE	32
		ĸ	SYSTEM SHUTDOWN		REMOVE CRYSTAL PROM EXCITER	SIMULATE BAD CRYSTAL	33
		٠ ·	SYSTEM SHUTDOWN, "FRE ON MONITOR PANEL,	"FREQ" LIGHT ON	DISCONNECT WIRE FROM E1 ON SAME P.C. BOARD AS CRYSTAL (IN EXCITER)	SIMULATE OPEN CONTROL FAILURE	£.
	BIPHASE MODULATOR (DPSK)	-	SYSTEM SHUTDOWN		SHORT EL OR E2 ON STRIP- LINE ASSY	SIMULATE SHORTED DIODE	35

DENT. 42 43 44 38 **3** . 7 36 37 39 SIMULATE OPEN DIODE SIMULATE BAD U2 SIMULATE BAD Q2 SIMULATE BAD SIMULATE BAD SIMULATE BAD SIMULATE BAD U6 SIMULATE BAD CONDITIONS OR NOTES SIMULATE SHORTED Q1 UNSCREW CR1 OF STRIPLINE 33 D SHORT U3-1 TO GROUND SHORT U1-1 TO GROUND SHORT U7-9 TO GROUND METHOD OF INSTALLATION SHORT U11-5 TO GROUND SHORT U2-11 TO GROUND SHORT U6-11 TO GROUND SHORT Q1 COLLECTOR (CASE) TO GROUND (CHASSIS) SHORT Q2 COLLECTOR (CASE) TO GROUND MALPUNCTION INSTALLATION GUIDE AMPLITUDE MODULATOR FAULT (MAY RESULT IN TEST PULSE ACCURACY FAULT AND EXECUTIVE SHUTDOWN). AMPLITUDE MODULATOR FAULT. AMPLITUDE MODULATOR FAULT. AMPLITUDE MODULATOR FAULT. AMPLITUDE MODULATOR FAULT. AMPLITUDE MODULATOR FAULT. AMPLITUDE MODULATOR FAULT. AMPLITUDE MODULATOR FAULT. AMPLITUDE MODULATOR FAULT. TABLE 2. SYMPTOM NO. ~ m S 9 σ MAINTENANCE AMPLITUDE MODULATOR LEVEL MAJOR UNIT RF UNIT

TABLE 2. MALFUNCTION INSTALLATION GUIDE

CONDITIONS INCENT.	RE THE EL 45	STATED THE R MUST BE ECTED AT	STATED THE R MUST BE ECTED AT ITIONS 46 AZIMUTH 4 ATION.			
	E REINSTATED ERROR MUST CORRECTED	_	Ę	COMDITIONS LISTED FOR BOTH AZIMUTH ELEVATION. REMOTE CONTRO STATUS ONLY.		
BEFORE THE CAN BE THE REINSTATED E ERROR MUST		_	ON THE BBD CONDITIONS BOARD (A4) LISTED FOR SHORT TPS TO BOTH AZIMU GND: AZ LC/S- ELEVATION. EL LC/S.		S-1 0 0 E	S-1 S-1 S-1 S-1 S-1 S-1 S-1 S-1 S-1 S-1
ITE CAN ITE CAN ITE ERIN ITE EREN MODE" CORR BOARD	- s/s	D COND) LIST P5 TO BOTH	IC/S- ELEV	C/S- TED OF OF ATUS	S 0 2 E	S. C. S. C.
AZIMUTH SITE OFF OR PUT THE AZIMUTH SITE IN "TEST MODE" OR REMOVE THE OR REMOVE THE	FROM THE AZIMUTH LC/S DRAWER.	ON THE BBD BOARD (A4) SHORT TP GND: AZ LA	el lc/s.	EL LC/S. ON THE BDC BOARD LOCATED IN SLOT A2 OF THE REMOTE CONTROL/STATUS ASS'Y. SHORT TP5 TO GROUND.	EL LC/S. ON THE BDC BOARD LOCATED IN SLOT A2 OF THE REMOTE CONTROL/STATUS ASS'Y. SHORT TP5 TO GROUND. ON THE BDC BOARD (A6) SHORT TP5 TO GND ON AZIMUTH LC/S.	ON THE BDC BOARD LOCATED IN SLOT A2 OF THE REMOTE CONTROL/STATUS ASS'Y. SHORT APS TO GROUND. ON THE BDC GND ON AZIMUTH LC/S. ON THE BAG BOARD IN SLOT (A10) SHORT TEST POINTS
		·			м	м
E ON, ON		DATA LINK LAMP ON THE MAINTENANCE MONITOR PANEL WILL SHOW DATA LINK ERROR. SYSTEM WILL REMAIN UP. ALSO REMOTE CONTROL/STATUS PANEL WILL NOT SHOW PROPER INDICATIONS FOR THE AZIMUTH STATUS; ELEVATION STATUS.	DATA LINK ERROR LIĞHT WILL APPEAR	rus LL Be	ON THE REMOTE CONTROL/STATUS PANEL. NO UPDATE DATA WILL BE MADE. SELECTION OF THE VAR. AUX DATA BY MEANS OF DRY, WET, ICY & CAT I, CAT II, CAT III, WILL NOT BE AFFECTED WHEN THE SELECTOR SWITCHES ARE ADJUSTED.	LL BE DATA BY CAT I, LL NOT B! R 6 WILL LAMP FENANCE
TIMING SYNC LAMP WILL COME ON, THE EL MAINTENANCE MONITOR ELEVATION SITE WILL GO DOWN.		NK LAMP ON THE MAINTENN PANEL WILL SHOW DATA I. SYSTEM WILL REMAIN UP. HOTE CONTROL/STATUS PAN I SHOW PROPER INDICATION AZIMUTH STATUS; ELEVATI	IT WILL	GENOIE CONTROL/STATUS NO UPDATE DATA WILL BE	MADE. MADE. MADE. MADE. MADE. MATERIAN OF THE VAR. AUX DATA MEANS OF DRY, WET, ICY & CAT I, AFFECTED WHEN THE SELECTOR MATERIAN OF DRY AND THE SELECTOR MATERIAN OF DRY AND THE SELECTOR MATERIAN OF DRY AND AND AND AND AND AND AND AND AND AND	SELECTION OF THE VAR. AUX DATA BY WADE. SELECTION OF THE VAR. AUX DATA BY WEANS OF DRY, WET, ICY & CAT I, CAT II, CAT III, WILL NOT IN SWITCHES ARE ADJUSTED. NUX DATA WORD IN ADDRESS 6 WILL AUX DATA WORD IN ADDRESS 6 WILL AUX LOOPE PRESENT. AUX DATA LAMP WILL COME ON, ON THE MAINTENANCE
	MAP WII	ON TH WILL S WILL NUTROL/ PROPER H STAT	R LIGH CONTRO	ATE DA	ANEL. NO UPDATE DATA ADE. EELECTION OF THE VAR. FEANS OF DRY, WET, ICY AT II, CAT III, RFECTED WHEN THE SELE WITCHES ARE ADJUSTED.	ATE DANHE VAR WET, I
	AINTEN AINTEN N SITE	K LAMP PANEL SYSTEM OTE COI SHOW AZIMUTI	K ERRO	ON OPPORT	NO UPDA NOF THE CAT II.	NO UPD) NOF THE DRY, CAT II. WHEN ARE AL
	MING SEVATION	DATA LINE MONITOR I ERROR. SALSO REM WILL NOT FOR THE A	DATA LINK ERROR LIGHT WILL AND ON THE REMOTE CONTROL/STATUS	ANEL. B	NEL. B DE. LECTION ANS OF I II, (FECTED	MADE. SELECTION OF THE WEANS OF DRY, WINDERFECTED WHEN THE WITCHES ARE ADDRY OF THE WALL BE PRESENT.
	117	DA MOI MII MII STO	Š	MAN.	SEI NAI	MARIA CAN
		д	~			
	YNC	¥			LINK	LINK
LEVEL	SYSTEM SYNC	DATA LINK			AUX DATA LINK	AUX DATA LIN Variable aux Data
IEVEL	SXS	DAT		· 	YOX	AUX VARI DATA
	S'Y					
MAJOR UNIT	CCAL CONTROL/STATUS ASS'Y					
*	STATE					

TABLE 2. MALFUNCTION INSTALLATION GUIDE

MAJOR UNIT	MAINTENANCE LEVEL	SYMPTOM NO.	SYMPTOM	METHOD OF SNSTALLATION	CONDITIONS OR NOTES	IDENT.
LOCAL CONTROL/ STATUS ASS'Y (CONT'D)	FIXED AUX DATA NO. 1 "BAR" BOARD	1	FIXED AUX DATA WORD IN ADDRESS 3 WILL BE MISSING AND ERROR LIGHT (AUX DATA) WILL DEVELOP ON THE MAINTENANCE MONITOR PANEL.	ON THE BAR BOARD IN SLOT (A12) SHORT PIN U12-9 TO GROUND.	AZIMUTH ONLY.	90
	FIXED AUX DATA 2. "BAS" BOARD	-	FIXED AUX DATA WORD IN ADDRESS 5 WILL BE MISSING FROM THE DATA STREAM. AUX DATA LAMP WILL COME ON ON THE MAINTENANCE MONITOR.	ON THE BAS BOARD IN SLOT All - PLACE A SHOKT FROM U12-9 TO GROUND.	AZIMUTHI ONLY.	15
	AUX DATA SELECTOR/WORD VERIFIER	-	FIXED AUX DATA WORD IN ADDRESS 4 WILL NOT BE TRANSMITTED AND FIXED AUX DATA IN ADDRESS 5 WILL NOT BE VERIFIED. AUX DATA LAMP ON THE MAINTENANCE MONITOR.	ON THE BAP BOARD IN SLOT A13 - PLACE A SHORT FROM U6-8 TO GROUND	AZIMUTH ONLY.	25
	AUX/ID/ ADDRESS/PARITY GENERATOR	٦	THE AUX DATA WORDS WILL HAVE THE WRONG FUNCTION IDENTIFICATION CODE. THE MAINTENANCE MONITOR WILL DETECT THIS AND DECLARE A AUX DATA ERROR AND A PREAMBLE ERROR THEN SHUT THE SUBSYSTEM.	ON THE BAW BOARD LOCATED IN SLOT A14 - SHORT PIN U13-2 TO GROUND.	AZIMUTH ONLY	53
-	MORSE CODE	ri	SYSTEM WILL GO OFF THE AIR AND THE MAINTENANCE MONITOR WILL INDICATE A PREAMBLE ERROR.	ON THE BAM BOARD LOCATED IN SLOT A-16 - SHORT TO GROUND U13-12	AZIMUTH ONLY	4.
	ID/BD/DPSK	ı	NO DATA IS BEING TRANSMITTED. SYSTEM WILL GO OFF THE AIR. MAINTENANCE MONITOR WILL HAVE PREAMBLE, BASIC DATA, IDENT., AUX. LAMPS WILL BE ON.	ON THE BAM BOARD IN SLOT A16 SHORT TP8 TO GROUND.	AZ OR EL	55
	SYS TIMING GEN	1	ELEVATION WILL GO DOWN ON SYS TIMING ERROR	ON THE BAK BOARD SHORT OUT U22-1 TO GROUND	AZIMUTH ONLY	98

TABLE 2. MALPUNCTION INSTALLATION GUIDE

	DENT.	57	88 .	65	09	19
	CONDITIONS OR NOTES	ELEVATION ONLY	AZIMUTH ONLY	ELEVATION ONLY	ELEVATION ONLY	AZIMUTH AND ELEVATION
	METHOD OF INSTALLATION	ON THE BAX BOARD SHORT U20-13 TO GROUND	ON THE BAL BOARD SHORT U8-4 TO GROUND	ON THE BAY BOARD SHORT U9-1 TO GROUND	NOTE THE SETTING OP SWITCH 85 & RECORD IT SO THAT THE SYSTEM MAY BE RESTORED TO ITS NORMAL OPERATING. SETTING. AFTER THIS HAS BEEN DONE MOVE THE SWITCH FROM POSITION #3 TO POSITION #2.	ON THE REAR OF THE LOCAL CONTROL/STATUS REMOVE P-9 FROM J9.
TO WITH THE THE PROPERTY OF THE	SYMPTOM	ELEVATION WILL GO DOWN ON SYS TIMING ERROR	SYSTEM WILL GO OFF THE AIR WITH ERP ERRORS & POSSIBLY OTHER ERRORS AS THE SIGNALS TURNING THE TRANSMITTER ON ARE INHIBITED.	SYSTEM WILL GO OFF THE AIR WITH ERP ERRORS & POSSIBLY OTHER ERRORS AS THE SIGNALS TURNING THE TRANSMITTER ON HAVE BEEN INHIBITED	ELEVATION WILL GO DOWN ON BEAM ACCURACY & BEAM ERP AS THE BEAM IS BEING CUT OFF ABOVE THE 2.5 J OF THE MONITOR HORN.	SUBSYSTEM WILL GO DOWN WITH EXECUTIVE ERROR. ON MONITOR THIS ERROR COULD BE SEVERAL DIFFERENT ERRORS. DEPENDING ON WHERE IN TIME THAT THE PLUG P9 WAS REMOVED.
	SYMPTOM NO.	7	H	~	m	-
	MAINTENANCE LEVEL	SYS TIMING GEN (CONT'D)	TIMING CONTROL			10 MHz OSC.
	MAJOR UNIT	LOCAL CONTROL/ STATUS ASS'Y (CONT'D)				

EENT.	79	63	•
COMENTIONS	AZIMUTH ONLY	AZIMUTH OR ELEVATION	AZIMUTH OR ELEVATION
METHOD OF	ON THE BBB BOARD IN SLOT A2 SHORT TP4 TO GROUND	ON THE BBA BOARD IN SLOT A1, GROUND TP4. CREATE AN EXECUTIVE ERROR BY TURNING OPP THE LOCAL CONTROL ON/OPP SWITCH MOMENTARILY.	ON THE BBA BOARD LOCATED IN SLOT A1 GROUND TP3
2. MALPUNCTION INSTALLATION GUIDE SYMPTOM	AZIMUTH AND ELEVATION WILL GO OPP THE AIR. AZIMUTH MONITOR WILL INDICATE A LOCAL CONTROL ERROR. THE ELEVATION WILL INDICATE A SYNC TIMING ERROR.	WHEN THE SUBSYSTEM GOES DOWN THE AURAL ALARM WILL NOT SOUND.	ALL THE STATUS INDICATOR LAMPS ON THE LOCAL CONTROL/STATUS PANEL MILL LIGHT UP.
TABLE 2. SYMPTOM	-	٦	٦
MAINTENANCE	SEQUENCER/ TIMER	LIGHT/DRIVER	LOCAL CONTROL STATUS INDICATOR
MAJOR UNIT	LOCAL CONTROL/ STATUS ASS'Y (CONT'D)		

	IDENT. NO.	\$	99	19	89	69
	CONDITIONS OR NOTES	NOTICE CAUTION THIS INVOIVES 120V AC. SO THE AC SHOULD BE THE CIRCUIT BREAKER ALIALCES BREFORE ANY ATTEMPT IS MADE TO IMPLEMENT THE FOLLOWING 4 PROBLEMS. AZIMUTH ONLY	AZIMUTH ONLY	ELEVATION ONLY	BLEVATION ONLY 68	AZIMUTH ONLY
	METHOD OF INSTALLATION	ON TERMINAL BOARD TB-5 LOCATED IN THE RIVOLVES BOTTOM REAR OF AC. SO THE CIRCULD BE ELECTRONICS CABINET THE CIRCUL BE ELECTRONICS CABINET ATHE CIRCUL BERAKER BE REMOVED) AFTER TURNING BEFORE AN THE AC OFF AT ATEMPT I CIRCUIT MADE TO BEREAKER CB-22 IMPLEMENT ERMOVE MIRE POLLOWING TB5-3. MOVE IT PROBLEMS. A SAFE DISTANCE FROM AZIMUTH O TIRCUIT TURNING TB5-3. TURN AZIMUTH O CIRCUIT BERAKER CB22 BACK ON.	FOLLOW PROCEDURE IN #1. ONLY REMOVE 7B5-10.	POLLOW PROCEDURE IN NO. 1.	FOLLOW PROCEDURE IN NO. 2.	REMOVE FUSE (F1) ON REAR OF LOCAL CONTROL/STATUS DRAWER.
. MALPUNCTION INSTALLATION GUIDE	SYMPTOM	RUNNING TIME METER IS NOT RUNNING.	RUNNING TIME METER IS NOT RUNNING.	RUNNING TIME METER NOT RUNNING.	RUNNING TIME METER NOT RUNNING.	RUNNING TIME METER NOT RUNNING.
TABLE 2.	SYMPTOM NO.	-	8	m	•	'n
	TEVEL MAINTENANCE	RUNNING TIME METER				·
	MAJOR URIT.	LOCAL CONTROL/ STATUS ASS'Y (CONT'D)				

TABLE 2. MALPUNCTION INSTALLATION GUIDE

MAJOR UNIT MAINTENANCE	SYMPTOM NO.	MOTAMYS	METHOD OF INSTALLATION	CONDITIONS OR NOTES	IDENT.
METER (CONT'D)	9	RUNNING TIME HETER NOT RUNNING	REMOVE FUSE (P1) ON REAR OF LOCAL CONTROL/STATUS	ELEVATION ONLY	20
CHASSIS PARTS	-	NO SIGNALS PRESENT ON BNC JACKS ON PRONT PANEL. RUNNING TIME METER STOPS.	BEHIND FRONT PANEL OF AZIMUTH LOCAL CONTROL/STATUS DRAWER REMOVE FLUG P8 (RIGHT SIDE)	AZIMUTH ONLY	12
	N	NO SIGNALS PRESENT ON BNC JACKS ON PRONT PANEL. RUNNING TIME METER STOPS,	BEHIND FRONT PANEL OF ELEVATION LOCAL CONTROL REMOVE PLUG PB (RIGHT SIDE)	ELEVATION ONLY	72
·	м	MORSE CODE WILL NOT SHUT OFF.	ON SWITCH S6 AT THE REAR OF THE LOCAL CONTROL/STATUS PANEL PLACE A JUMPER WIRE BETWEEN TERMINALS 1 AND 3	AZIMUTH ONLY	73

TABLE 2. MALFUNCTION INSTALLATION GUIDE

	IDENT. No.	14	2
	CONDITIONS OR NOTES	SIMULATES BAD POWER SUPPLY	BAD FUSE
	METHOD OF INSTALLATION	REMOVE AC WIRE SIMULATES BAD FROM 20V POWER POWER SUPPLY SUPPLY TERMINAL BOARD	REMOVE +20 VOLT POWER SUPPLY PUSE PROM PRONT PANEL
		TWI	
Tarion manufacture management	WO.	EXCITER AND TWT PANEL ON.	
CACLLOS AND	SYMPTOM	SYSTEM SHUTDOWN. EXCITER ALLIGHTS ON MONITOR PANEL ON.	SYSTEM SHUTDOWN.
		SYSTEM LIGHTS	SYSTEM
· angus	SYMPTOM NO.	1	-
	MAINTENANCE LEVEL	20v Power Supply	CHASSIS PARTS
	MAJOR UNIT	POWER SUPPLY DRWR	

TABLE 2. MALPUNCTION INSTALLATION GUIDE

CONDITIONS IDENT. OR NOTES NO.	92		11	77	77 87 97 97	77 78 78 79	77 80 80 80 81	77 78 80 80 81	77 78 79 80 81 83	77 78 80 80 81 81 81 81 81 81 81 81 81 81 81 81 81
	6-8 TO		0-8 TO	0-8 TO 0-6 TO 4A4	6-8 TO 4A4 4A4 4A4 4A19	0-8 TO 0-6 TO 6-8 TO 6-8 TO 6-8 TO	0-8 TO 0-6 TO 6-8 TO 6-8 TO 6-8 TO 6-8 TO 6-8 TO 6-8 TO	0-8 TO 6-8 TO	0-8 TO 0-6 TO 0-6 TO 0-8 TO 0-8 TO 0-8 TO 0-8 TO 0-8 TO 0-8 TO 0-8 TO 0-8 TO 0-8 TO	1-8 TO 1-8 TO 1-6 TO 1-6 TO 1-8 TO 1-8 TO 1-4 TO 1-
T U26-8 TO		T U30-8 TO ND 1A1A4A3	•	T U30-6 TO IND	T U30-6 TO ND LALALA44 T U26-8 TO ND	T U30-6 TO ND 11A1A4A4 T U26-8 TO 11A1A4A19 TT U30-8 TO ND	T U30-6 TO IAIA4A4 T U26-8 TO IAIA4A19 IAIA4A19 T U36-8 TO IAIA4A19 T U26-8 TO IAIA4A20	T U30-6 TO LALA44 T U26-8 TO LALA419 LALA419 T U26-8 TO LALA4419 T U26-8 TO LALA4420 T U30-8 TO ND LALA4A20 T U30-8 TO ND	T U30-6 TO IAIA44 T U26-8 TO IAIA419 T U30-8 TO IAIA419 T U36-8 TO IAIA4A20 IAIA4A20 IAIA4A20 IAIA4A20 IAIA4A20 IAIA4A20 IAIA4A20 IAIA4A20 IAIA4A20	T U30-6 TO IAIA44 T U26-8 TO IAIA419 T U30-8 TO IAIA419 T U30-8 TO IND IAIA420 T U30-8 TO IND IAIA420 T U30-8 TO IND IAIA4420 T U30-8 TO IND IAIA446 T U11-4 TO IND IAIA446
SHORT U26-8 TO GROUND AZIAIAIA4A3 SHORT U30-8 TO GROUND AZIAIAIA4A3	HORT U30-8 TO ROUND ZIAIAIA4A3	•	SHORT U30-6 TO GROUND AZJAJAJA444		SHORT U26-8 TO GROUND AZIAIAIA4A19	SHORT U26-8 TO GROUND AZIAIAIAAAI9 SHORT U30-8 TO GROUND AZIAIAIAAAI9	SHORT U26-8 TO GROUND AZIAIAIAAA19 SHORT U30-8 TO GROUND AZIAIAIAAA19 SHORT U26-8 TO GROUND	SHORT U26-8 TO GROUND AZJAJA4A19 SHORT U30-8 TO GROUND SHORT U26-8 TO GROUND AZJAJAJA4A20 AZJAJAJA4A20 SHORT U30-8 TO	SHORT U26-8 TO GROUND A21A1A1A4A19 SHORT U30-8 TO GROUND A21A1A1A4A20 GROUND SHORT U30-8 TO GROUND A21A1A4A20 SHORT U30-8 TO GROUND A21A1A1A4A20 A21A1A1A4A20	HORT U26-8 TO Z1A1A1A4A19 HORT U30-8 TO ROUND Z1A1A1A4A19 HORT U26-8 TO ROUND ROUND ROUND ROUND Z1A1A1A4A20 HORT U11-4 TO ROUND Z1A1A1A4A6 HORT U11-12 Z1A1A1A4A7
SHORT U26-8 T GROUND AZIAIAIA4A3 SHORT U30-8 T GROUND AZIAIAIA4A3 SHORT U30-6 T GROUND	SHORT U30-8 1 GROUND AZIAIAIA43 SHORT U30-6 1 GROUND	SHORT U30-6 1 GROUND AZIAIAIA444		SHORT U26-8 1 GROUND AZIAIAIA4A19		SHORT U30-8 1 GROUND AZlalala4A19	SHORT U30-8 1 GROUND AZIAIAIA4A19 SHORT U26-8 1 GROUND AZIAIAIA4A20	SHORT U30-8 1 GROUND AZIAIAIA4A19 SHORT U26-8 1 GROUND AZIAIAIA4A20 SHORT U30-8 1 GROUND	SHORT U30-8 1 GROUND AZIAIAIA419 SHORT U26-8 1 GROUND SHORT U30-8 1 GROUND AZIAIAIA420 AZIAIAIA4A20	SHORT U30-8 1 GROUND AZIAIAIA419 SHORT U26-8 1 GROUND AZIAIAIA4A20 GROUND AZIAIAIA4A20 SHORT U11-4 7 GROUND AZIAIAIA4A6 SHORT U11-1 TO GROUND AZIAIAIA4A6
	SHORT U3 GROUND AZIAIAIA SHORT U3 GROUND AZIAIAIA SHORT U2 GROUND	SHORT U3 GROUND AZ 1 A 1 A 1 A 1 A 1 A 1 A 1 A 1 A 1 A 1	SHORT UZ	AZIAIAIA	SHORT U3 GROUND AZIAIAIA					
	SHO GRO GRO SHO SHO SHO SHO SHO SHO SHO	SHOI GROI SHOI GROI AZ L SHO	SHOP GROD AZ 1.1 SHOP	SHO	AZI				TEM W	E .t
2							SYSTEM S			į
SYSTEM SHUTDOWN; N. SYSTEM PAULT. N. SYSTEM PAULT. PAULT. SYSTEM PAULT. SYSTEM SYSTEM SYSTEM SYSTEM SYSTEM SYSTEM SYSTEM SYSTEM	SYSTEM ULT. SYSTEM ULT. SYSTEM AULT. SYSTEM IULT. SYSTEM IULT.	SYSTEM SYSTEM SYSTEM SYSTEM IULT.	SYSTEM AULT. SYSTEM IULT. STEM SHUT	SYSTEM SULT.	STEM SHUT			EXEC FAULT: SYSTEM SHUTDOWN.		EXEC. FAULT;
[- 그가 그가 그의 그?	HT ON. HT ON. HT ON. EC. FAUI	HT ON. EC. PAU	XEC. FAI	HT ON.	EC. FAU.		BEAM ACCURACY LIGHT ON. SHUTDOWN; EXEC. FAULT.	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	SISTEM	OWN. E
EXEC. FAULT. SCAN MOD LIGHT ON SHUTDOWN; EXEC. F LCL CONT LIGHT ON SHUTDOWN; EXEC. F BEAM ERP LIGHT ON	WY LIGHWY EXEWY TO THE THE THE THE THE THE THE THE THE THE	W LIGH	RP LIGH		SLS LEFT LIGHT ON. SY SHUTDOWN; EXEC. FAULT.	FREQ LIGHT ON. EXEC. FAULT.	CCURACY NN; EXE		tult: S	EXEC FAULT: SYST PRAMBL LIGHT ON. SYSTEM SHUTDOWN.
PRAMBL LIGHT EXEC. FAULT. SCAN MOD LIG SHUTDOWN; E) LCL CONT LIG	SCAN MC SHUTDON LCL CO	וכר כסו	SHUTDO	BEAM ERP L SHUTDOWN;	SLS LE	PREQ LIGHT OF EXEC. FAULT.	BEAM A(SHUTDO)		EXEC F1	EXEC FIPRAMBL
1		7	m	4	'n	٠			-	
EXECUTIVE INTEGRATOR 'BCD'								•	MONITOR CONTROL 'BCM'	MONITOR CONTROL 'BCM' MORSE CODE GENERATOR 'BAN'
1	MAINT. MONIT. DRWR.									
	MAINT. DRWR.									

TABLE 2. MALFUNCTION INSTALLATION GUIDE

IDENT.	98	87	60	6	8	6	26	6	*	95
COMBITIONS OR NOTES									DISABLES MORSE CODE GEN	DISABLES DPSK GEN
METHOD OF INSTALLATION	SHORT U2-5 TO GROUND AZIAIAIAAII	SHORT U9-5 TO GROUND AZIAIAIAAII	SHORT U6-13 TO GROUND AZIAIAIA4A13	SHORT U9-13 TO GROUND AZIAIAIA4A13	SHORT B20 TO GROUND AZ1A1A1A4A9	SHORT B7 TO GROUND AZIAIAIA4A9	SHORT TP-7 TO GROUND AZIAIAIA4A24	SHORT TP-7 TO GROUND AZIAIAIA4A25	SHORT U12-6 TO GROUND AZ1A1A1A4A26	SHORT U10-8 TO GROUND AZIAIAIA4A26
SYMPTOM	ANTENNA +24V LIGHT ON. MAINT. PAULT.	MONITOR +5V LIGHT ON. MAINT. PAULT.	TWIN PWR OUT LIGHT ON. MAINT. PAULT.	EXCTR PWR OUT LIGHT ON. MAINT. PAULT.	PRAMBL LIGHT ON. EXEC. PAULT; SYSTEM SHUTDOWN.	AUX INP LIGHT ON. MAINT. PAULT.	PRAMBL LIGHT ON. EXEC. PAULT; SYSTEM SHUTDOMN.	PRAMBL LIGHT ON. EXEC. PAULT; SYSTEM SHUTDOWN	PRAMBL LIGHT ON. EXEC. PAULT; SYSTEM SHUTDOWN.	PRAMBL LIGHT ON. EXEC. FAULT; SYSTEM SHUTDOWN.
SYMPTOM NO.	1	~	н	7	1	7	-	-	-	N
MAINTENANCE S	ANALOG COMPARATOR #3 'BCW'		ANALOG COMPARATOR #2 'BCG'	***************************************	DECISION BCB:		AUX ID/ ADDRESS/PARITY GENERATOR 'BAW'	ID/BASIC DATA/ DPSK 'BAM'	AZIMUTH SYSTEM TIMING GEN 'BAK'	
MAJOR UNIT	MAINT. MONIT. DRWR. (CONT'D)									

TABLE 2. MALPUNCTION INSTALLATION GUIDE

IDENT.	%	93	8	66	92	101	102	103
COMPITIONS OR NOTES	REMOVES SEQUENCE INPUT TO MONITOR CONTROL	REMOVES 100 kHz CLOCK	ALSO CAUSES MAIN. PAULT - TWTA PWR OUT				•	
METHOD OF INSTALLATION	SHORT U10-5 TO GROUND AZIAIAIA4A28	SHORT U1-10 TO GROUND AZIAIAIA4A28	SHORT TP8 TO GROUND AZIAIAIA4A29	SHORT TP2 TO GROUND AZIAIAIA4A29	SHORT U2-6 TO GROUND AZIAIAIA4A29	SHORT U3-6 TO GROUND AZLALAIA1A4A29	SHORT U22-6 TO GROUND AZ1A1A1A4A29	SHORT TP7 TO GROUND AZIAIAIA4A29
SYMPTOM	MON TMG LIGHT ON. EXEC. FAULT; SYSTEM SHUTDOWN.	LEPT SLS LIGHT ON. EXEC. FAULT: SYSTEM SHUTDOWN.	BEAM ACCURACY LIGHT ON. EXEC. PAULT; SYSTEM SHUTDOWN.	TEST PULSE ACCURACY LIGHT ON. EXEC. FAULT; SYSTEM SHUTDOWN.	SIS LEFT LIGHT ON. EXEC. FAULT: SYSTEM SHUTDOWN.	SLS RIGHT LIGHT ON. EXEC. FAULT; SYSTEM SHUTDOWN.	IDENT ERP LIGHT ON. EXEC. FAULT: SYSTEM SHUTDOWN.	EXEC. FAULT; SYSTEM SHUTDOWN.
SYMPTOM NO.	ı	7	-	~	m		'n	•
MAINTENANCE LEVEL	MONITOR TIMING 'BCL'		SCAN TIMING					
MAJOR UNIT	MAINT. MONIT. DRWR. (CONT'D)							

TABLE 2. MALPUNCTION INSTALLATION GUIDE

SCAN TIMING SCAN TIMING SCAN TIMING SCAN TIMING SHUTDOWN. (SEE NOTES) SHUTTOWN. (SEE NOTES) SHORT UI-10 SHUTTOWN. (SEE NOTES) SHORT UI-10 SHUTTOWN. (SEE NOTES) AMALOG 1 BEAM ERP LIGHT ON. SYSTEM TO GROUND AZIALIAAA29 SHUTTOWN, EXEC. FAULT. SHORT UI-13 SHUTTOWN, EXEC. FAULT. SHORT UI-13 SHUTTOWN, EXEC. FAULT. SHORT UI-13 STR. TO GROUND AZIALIAAA30 AZIALIAAA30 AZIALIAAA30 AZIALIAAA30 AZIALIAAA30 AZIALIAAA30	90	E . 8 B	KE . 2 -	90	107
SCAN TIMING 7 EXEC & MAINT PAULTS; SYSTEM SHUTDOWN. (SEE NOTES) B EXEC & MAINT PAULTS; SYSTEM SHUTDOWN. (SEE NOTES) SHUTDOWN. (SEE NOTES) SHUTDOWN. (SEE NOTES) SHUTDOWN. (SEE NOTES) THE SHUTDOWN, EXEC. FAULT. "BCE" ANT TEMP LIGHT ON. MAINT. FAULT.	CONDITIONS OR NOTES	ELIMINATES START PULSE CAUSING MAIN PAULT: TWTA PWR OUT, AND 1 OF 6 POSSIBLE EXE FAULT INDICATIONS 1) BEAM ACCURACY 2) TEST PULS ACCURACY 3) EBAM ERP 4) SLS RIGHT 6) IDENT ERP	ELIMINATES 100 kHz CLOC CAUSING MAIN PAULT: TWTA PWR OUT, AND 1 OF 6 POSSIBLE EXE PAULT INDICATIONS LISTED POR SYMPTOM NO.		
SCAN TIMING 7 EXEC & HAINT PAULTS; *BCJ* (CONT*D) 7 EXEC & HAINT PAULTS; *BCJ* (CONT*D) 7 SHUTDOWN. (SEE NOTE SHUTDOWN. (SEE NOTE SHUTDOWN; EXEC. FAUL *BCE* 2 ANT TEMP LIGHT ON.	METHOD OF INSTALLATION	SHORT U6-1 TO GROUND AZIAIAIA4A29	SHORT UI-10 TO GROUND AZIAIAIA4A29	SHORT U2-13 TO GROUND AZIAIAIA1A30	SHORT U6-5 TO GROUND AZIAIAIA4A30
MANTENANCE LEVEL SCAN TINING 'BCJ' (CONT'D) COMPARATOR 'BCZ'	SYMPTOM	BKEC & MAINT PAULTS; SYSTEM Shutdown. (SEE NOTES)	Shutdown. (See Notes)	BEAM ERP LIGHT ON. SYSTEM SHUTDOWN; EXEC. PAULT.	
	SYMPTOM NO.	2	60	-	7
1.8	MAINTENANCE LEVEL	'BCJ' (CONT'D)		ANALOG COMPARATOR 'BCE'	
MAJOR UNIT DIMER. (COMP.)	MAJOR UNIT	DRIFF. (COMT'D)		- • 	

TABLE 2. MALPUNCTION INSTALLATION GUIDE

MAJOR UNIT	MAINTENANCE LEVEL	SYMPTOM NO.	SYMPTOM	METHOD OF INSTALLATION	CONDITIONS OR NOTES	IDENT.
MAINT. MONIT. DRWR. (CONT'D)	DETECTOR/ COMPARATOR 'BCR'	1	BEAM & TEST PULSE LIGHT ON. SYSTEM SHUTDOWN, EX. PAULT.	SHORT JUNCTION OF R1 & R2 TO GROUND AZIAIAIA4A31		108
	BEAM ACCURACY COUNTER 'BCS'	٦	BEAM 6 TEST PULSE LIGHT ON. SYSTEM SHUTDOWN, EX. PAULT.	SHORT U3-15 TO GROUND AZIAIAIA4A32		109
		۶ .	BEAM LIGHT ON. SYSTEM SHUTDOWN. Exec. Pault.	SHORT U1-10 TO GROUND AZIAIAIA4A32		9
		м	TEST PULSE LIGHT ON. SYSTEM SHUTDOWN. EXEC. PAULT.	SHORT U5-10 TO GROUND AZIAIAIA4A32		=
•	DIGITAL COMPARATOR 'BCC'	~	PREC LIGHT ON. SYSTEM SHUTDOWN; EXEC. PAULT.	SHORT U16-13 TO GROUND AZIAIAIAAA33		112
		7	BEAM LIGHT ON. SYSTEM SHUTDOWN; EXEC. PAULT.	SHORT U12-5 TO GROUND AZIAIAIAAA33		113
		e	TEST PULSE LIGHT ON. SYSTEM SHUTDOWN; EXEC. PAULT.	SHORT U12-13 TO GROUND AZIAIAIA4A33		ž
		•	PREG LIGHT ON. SYSTEM SHUTDOWN; EXEC. PAULT.	SHORT U15-5 TO GROUND AZIAIAIAAA33		
	•	'n	PREO, BEAM, TEST PULSE LIGHTS ON. SYSTEM SHUTDOWN; EXEC. FAULT.	SHORT U11-3 TO GROUND AZIAIAIA4A33		911
						,

TABLE 2. MALPUNCTION INSTALLATION GUIDE

	NO.	711	8	611	120	121	122	123	
Ī	CONDITIONS OR NOTES								
	METHOD OF INSTALLATION	CHANGE S2 SETTING (+) OR (-) 1 DIGIT AZIAIAIAA34	REMOVE COAX CABLE CONNECTED TO A4J3 OF AZIAIAIA4A34	SHORT U16-8 TO GROUND AZIAIAIA4AI	SHORT U26-6 TO GROUND A21A1A1A4A1	SHORT U29-8 TO GROUND AZIAIAIA4A2	SHORT U15-6 TO GROUND AZIAIAIA4A2	SHORT U29-8 TO GROUND AZIAIAIA4A18	
	SYMPTOM	PREG LIGHT ON. SYSTEM SHUTDOWN; EXEC. FAULT.	EXEC. FAULT.	MOD PHASE LIGHT ON: MAINT. PAULT.	AUX DATA LIGHT ON. MAINT. PAULT.	+20V ELECTRONICS LIGHT ON. MAINT PAULT.	+5V MONITOR LIGHT ON. MAINT PAULT.	ELEC TEMP LIGHT ON. MAINT. FAULT.	
	SYMPTOM NO.	1	N	-	7	м	*	٠n	
ſ	MAINTENANCE	PREQUENCY MONITOR 'BCP'		MAINTENANCE INTEGRATOR 'BCF'		-			
	MAJOR UNIT	MAINT, MONIT. DRWR. (CONT'D)							

TABLE 2. MALFUNCTION INSTALLATION GUIDE

NO.	124	125	126	121	128	
ξ :S	CR4	CR26	CR30	CR34		
COMPITIONS OR NOTES	SIMULATES CR4 BURN OUT	SIMULATES CR26 125 BURN OUT	SIMULATES CR30 BURN OUT	SIMULATES CR34 BURN OUT	SIMULATES PAULTY 53	
	SIP	SIN	STO	SIP		·
D OF ATION	R4 A4A35	R26 A4A35	R30 A4A35	R34 A4A35	WIRE E30 AT S3	
METHOD OF INSTALLATION	SHORT CR4 AZIAIA:A4A35	SHORT CR26 AZIALALAA4A35	SHORT CR30 AZIAIAIA4A35	SHORT CR34 AZIAIAIA4A35	BETWEEN E30 AND S3, AT S3	
	8	<i>s</i> ≺	ω∢			
	SYSTEM	IGHT D.	GHT D.	NOT	BY LAN	
		NOT L	OT LI	DOES IS AC	ATED	
SYMPTOM	HT OC	DOES IS ACT	OES N	IGHT	ACTIV	
S	or s	IGHT EST 1	GHT E	+15 I	NOT , S3.	
	STATU ING.	ERP L	IN LI	ONIC	LAMPS	·
	MAINT STATUS LIGHT OUT.	IDENT ERP LIGHT DOES NOT LIGHT WHEN LAMP TEST IS ACTIVATED.	AUX DATA LIGHT DOES NOT LIGHT WHEN LAMP TEST IS ACTIVATED.	ELECTRONIC +15 LIGHT DOES NOT LIGHT WHEN LAMP TEST IS ACTIVATED.	PANEL LAMPS NOT ACTIVATED BY LAMP TEST SWITCH, S3.	
SYMPTOM NO.	1	N	м	4	-	
					CHASSIS PARTS, PRONT PANEL SWITCHES	
MAINTENANCE LEVEL	MAINT. MON. INDIC.				CHASSIS PAR PRONT PANEL SWITCHES	
MA					CHAS PRON SWIT	
=	MAINT. MONIT. DRWR. (CONT'D)					,
MAJOR UNIT	₹ 8					
W.	MAINT.					·

TABLE 2. MALPUNCTION INSTALLATION GUIDE

	201101121111111	010000000		22 22.53	Court Troops	1
MAJOR UNIT	IEVEL	NO.	SYMPTOM	INSTALLATION	OR NOTES	9
MONITOR POWER SUPPLY DRAWER	MONITOR RECEIVER ASSEMBLY	t	SYSTEM SHUTDOWN. PREAMBLE, TEST PULSE ACCURACY OR BEAM ACCURACY PAULT INDICATED.	DISCONNECT CABLE PROM A2J5	SIMULATES BAD OSCILLATOR ON REGULATOR BOARD A3U3	621
		7	SYSTEM SHUTDOWN (SAME AS SYMPTOM #1)	DISCONNECT CABLE FROM Z1-R	SIMULATE BAD MIXER	130
		m	SYSTEM SHUTDOWN (SAME AS SYMPTOM 81)	DISCONNECT PWR CONNECTOR TO C-BAND L.O	SIMULATE BAD C-BAND L.O. MULTIPLIER	131
		•	SYSTEM SHUTDOWN (SAME AS SYMPTOM #1)	REMOVE CRYSTAL FROM C-BAND L.O Al	SIMULATE BAD CRYSTAL	132
	•	w	SYSTEM SHUTDOWN, PREAMBLE LIGHT ON MONITOR PANEL ON.	SHORT AJE2 TO GROUND (LEAD OF ANI - 75 OHM RESISTOR IS CONNECTED TO E2)	SIMULATE BAD A3U1	133
		v o	SYSTEM SHUTDOWN (SAME AS SYMPTOM #1)	SHORT TO GROUND CAUSES VCO IN THE JUMPER C-BAND L.O. BETWEEN PINS 5 TO UNLOCK AND 9 OF C-BAND L.O. POWER CONNECTOR	CAUSES VCO IN C-BAND L.O. TO UNLOCK	134
		2	SYSTEM SHUTDOWN (SAME AS SYMPTOM #1)	TAPE OR PUSH OUT CONTACT ON JI-F OF MONITOR RECEIVER ASSY	SIMULATE BROKEN WIRE OR BAD CONNECTOR	135
		∞	SYSTEM SHUTDOWN. PREAMBLE LIGHT ON MONITOR PANEL ON.	SHORT TP13 SIMULA (U206-1) OF A2, A2Q202 RCVR MODULE, TO FAILUR GROUND	SIMULATE A2Q202 FAILURE	136
						ŀ

TABLE 2. MALPUNCTION INSTALLATION GUIDE

MAJOR UNIT	MAINTENANCE LEVEL	SYMPTOM NO.	MOTAMYS	TOM	METHOD OF INSTALLATION	CONDITIONS OR NOTES	IDENT.
MONITOR POWER SUPPLY DRAWER (CONT'D)	MONITOR RECEIVER ASSEMBLY	6	SYSTEM SHUTDOWN, TEST PULS. AND/OR BEAM ACCURACY FAULTS INDICATED.	62	SHORT COLLECTOR SIMULATE OF A2Q104 TO A2Q104 GROUND PAILURE	SIMULATE A20104 Pailure	137
	(COMT. D)	10	SYSTEM SHUTDOWN. INDICATED.	PREAMBLE FAULT	SHORT A2TP5 TO GROUND	SIMULATE A2Q201 OSC CIRCUIT PAILURE	138
		77	SYSTEM SHUTDOWN. TEST PULSE ACCURACY AND OR BEAM ACCURACY PAULT.		SHORT A2TP2 TO GROUND	SIMULATE BAD A2U111	139
		12	SYSTEM SHUTDOWN.	PREAMBLE FAULT. SHORT A2TP15 TO GROUND	SHORT A2TP15 TO GROUND	SIMULATE BAD A2U112	140
		13	SYSTEM SHUTDOWN.	PREAMBLE PAULT.	SHORT AZTP7 TO GROUND	SIMULATE BAD A2U206	7
		7	SYSTEM SHUTDOWN.	PREAMBLE PAULT.	SHORT A2TP6 TO GROUND	SIMULATE BAD A2U205	142
		15	SYSTEM SHUTDOWN. PREAMBLE, PULSE ACCURACY, AND OR BEAM ACCURACY FAULT.	TEST	SHORT TP1 ON SIMULATE REGULATOR BOARD +12 VOLT A3 TO GROUND REGULATO	SIMULATE BAD +12 VOLT REGULATOR	143
		16	SYSTEM SHUTDOWN. PREAMBLE, PULSE ACCURACY, AND OR BEAM ACCURACY FAULT.	PREAMBLE, TEST ND OR BEAM	SHORT TP2 ON REGULATOR BOARD A3 TO GROUND	SIMULATE BAD -12 VOLT REGULATOR	7
		17	SYSTEM SHUTDOWN. PREAMBLE, PULSE ACCURACY, AND OR BEAM ACCURACY FAULT.	PREAMBLE, TEST ND OR BEAM	UNSOLDER WIRE FROM A2J4 INTERNAL TO A4	SIMULATE BAD 1ST I.P. STRIP	145
		18	SYSTEM SHUTDOWN. PREAMBLE, PULSE ACCURACY, AND OR BEAM ACCURACY FAULT.	PREAMBLE, TEST ND OR BEAM	DISCONNECT PI FROM A2J1	SIMULATE BAD CONNECTOR	146
	Supply	-	SYSTEM SHUTDOWN		DISCONNECT AC SIMULATE BAD WIRE PROM POWER POWER SUPPLY BUPPLY TERMINAL BOARD	SIMULATE BAD POWER SUPPLY	142

TABLE 2. MALPUNCTION INSTALLATION GUIDE

MONITOR POWER 15V POI BUPPLY DRAWER SUPPLY (CONT'D) CHASSI		Ę			2505 50	<u>.</u>
СНАЯ	15v Power Supply		SYSTEM SHUTDOWN.	DISCONNECT -15 VOLT WIRE FROM TERMINAL BOARD	SIMULATE BAD POWER SUPPLY	148
	CHASSIS PARTS	-	SYSTEM SHUTDOWN. MONITOR PANEL LIGHTS OFF. AC PUR LAMP OFF ON MONITOR POWER SUPPLY DRAWER.	DISCONNECT WIRE FROM AC POWER SWITCH	SIMULATE BAD SWITCH	149
		~	SYSTEM SHUTDOWN.	REMOVE FUSE	BLOWN FUSE	150
······································		m	SYSTEM SHUTDOWN. PREAMBLE, TEST PULSE ACCURACY, AND OR BEAM ACCURACY FAULTS.	REMOVE CONTACT	SIMULATE BAD P1	151
COOLING FAN CHASS	CHASSIS PARTS	<u>н</u>	FAN OFF - OVER TEMPERATURE FAULT INDICATED IF CABINET EXHAUST TEMPERATURE EXCEEDS +50°C.	REMOVE FAN FUSE BAD FUSE ON TOP REAR OF CHASSIS	BAD FUSE	152
		N	SAME AS SYMPTOM 1	REMOVE AC WIRE FROM TERMINAL BOARD IN PAN DRAWER	SIMULATE BROKEN WIRE	153
		m	AIR BLOCKED - OVER TEMPERATURE COVER AIR PAULT INDICATED IF CABINET FILTER WITH EXHAUST TEMPERATURE EXCEEDS +50°C CARDBOARD OR HEAVY PAPER	COVER AIR FILTER WITH CARDBOARD OR HEAVY PAPER	SIMULATE DIRTY 154 FILTER	154
						

TABLE 2. MALPUNCTION INSTALLATION GUIDE

MAJOR UNIT	MAINTENANCE	SYNAPTON NO.	SYMPTOM	METHOD OF INSTALLATION	CONDITIONS OR NOTES	DENT.
ANTENNA	SCAN SWITCH	-	SCAN SWITCH PAULT IND. DSI ON INT. SCAN SWITCH MONITOR DSS ON SCAN SWITCH MONITOR	MASK OPP PIN 3 SV SUPPLY TO OP J6 ON S13 SWITCH	SV SUPPLY TO SWITCH	155
		~	SCAN SWITCH PAULT IND. DSI ON INT. SCAN SWITCH MONITOR DSS ON SCAN SWITCH MONITOR	MASK OPP PINS 2 AND 15 OP 36 ON S13	CONTROL TO SWITCH	156
	,	~	SCAN SWITCH PAULT IND. DSI ON INT. SCAN SWITCH MONITOR DS5 ON SCAN SWITCH MONITOR	MASK OPP PIN 6 MONITOR PROM OP J6 ON S13 SWITCH	MONITOR PROM SWITCH	157
		₹	SCAN SWITCH FAULT IND. DSI ON INT. SCAN SWITCH MONITOR DS5 ON SCAN SWITCH MONITOR	MASK OPP PIN 4 -40V SUPPLY OP J6 ON S13 TO SWITCH	-40V SUPPLY TO SWITCH	158
		'n	SCAN SWITCH PAULT IND. DS1 ON SCAN SWITCH MONITOR EXPANDER BOARD #1 DS5 ON SCAN SWITCH MONITOR BOARD	MASK OPP PIN 3 SV SUPPLY OP J6 ON S5 TO SWITCH	SV SUPPLY TO SWITCH	159
		v	SCAN SWITCH PAULT IND. DS1 ON SCAN SWITCH MONITOR EXPANDER BOARD #1 DS5 ON SCAN SWITCH MONITOR BOARD	MASK OPP PINS 2 AND 15 OP J6 OM S5	CONTROL TO SWITCH	091
		7	SCAN SWITCH PAULT IND. DS1 ON SCAN SWITCH MONITOR EXPANDER BOARD #1 DS5 ON SCAN SWITCH MONITOR BOARD	MASK OPP PIN 6 MONITOR PROM OP J6 ON S5 SWITCH	MONITOR PROM SWITCH	191
		60	SCAN SWITCH PAULT IND. DS1 ON SCAN SWITCH MONITOR EXPANDER BOARD #1 DS5 ON SCAN SWITCH MONITOR BOARD	MASK OPP PIN 4 -40 V SUPPLY ON J6 ON S5 TO SWITCH	-40 V SUPPLY TO SWITCH	162
		•	SCAN SWITCH FAULT IND. DSI ON SCAN SWITCH MOWITOR EXPANDER BOARD #2 DS? ON SCAN SWITCH MONITOR BOARD	MASK OPP PIN 3 SV SUPPLY OP J6 ON S9 TO SWITCH	5V SUPPLY TO SWITCH	163

TABLE 2. MALPUNCTION INSTALLATION GUIDE

MAJOR UNIT	MAINTENANCE LEVEL	SYMPTOM NO.	SYMPTOM	METHOD OF INSTALLATION	CONDITIONS OR NOTES	IDENT. NO.
ANTENNA (CONT'D)	SCAN SWITCH (CONT'D)	01	SCAN SWITCH FAULT IND. DSI ON SCAN SWITCH MONITOR EXPANDER BOARD #2 DS5 ON SCAN SWITCH MONITOR BOARD	MASK OPF PINS 2 AND 15 ON J6 OF S9	CONTROL TO SWITCH	164
		11	SCAN SWITCH FAULT IND. DSI ON SCAN SWITCH MONITOR EXPANDER BOARD #2 DS5 ON SCAN SWITCH MONITOR BOARD	MASK OFF PIN 6 MONITOR FROM OF J6 ON S9 SWITCH	MONITOR PROM SWITCH	165
	SCAN MON.	~	SCAN MON. PAULT INDIC. DS1 ON SCAN CONTROL COMPARATOR	REMOVE PUSE ON SCAN MON.	REMOVE FUSE ON AC TO MONITORS 166 SCAN MON.	166
		8	SCAN SWITCH PAULT INDIC. DSS ON SCAN SWITCH MONITOR	MASK OPP PINS 9 AND 22 ON JG OP SCAN MOD.	+5V	167
		m	SCAN SWITCH PAULT INDIC. DSS ON SCAN SWITCH MONITOR	MASK OFF PINS 10 AND 23 OF JG ON SCAN MOD.	+24V	168
		4	BRAM ACC. INDICATOR	MASK OFF PINS 1 AND 14 OF JG ON SCAN MOD.	SIGNAL INPUT	691
	ANT. SELECT SWITCH	-	erp indicators for several Antennas	MASK OFF PINS 4 AND 12 OF J6 ON ANT. SEL. SWITCH	-40V LINE	170
BEAM STEERING	SCAN CONTROL	A	SCAN ELECTRONICS PAULT. DS3 ON SCAN CONTROL COMPARATOR	MASK OPP PIN B23 ON SCAN CONTROL BD. IN BM STEERING	CONTROL TO SCAN MOD	<u>171</u>
		7	SCAN ELECTRONICS PAULT DS2 AND DS4 ON SCAN CONTROL COMPARATOR	MASK OFF PIN B32 ON SCAN CONTROL BD	100 kHz CLOCK TO MONITOR	271

SWITCH MONITOR SWITCH MONITOR FAULT SWITCH MONITOR FAULT SWITCH MONITOR FAULT SWITCH DRIVER MONITOR FAULT SWITCH DRIVER MONITOR FAULT CC CNTR PAULT SCAN MOD. CONTROL FAULT SWITCH CONT. FAULT CONDITIONS OR NOTES CLOCK PAULT MASK OFF PIN B24 ON SCAN SWITCH MONITOR B26 ON SCAN SWITCH MONITOR EXPAND ON TIE TP3 OF SCAN CONTROL MONITOR TO VCC MASK OFF PIN A8 ON SCAN SWITCH DRIVER B10 ON SCAN MASK OPP PIN B24 ON SCAN CONTROL MONITOR MASK OFF PIN B35 OF SCAN CONTROL MASK OPP PIN SCAN CONTRCL MONIT. MASK OFF PIN MASK OPP PIN MASK OFF PIN B29 ON INT. SCAN SWITCH DRIVER METHOD OF INSTALLATION BII ON INT. SCAN SWITCH GND TP2 OF MONITOR HONITOR MALFUNCTION INSTALLATION GUIDE SCAN SWITCH PAULT DS2 ON INT. SCAN SWITCH MONITOR SCAN SWITCH FAULT DS2, DS5 ON SCAN SWITCH MONITOR SCAN SWITCH FAULT DS2, DS5 ON SCAN SWITCH MONITOR SCAN ELECTRONICS PAULT DSI ON INT. SCAN SWITCH DRIVER SCAN ELEC. FAULT DS3, DS4 ON SCAN CONTROL COMP. SCAN ELEC. PAULT DS3, DS4 ON SCAN CONT. COMP. SCAN ELEC. FAULT DS3, DS4 ON SCAN CONT. COMP. SCAN ELECTRONICS FAULT DS4 ON SCAN CONT. COMP. DS1 ON SCAN CONT. MONITOR SCAN ELECTRONICS FAULT DS1 ON SCAN SWITCH DRIVER MON. EXP. SYMPTOM SCAN SWITCH FAULT DS5 ON S.S. MONITOR DS3 ON S.S. MON. EXF TABLE 2. SYMPTOM ~ -~ -SCAN SWITCH MON. EXPANDER INTERMEDIATE SCAN SWITCH DRIVER SCAN CONTROL COMP. SCAN CONTROL MONITOR SCAN SWITCH MONITOR MAINTENANCE SCAN SWITCH DRIVER INT. SCAN SWITCH MON. 10 MHz OSC. BEAM STEERING (CONT'D) MAJOR UNIT

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TABLE 2. MALPUNCTION INSTALLATION GUIDE

	TEST SWITCH	TEST SWITCH	SIMULATE BAD	· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·	<u> </u>
TEST SHORTED LAMP TEST SWITCH				K . #	e = =	g * ±
		r 10 LATOR R	PIN OF	, #	T PIN UF T PIN H SIMULAT CONNECT OR) +5V TO +1V	PIN UF POWER CONNECT OR) +5V TO +1V OR E
"TEST" POSITION			MODULE	MODULE PUSH OUT PIN OF JI (POWER CONNECTOR)	MODULE PUSH OUT PIN OF OF JI (POWER CONNECTOR) ADJUST +5V SUPPLY TO +1V	MODULE MODULE PUSH OUT P OF JI (POW CONNECTOR) ADJUST +5V SUPPLY TO LOOSEN OR INSULATE OUTPUT CONNECTION
	EAM	CURACY, , AND/OR		CURACY, D/OR	CURACY, D/OR +5V)	CURACY, D/OR +5V) P FAULT
	ORS ON BI	BEAM ACON SWITCH		BEAM ACC ITCH, ANI ULT	BEAM ACO ITCH, ANI ULT PAULT (BEAM ACC TITCH, AND ULT FAULT (- BEAM ERI
ELECT. P.	FAULT INDICAT	UTDOWN - ROL, SCA PAULT		UTDOWN - SCAN SW LATOR PA	IUTDOWN - SCAN SW ILATOR PA R SUPPLY	UTDOWN SCAN SW LATOR FA R SUPPLY UTDOWN
STEERING ELECT. PAULT SCAN SWITCH PAULT	SCAN MOD. PAULT ALL PAULT INDICATORS ON BEAM STEERING	SYSTEM SHUTDOWN - BEAM ACCURACY, SCAN CONTROL, SCAN SWITCH, AND/OR BEAM ERP FAULT		SYSTEM SHUTDOWN - BEAM ACCURACY, BEAM ERP, SCAN SWITCH, AND/OR SCAN MODULATOR FAULT	SYSTEM SHUTDOWN - BEAM ACCURA BEAM ERP, SCAN SWITCH, AND/OR SCAN MODULATOR PAULT ANT. POWER SUPPLY PAULT (+5V)	SYSTEM SHUTDOWN - BEAM ACCURACY, BEAM ERP, SCAN SWITCH, AND/OR SCAN MODULATOR FAULT ANT. POWER SUPPLY FAULT (+5V) SYSTEM SHUTDOWN - BEAM ERP FAULT
٦		7		m		
CHASSIS PARTS					SV POWER SUPPLY	SV POWER SUPPLY RF DETECTOR
BEAM STEERING (CONT'D)					ANT. POWER SUPPLIES	ANT. POWER SUPPLIES MONITOR HORN ASSY

COMPLTIONS OR NOTES (OR JUMPER TB1-d TO TB1-6) SHORT R13 OF LPB A3 IN ELEVATION SHELTER SIGNAL JUNCTION BOX SHORT R14 OF LPB A3 IN ELEVATION SHELTER SIGNAL JUNCTION BOX JUMPER TB1-1 TB1-2 OF LPB A5 IN EL SHELTER SIGNAL JUNCT. BOX WIRE FROM TB2-9 OF LPB Al IN EL SHELTER SIG. JUNCTION BOX LIFT R5 AND R6 ON LPB A3 IN ELEVATION SHELTER DISCONNECT WIRE FROM TB2-7 OF LPB ELEVATION SHELTER SIG. METHOD OF INSTALLATION RAISE R7 OR RAISE R7 OR JUNCT. BOX DISCONNECT ELEVATION SHUTDOMN - (MAY TAKE HOURS) SYSTEM TIMING FAULT. SYNC PRESENCE MAINTENANCE FAULT LIGHT (IMMEDIATELY) MALPUNCTION INSTALLATION GUIDE SYSTEM SHUTDOWN - BEAM ERP PAULT ANTENNA +5V P.S. MAINTENANCE PAULT LIGHT ANTENNA +24 P.S. MAINTENANCE PAULT LIGHT ELEVATION SHUTDOWN - SYSTEM TIMING PAULT SYMPTOM DATA LINK FAULT TABLE 2. SYMPTOM ~ ~ ~ -皇 m MAINTENANCE LEVEL LPBD #1 LPBD #2 LPBD 44 **IISCELLANEOUS** MAJOR UNIT

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TABLE 2. MALPUNCTION INSTALLATION GUIDE

ANTENNA +5V P.S. MAINTENANCE FAULT LIGHT
ANTENNA -40V P.S. MAINTENANCE PAULT LIGHT
antenna +24v P.S. Maintenance Pault light
SYSTEM SHUTDOWN
SYSTEM SHUTDOWN
SYSTEM SHUTDOWN

Appendix E

Reliability and Maintainability
Predictions Prepared for the MLS Basic
and General Aviation Airborne Equipment

Contract No.
DOT FA-72WA-2801

prepared by

The Bendix Corporation

Communications Division

Towson, Maryland 21204

January 1978

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E.3	SUMMARY RESULTS	E-1
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E.3.3	Prediction Details	E-7
	SUPPLEMENT A	E-8

APPENDIX E

RELIABILITY AND MAINTAINABILITY PREDICTIONS PREPARED FOR THE MLS BASIC AND GENERAL AVIATION AIRBORNE EQUIPMENT

E.1 INTRODUCTION

This Appendix presents the results of the reliability predictions prepared for the MLS Basic Narrow and Small Community airborne equipments.

E.2 REQUIREMENTS

The reliability and maintainability requirements for the Basic Narrow airborne equipment are specified in FAA-ER-700-07, Table 11-7A. The requirements are a mean-time-between-failures (MTBF) of 1500 hours, mean-elapsed-time, maintenance (MET) of 0.25 hours and maintenance-man-hours/operating-hour (MMH/OH) of 0.0005.

E.3 SUMMARY RESULTS

E.3.1 Basic Narrow Airborne Equipment

The result of the reliability prediction is an MTBF of 1,870 hours for the active angle equipment less the auxiliary data display, and 1,290 hours with the auxiliary data display. The prediction is based on an ambient temperature of 30°C, considered a typical environment for the equipment. The equipment is designed to be fully operational at the maximum specified temperature. For completeness, the variability of the MTBF with temperature over the possible operating temperature range is shown in Figure E-1. The detailed reliability block diagram for the active Basic Narrow airborne equipment at 30°C is shown in Figure E-2.

The MTBF for the executive monitor equipment is 23,300 hours. Combining this with the results for the active equipment, the total system MTBF is 1,700 hours without the auxiliary

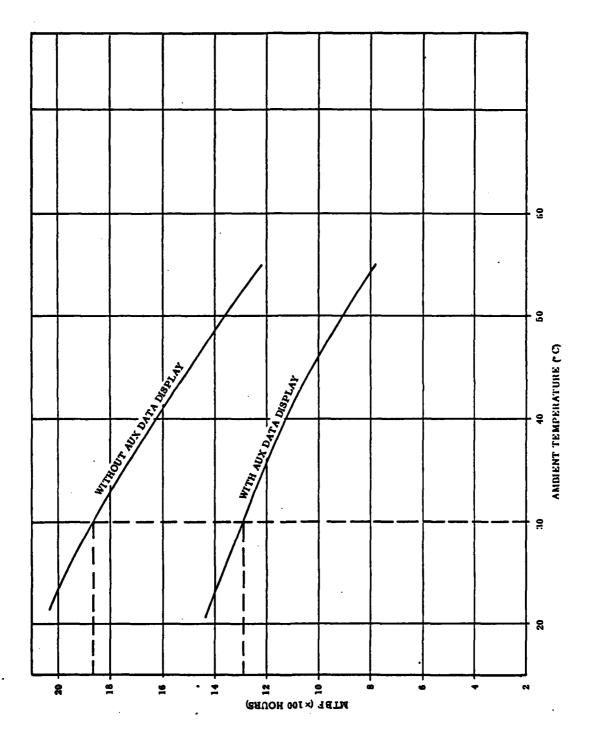


FIGURE E-1. BASIC NARROW AIRBORNE EQUIPMENT

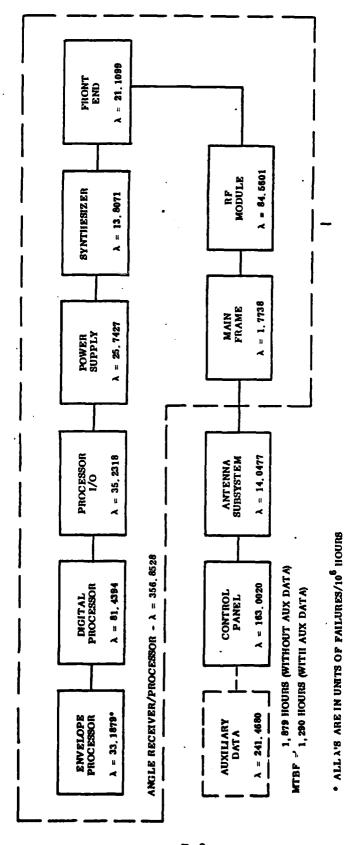


FIGURE E-2. BASSIC NARROW AIRBORNE EQUIPMENT

data display and 1,200 hours with the auxiliary data display.

Maintenance monitoring equipment has been added to aid in fault localization and isolation. Failures in this equipment do not cause degradation of system operation. A prediction, however was performed for this equipment for use in determining system maintainability characteristics. The predicted MTBF for the maintenance monitoring equipment is 79,000 hours.

Estimates of maintenance times have been made for all elements of the Basic Narrow airborne equipment. The resultant mean-time-to-repair (MTTR) values are shown in the following table, where MTTR is defined as the time required to repair after the equipment has been removed from the aircraft.

UNIT	(F/10 ⁶ hrs.)	MTTR (HRS)
Angle Rcvr/Processor	412.4868	0.50
Control Panel	163.0020	0.25
AUX Data Display	241.4680	0.25
System	816.9568	0.38

The MMH/OH (average maintenance hours per operating hour) is therefore

$$MMH/OH = F.R. \times MTTR = 0.00032$$

Also, the MET, which is the average maintenance time for localizing and replacing the entire airborne equipment, is estimated to be 0.17 hours.

E.3.2 Small Community Airborne Equipment

The predicted MTBF for the Small Community airborne equipment is 1,590 hours, computed for an ambient temperature of 30°C. Figure E-3 illustrated the relationship of MTBF to ambient temperature. Figure E-4 shows the detailed reliability block diagram for this configuration at 30°C.

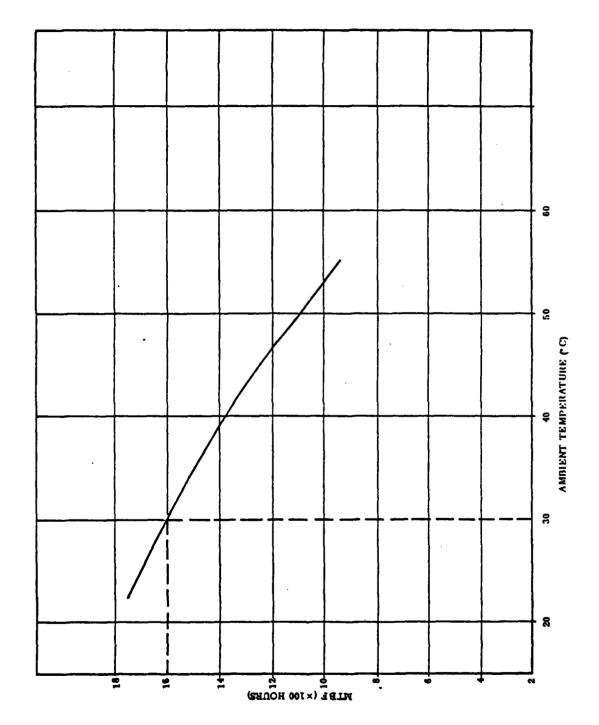


FIGURE E-3. SMALL COMMUNITY AIRBORNE EQUIPMENT

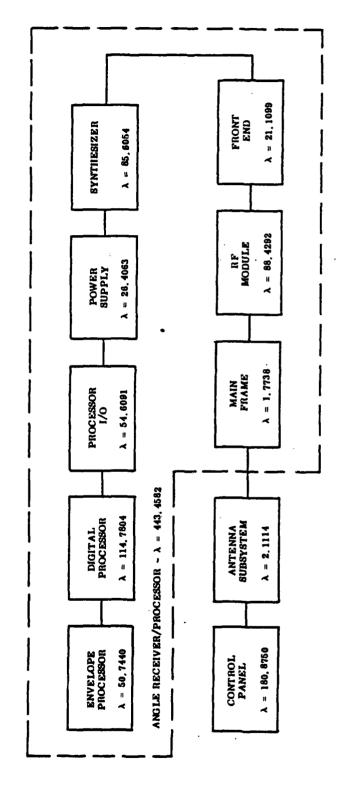
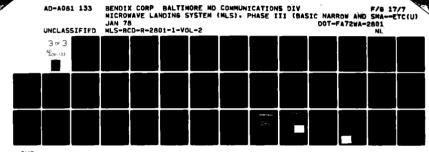


FIGURE E-4. SMALL COMMUNITY AIRBORNE EQUIPMENT



BND BDG

The estimated MTTR parameters are shown in the following table.

UNIT	(F/10 ⁶ hrs.)	MTTR (HRS)
Angle Rcvr/Processor	443.4582	0.50
Control Panel	180.8750	0.25
System	624.3332	0.43

The computed MMH/OH is 0.00027 and the estimated MET is 0.17 hours.

E.3.3 Prediction Details

The source of failure rates used in the prediction is Mil-HDBK-217B. The Airborne, inhabited environmental factors contained in this source were applied to account for the intended operating environment.

An operating ambient temperature of 30°C was assumed for both the Basic Narrow and the Small Community prediction. This is estimated to be the typical temperature at which the equipment will operate. Temperature rises within the equipment were applied on a subassembly level depending on the location of the subassembly within the equipment and are based on measured values. The temperature rises which were used range from 0°C to 35°C. These temperature rises were added to the ambient temperature in performing the prediction; that is, for an assembly with a 20°C internal rise, the 30°C prediction was made using 50°C to enter the part failure rate tables.

Detailed computer listing of the reliability predictions are given in Supplement A. Two separate listings are included, one for the Basic Narrow and one for the Small Community equipments. Each lisiting shows a complete part breakdown for each subassembly/board in the equipment, the operating electrical stress and the part failure rates for four different temperatures, 0°C, 25°C, 30°C and 54°C. The last page of each computer listing shows a summary of each subassembly/board failure rate and the total failure rate of the equipment.

SUPPLEMENT A

Detailed Computer Listings of Reliability Predictions for Basic

Narrow and the Small Community Airborne Equipment

A SSENDIY A	SSEAMIN ACTIVE COURP	SHA/	SHBASSEMBIY ANGLE	C BFF/PROC	4400	FNVELAPE	2040 30	THE	INTERMAL TEMPERATURE	ATURE RISE	20
								•			1
LRVIPONEFUT/T (f.P.1) AINPO	LWVIPONKTHT/TFMFEATUPE CONDITION FAIRS (f.p.1) AINDRAFAHINED (f.R.2) A . DEGPE	1011101 (F. 25		FOLLOV Pporf, junarijer S c	(f.P.3) 30 been	AIPPORNE TEES C	.3) AIPPORME, IMMABITED Degrees C	5.	.R.4) AIRBORNE, 4 Degrees C	· IRNARI TED	
CRT PAPT		PART	NON-STB PART NO.	PERCI GIY	F.R. SOURCE	7	FRROR	(E.R.1)	(f.n.2)	(f.A.3)	(5.8.4)
73	LEC.						; ; ; ; ; ;	2.23012	2.39460	2.45221	2.92046
~				· ·				1.74689	1.87407	1.91162	2.2775
21 75 61(6)	FICKORLFC. LINEAR			•				2.81208	2.74.55	3.46678	7141-6
<u>د</u>				. ~		•		1.51602	2.00917	2.26327	5.66171
3	551/45			c		•		2.12364	2.31456	2.3R144	2.93540
27 .				0.				0.77748	0.81982	0.83465	0.95749
								0.77748	0.81982	0.83465	0.95749
ຊ				•				0.48563	0.51754	0.52872	0.62130
				~ ·				0.84377	0.89301	0.91026	1.05413
3012 31				-				0.26025	0.27031	0.27383	0.36303
~	Sa/155			•				6.505.0	0.70855	0.21075	0.229F1
33T, 51 /1				•				0.46370	1.00.1	104404	2076.0
	MICTORILE SOLVES		•	•				75075	C9784. 1	25770 7.	17060 66
74 17 1916	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7		. •					2,10221	1,0705	1,15021	7.76906
je N	こうじょう かんしゅう かいしょうしゅうしゅう しんしゅうしん しんしゅつ アンドラン・アンドラン・アンドラン・アン・アン・アン・アン・アン・アン・アン・アン・アン・アン・アン・アン・アン					٠		0.19437	0.36712	0.41531	0.72414
1 15 RTS1	RESISTABLE LEB-COMP.)	RC B		.01				0.00487	0.01187	0.01418	0.03332
	RESISTING (FIVED-CORP)	BC K		*				0.00235	0.00571	0.00682	0.01597
2 ,	SISTOR (FIXED-COMP)	PC P		- 4				0.00207	0.00498	0.00594	0.01377
	HISISTAP(FIVED-COMP)	RCR		1.				0.00171	0.00411	0.00400	0.01136
	25215135(FIVED-CO%P)	۳ ا		31.				0.00089	0.00223	0.00268	0.01656
	CARDINATION OF THE PROPERTY OF	Z (70.				45100.B	0.00.00		20.00
		× 0						190000		2 200 2	
15 26 51	RESISTOR (FIRESTORE)	. a							0.00148	0.00127	0.01416
	ELSISTER (FIXED-LORP)			-				0,00052	0.00125	0.00148	0.00344
	STORESTORESTORES	. e		- a-				0.00061	0.00148	0.00177	0.00416
	RESISTANCE (FIVEN-COMP)	2 Y						0.00061	0.00148	6.00177	0.00416
	NFSISTAN (FIXED-CORP)	¥ 2.4		-				0.00052	0.00125	0.00148	0.00344
?	MESISTUR (POWER-FILM)	4		٠				0.02866	0.03597	0.03765	0.04672
7	PF SISTOR (POWER-FILM)	42						0.02866	0.03597	0.03765	-046
• •	f (7film)		14757A	,				0.53725	0.66081	0.69216	0.95011
	CFFAC JTOF (CFRAHIC)	5						0.25108	0.26924	0.27302	٧.
2	CALACITOF (CERAMIC)	ž	•	10.				.3390	1.43593	1.45613	1.55.70
1. 25 CAUA	CA"AC J TOW (C! KAPIC)	5	•		•			0.16145	0.17313	0.17557	0.18774
	CAP/CIT+R(CERA+IC)	ž						0.0001	0.0%654	0.08776	0.09575
	CALTEN (CERANIC)	ž		-				0.08071	0.08654	974800	0.00385
	CAFACIT' P(CFRA"IC)	5		-				0.08071	0.08654	0.08776	0.09575
1.	CATACITOM (CLKA 11C)	5						0.04090	0.07675	0.07797	2750°0
	C>+ &C IO & (CF EAM IC)	ž		~ ·				21252.0	0.25963	0.26328	0.28154
	CAPACITY K (CERA' IC)	ž		-				n.08071	.0765	9.080.0	0.09385
1 (8.8)	CATACITOR (LERANIC)	X.		-				n.08n71	0.08654	0.08776	0.09385

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CONTRAC	CONTRACT MES PROFRAM	B INJUATION	RASIC AIRBORNE EQUIP	EQUIP DATE	S/26/76	76 REV			
ASSEABL	ASSEMPLY ACTIVE EQUIP	SUBASSEMPLY ANGLE PEC/FROC	PEC/FROC	HOARD DI	PIGITAL PROC		INTERNAL TEMPERATURE RISE	ATURE RISE	92
1 MV 3 ROH (1 . h. 1) 3 O E	INVIROUPLITZTIMPERATURE CONDITION I	IBITION PAIPS FOLLOW (F.R.2) AIRPORMF-IMHARITED 25 BEGKEES C	. SHHAPITED	(f.r.3) Atrporme, Ipharited 30 degrees c	PORNE , I PHA C		(f.R.4) AIRPORNE-INNAMITED 54 DEGREES C	322391160	
TANK TANK	- 4	TAT TOX-STATE TO	PERCY OTY STRESS	F.R. B	REV ERROR CODE	(1.8.1)	(f.R.2)	(f. n. 3)	(f.n.4)
					; ; ; ; ; ; ;	25.0000	25.06600	25.00000	25.00600
- E	PICROLLEC. LSI		•	s		4.60497	6.03601	6.51336	10.27014
-	BAP MEMORY		· ·			16.61782	21,35752	22.93851	35.3K353.
4	ROF MERCHY		•			0.67191	0.72977	0.75004	0.91793
•	MICKOCLEC. SSI/MSI		 - :			0.19401	0.97764	1.00720	1.25042
•						1.26566	1,33952	1.36539	1.57969
*	MICHOFLEC. SSI/MS!		•			0.44172	0.46852	162270	0.55566
•						0.69917	0. 76139	O. 78319	0.96372
•	HICROELLC. SSI/MSI		- ·			1.68754	1.78602	1.82052	2.10626
•	"JCROFLIC. SS./MSI		•			4.43729	11,23606	14.49800	54.16652
-	BAT BERORY		• ·			11504	1.19730	1.72611	1.46473
	MICPOFLEC. SSI/MSI		•			1.16623	1.22973	1.25197	1.43623
•			•			0.55753	0.59865	0.61305	0.73234
•	MICADFLEC. SSI/MSI					0.60150	0.66809	0.70255	1.16339
			•			0.71216	0.77651	0.79905	0.98575
	BSCROELLC. SS1/MS3		- ·			26025	0.27031	0.27383	0.30303
-	ATCHOFLEC. SSI/MSJ		•			0.26025	0.27031	0.27383	0.30303
•	MILKUTLEC. SSI/MSI		•			0.26025	0.27031	D.27383	0.30303
	AICPOLLEC. SSI/4SI		• •			\$0800 C	0.00963	0.01014	0.01452
•	CAFACITIR(TAWT. EL.) (SR	CSR				0.30936	0.58589	10199.0	1.15252
_	701734767					0.20000	0.2000	0.2000	0.20000
•	QUARTZ CRYSTAL) ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ;	1		
		4				61.77066	75.76927	81.43937	146.2:
	THE PURISOR DAILE FOR THE		•						

ASSEMILY ACTIVE FOUTP	VE FOUTP	SUBA	SUBASSEMELY ANGLI	ANGLE RECIPRAC	8048	PROCESSOR 1/0	104 1/0	-	INTERNAL TEMPERATURE	EMPERAT	UNE RISE	20
NUTRONNENT/I	INVIGOUPENT/TEMPERATURE CONDITION PAIDS (F.H.1) AINFORME/INHARITED (F.H.2) A II DEGNES C	No 1110N (f.		FOLLOW PEORME, INHARITED S C	(f.m.3) ATRPO 30 DEEMEES C	ATEFORME TEES C	(f.m.3) Atrporme/Immabited 3D Degres C	5.	.R.4) AIRBORNE.INHABITED 4 DEGNEES C	JORNE . IN	HABITED	
CKT PART	•	PART 17PE	PARI NON-SID	PERCT GIY STRESS	F.R. SOURCE	» F		(1.8.1)	ł	(F.B.2)	(1.1.3)	(3.8.5)
USC BOR BERORY					· · · · · · · · · · · · · · · · · · ·	! ! !		1.54034	3.78462	162	4.86435	17.97064
	100				_			0.63942	1.61312	112	2.08028	7.76165
USA PICHOELIC.	fc. Linean			.0				4.93647	5.59792	192	5.94013	10.51704
U45 AJCFOLLIC.	IC. LINEAR				_			0.60150	0.66909	60	0.70255	1.16339
uss sickofter.	CC. LIVEAR			•				2.91471	3.26220	02:	3.44198	47478° S
137 HICHOFLIC.	.rc. \$\$1/M\$1							2.27012	2.39460		2.45221	2.92944
HII MICROELEC.	EC. SSI/MSI							0.44172	0.46852		6.47791	0.55566
U4: PICEDELEC.	EC. 551/HS1			.0	_			0.55753	0.594		0.6130S	0.73236
HAR MICHOELEC.	EC. \$51/451			e -				0.36364	0.38235		0.38890	0.44319
	FC. 551/MS1							3.28777	3.56590	200	3.66332	11074.4
								1.10932	2.80901	101	3.62450	13.54163
	FC. SSI/MSI							0.47191	77621.0	111	0.75004	0.91703
UP FICRUELLC.	Lt. SSI/MSI			0.0	~			0.60342	0.6290	060	0.63917	0.71600
	.EC. \$51/451			•	_			C.26025	0.27031	331	C.27383	0.30303
U1) MICHOFLEC.	EC. \$51/451				_			0.60543	0.65326	126	0.47001	0.80878
U12 HICRUELEC	.EC. SSI/MSI	•			_			0.24025	0.27031	334	0.27383	0.311303
WIS MICROELEC.	.EC. \$\$1/HS1							0.0000.0	0,0000	900	00000-0	0.0000
U15 MICRUFLEC.	EC. LINEAR			_ =	_			0.60150	60499°D		0.70755	1.16330
HIS MICPOELEC.	.tc. \$51/KS1			.0	_			0.30171	0.31495		U.31959	0.35KW
U15 MICANFLFC.	ft. SSI/MSI				_			0.38874	0.40		0.41732	0.47874
TRANSISTOR	TOR (GF)	M		25.				0.78662	1.49053	153	1.71936	4.33A11
Olobe (SI)	(15)	6 P		10.				0.30493	0.51551	151	0.56777	D.R7764
4ES1510	HESTSTOR (FIXED-COMP)	BC B		2. 12	•			C.00634	0.01524	124	0.01817	0.04219
PES1510	PESISTOR (FIXED-COMP)							0.00291	0.00721	721	0.00864	0.02050
CESIS 18	MESISTOR (FIXED-COMP)			3. 10				0.00538	0.01295	564	0.01544	10210.0
RESISTA	RESISTOR(FIXED-COMP)				•			0,00211	0.00508	108	90900.0	0.01406
DFS1510	RESISTOR (FIXED-COMF)	RCR						0.00184	79700"0	791	0.00558	0.01356
# S1810	RESISTOR (FIXED-COMP)	2			•			0.00122	0.00297	26	0.00354	0.00733
PESISTO	PESISTOR (FINED-COMP)			15. 2	•			0.00133	0.00327	127	0.00391	0.00926
HESIST	HESTSTOR (FOLER-FILE)			7.	•			0.01329	0.01658	558	0.01733	0.02142
HSC BESISTA	BUSISION (FIXER-COMP)			1. 14				0.00726	0.01744	17.	0.02078	0.04718
	20.0		•		_			0.25732	0.48733	733	0.54981	0.95864

THIS DOCUMENT IN PERT CHARLITY PRACTICABLE.

THE COPY SHAD SHAD SHAD A SIGNIFICATION OF PAGES WHICH DO NOT REPRODUCE LEGIBLY.

CONTRACT		HLS PROGRAM		ELUIFMENT	BASIC AIRBORNE	£ 401 P	DATE	3/196/16	n t		•	
ASSER	SSEMBLY ACTS	ACTIVE EQUIP	SUBA	ISSEMBLY ANGLE	E REC/PROC	POAR	POVER SUPPLY	SUPPLY	JULE	INTERNAL TEMPERATURE	ATURE AISE	90
6	VIRUNHFWI/I .m.1) A IRIN U DEGREES C	EMPEHATURE RNE, INNAGII	COMBITION (F.	R.23	PS FOLLOW AIRPORME, INMARITED REES C	(r.a. S) AIRPOL 3(1 DEGREES C	A IRPORNI Rf ES C	.A.S) AIRBORNE, IMMABITED (* Degres C		(f.e.4) Airhorní, imhabited Sá degres c	S M A D & TE D	
CV1 SVH-L	PART DFSCH		PART	NON-STB PART NO.	PERCT QTY STRESS	F.R. Sounce	REV	FROR	(f.n.1)	(f.B.2)	(f.n.3)	(f.P.4
5	MICKUELEC.	EC. LINEAR	i } !	1 1 1 1 1 1 1 1	0. 1		1 1 1 1 1 1 1		0.52891	0.58464	0.61347	0.99907
70	MICRUELEC				e :				0.42923	0.47095	0.49253	0.74119
5 :	MULSISHWALL AND A STORE	108 (SI)	- q						0.31670	11.42652	0.45816	0.615.0
y M	#115151711 #115151411		Z Z		· ·				0.10363	0.13880	0.14670	0.19034
70	#U181844#		HPR						0.10363	0.13480	0.14670	0.19734
50	TF INSISTOR	TOR (SI)	2						0.15161	0.19881	0.21004	0.27818
ý r	TRANS IS TOR								0.13181	0.19461	0.1410	2444
5	DIOPE	_			23.				0.51997	0.83482	0.91243	1.38313
2 % 3	3	(ZEHER)	;		-				0.33147	0.41244	0.42958	0.51871
C + 2	30316	(15)	9		- ;				0.05542	0.09799	0.10872	0.17259
	= 7	(51)	a 5		57. 15.				0.17.65	U. 66768	0.2050	0.45145 0.4444
	101000	(25)	- 6		14.				0.17418	0.28934	0.31779	0.48694
C # 3	3	(21)	3		, s				0.25631	0.44384	0.49075	0.76966
Ck 16		(ST)	ę,		2. 2				0.11499	0.20225	0.22419	0.35470
CRAS	6100E	^	<u>.</u>		· ·				0.11083	0.19598	0.21743	0.34517
5:	TKANSISICA	Translate (SI)	Z 0						0.09983	0.13422	0.14192 A 00122	0.18424
2 3	SISIS SA	MENIOR (FIVED-COMP)							0.00052	0.00125	0.00148	0.00344
. ex	THERMISTOR	TOR							0.52000	0.52000	0.52000	0.52000
:	RESISTO	RESISTOR (FIXED-COMP)			-				0.00052	0.00125	0.00148	0.00344
Ş	RESISTO	RESISTOR (FIXED-COMP)			-				0.00052	0.00125	0.00148	0.00344
⊃ N ≖ 3	RESISTO	STOK (FIXED-CO4P)							0.00052	0.00125	0.00148	7 774113
֚֚֚֚֓֞֞֞֞֞֟֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֡֓֡֓֡֡֡֓֓֡֓֡	2 2 2	RESISTOR (FIXED-COMP)							0.00061	0.00148	0.00177	0.00416
£ 1 S	_	RESISTOR (FIXED-COMP)			-				0.00052	0.00125	0.00148	0.60344
k 1 k	_	STOR (FIVED-COMP)			80.				0.00213	0.00577	0.00705	0.01435
к1516 813	1538	STOR (FIXED-COMP)	¥ 5		. 0. .0.				0.00356	0.00451	0.01157	0.020.0
	OTSISTO	CIUD (EIXED-COMP)							0.00104	0.00.00	0.00300	AKCAA. A
H 2 4	HES1810	STUK (FIXED-COMP)			-				0.00052	0.00125	0.00148	9,0000
1123	RES1510	STOR (FIXED-COMP)			10. 1				0.00061	0.00148	0.00177	0.00414
# 2 4 	5	STOK(FIXED-COMI)							0.00052	0.00125	0.00148	97600.0
\$? !		STOK (FIXED-COMP)			- ·				0.0005	26100.0	20100	0.00.00
2 Y 2	#[5]5]#	ST. M. C. L. M. C. C. C. C. C. C. C. C. C. C. C. C. C.	Z 4		• •				0.00052	0.00125	0.00.00 8.41.00.0	7710000
1 / N	2 2	SISTOR (FIXED-UV)			20°				0.19124	0.24822	0.26151	0.33591
K.3.1	3	STOP (FLYED-COMP)			-				C.00052	0.00125	0.00148	0.00344
632	WE S 1 S 1 O	STOR (POVER-FILM)	X X X		2. 1				n.n0672	0.00839	0.00877	0.010.85
r 3 S	5	STOR (FORTB-1111)			-				0.00665	0.000	0.00866	0.010.7
# 2¢	3	S1 38 (*0*E** FILM)			· ·				0.60761	0.00479	0.00019	0.01141
2 2	7		4						0.00037	0.00137	20000	97.500.0
# 50 # 57	9651510	\$15 f0# (F1 xF0 - COMF)	# & C						0.00057	0.00137	0.00163	0.00.0
					•							,

T ANGLE REC (PROC ROARD POWER SUPPLY FOLLOW SUPPLY	100	LONTRACT	T MLS PROGRAM		EQUIPMENT	1848	C AIRB	BASIC AIRBORNE FAUIP		DATE	2/26/76	REV				
	A 5 51	T. B. L.	T ACTIVE EQUIP	7 8 ns		GLE RE	C/PROC		ROARS	POVER	SUPPLY	Ξ	INTERNAL TEMPERATURF	ENPERATU	AF NISE	90
## 51877# (FINE) PART HOW-STO STRESS SOURCE CODE ## 51877# (FINE) PCR 17PE PART HOW-STO STRESS SOURCE CODE ## 51877# (FINE) PCR 13. 1 10. 10. 1 10. 1 10. 1 10. 1 10. 10. 1 10. 10. 1 10. 10.	2	K. 1)	HALNITEMPERATURE CON ATRECRESIMANITED HEES C	017101 (f.		I OU AME / IN	HAB I TE		(f. 8.3) 30 of68	AIRBORN FFS C	IE , INNABIT		(f.R.4) AIRBORNE-INHABITED 54 DEGREES C	386 - 38E	ABITED	
# \$1810# (FIRE - COMP) PCR # \$1810# (FIRE - COMP) RCR # \$1851870# (FIRE - COMP) RCR # \$100	CKT SYB	=				PE	,		F.R.	2		F. 2	(F.B.2)		(F.R.3)	(f.R.4)
## \$1510 # (FIRED-COPP) # CR		3			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1		-			1 1 1 1 1 1	0.00064	0.00157) 	0.00188	0.00444
## # # # # # # # # # # # # # # # # # #	842	_		20			20.	.				0.00073	0.00160		0.00216	0.00515
CAPACITOR (CALIM. EL.) CS	~ >		_	2	AAR IS IS E		€.	_				0.89732	n.94263		992560	1.00.1
######################################	ī	_		3			2:	~ •				2.67684	4.67378		5.34712	11.575/4
CAPACITUR (CERANIC) CR CAPACITUR (TANT. EL.) CSR CAPACITUR (TANT. EL.) CSR CAPACITUR (CERANIC) CR CAPACITUR (CERANIC) CR CAPACITUR (CERANIC) CR CAPACITUR (CERANIC) CR CAPACITUR (TANT. EL.) CSR CAPACITUR (TANT. EL.) CSR CAPACITUR (TANT. EL.) CSR CAPACITUR (TANT. EL.) CSR CAPACITUR (TANT. EL.) CSR CAPACITUR (TANT. EL.) CSR CAPACITUR (TANT. EL.) CSR CAPACITUR (TANT. EL.) CSR CAPACITUR (TANT. EL.) CSR CAPACITUR (TANT. EL.) CSR CAPACITUR (TANT. EL.) CSR CAPACITUR (TANT. EL.) CSR CAPACITUR (TANT. EL.) CSR CAPACITUR (TANT. EL.) CSR FOURTR (TANT. EL.) C	3:	۰ د		E 2.								24444	0.0410		70949.0	0.424.0
CAPACITOR (CERANIC) CK CAPACITOR (TANT. EL.) CSR CAFACITOR (TANT. EL.) CSR CAFACITOR (TANT. EL.) CSR CAPACITOR (TANT. EL.)	::			; E						•		0.00540	0.01476		0.01804	\$2.70
CAFACTION (TANT, EL.) CSR	Ü			: ¥			: ~:	-				0.08073	0.08657		0.08778	0.09387
S CAFACTION (TANT, EL.) CS# 15. 1 10. 2 10. 2 10. 2 10. 2 10. 2 10. 2 10. 2 10. 2 10. 2 2 2 2 2 2 2 2 2	2			CSR			٠.	_				0.00284	0.00339		0.00357	0.00512
S CAFACITUR (CERANIC)	:		7	CSB			15.	_				0.00104	0.00125	•	0.00131	0.001FF
CAPACITOR (TANT. EL.) CSR CAPACITOR (TANT. EL.) CSR CAPACITOR (TANT. EL.) CSR CAPACITOR (ALUM. EL.)	1713	13		¥			<u>.</u>	~				0.16734	0.17949		.18202	0.19464
CAPACITOR (TANT, EL.) CSR CAFACITOR (TANT, EL.) CSP CAPACITOR (TANT, EL.) CSR CAPACITOR (CERASIC) CAPACITOR (CERASIC) CAPACITOR (CERASIC) CAPACITOR (CERASIC) CAPACITOR (CERASIC) CAPACITOR (CERASIC) CAPACITOR (CERASIC) CAPACITOR (CERASIC) CAPACITOR (CERASIC) FOUFR WFREFFILTER FOUFR WFREFFILTER FOUFR WFREFFILTER FOUFR WFREFFILTER FOUFR WFREFFILTER COMMECTOR COMMETTER 1			×	,		2 0.	_				0.10462	0.11218		0.11376	0.12165	
CAFACITOR (TANT. EL.) CSR CAFACITOR (ALIM. EL.) CSR CAFACITOR (ALIM. EL.) CSR CAFACITOR (ALIM. EL.) CU CAFACITOR (ALIM. EL.) CU CAFACITOR (ERAMIC) CAFACITOR (FILTER POUER NEWPORTER POUER NEWPORTER POUER NEWPORTER POUER NEWPORTER POUER NEWFORTER POUER NEW	C 1 3			CSR	•		20:	- ,				0.08998	0.10767		.11341	0.16238
CAPACITOR (ALW. EL.) CW	֓֞֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓			450			ğ.					0.041/8	0.0200		0.02.00	0.0754
CAFACISTACALUM. EL. CU							9					0.00140	0.07408		20220.0	2 111.03
CATACIONE CENTRE CONTROL CONTR	[2]	_		3 :			• •					750467	U.V45/7	•	70676	7.22746
POWER NEWFILTER POWER NEWFILTE	777			3 :								0 0 14 14 0	2020		20101	0.00712
POWER KERPETTER POWER KERPETTE	<u>.</u>	_		.								0.800			23750	0.04448
POSTER NEWAPILTER NEWAPILTER P	3	- 4					;		,			0.02820	0.0330		0.03452	0.04688
POSER XFRA/FILTER POSER XFRA/FILTER POSER XFRA/FILTER POSER XFRA/FILTER POSER XFRA/FILTER POSER XFRA/FILTER POSER XFRA/FILTER POSER XFRA/FILTER POSER XFRA/FILTER POSER XFRA/FILTER POSER XFRA/FILTER POSER XFRA/FILTER POSER XFRA/FILTER POSER XFRA/FILTER POSER XFRA/FILTER		. 2						-				0.02820	0.03301		0.03452	0.04688
POWER XFRAFILTER POWER YFRAFILTER POWER	7	. 4						_				0.02820	0.03301		.03452	0.04672
POWER MERCALTER POWER MERCALTER POWER MERCALTER POWER MERCALTER CONNECTED	2	۵.						_				0.02820	0.03301		.03452	0.04628
FOWER MEMAFILTER FOWER MEMFILTER FOWER MEMAFILTER FOWER MEMFILTER FOWER MEMAFILTER FOWER MEMFILTER FOWER MEMAFILTER FOWER MEMFILTER FOWER MEMAFILTER FOWER MEMAFILTER FOWER MEMFILTER FOWER MEMAF	9	. 4					.	_				0.02820	0.03301		6.03452	0.046 FR
FOWER XFM/FILTER POWER XFM/FILTER CONTENTS XFMF/FILTER CONTENTS XFMF/FILTER CONTENTS XFMF/FILTER CONTENTS XFMF/FILTER	[]	. 3						_				0.02820	0.03301		0.03452	0.04688
POWER MERRITTER 0. 1 CONNECTOR COUNTY OF THE	=======================================	•						_				0.02820	0.03301	_	0.03452	0.04688
	=	•					:	_				0.03452	0.04767		0.05213	0.09414
	12		OUFR XFMR/FILTER				. =					0.03452	0.04767		0.05213	0.09416
		•					•	•						,		
• • • • •	101	AL F	TOTAL FAILUPE HATES FOR THIS LEVEL ARE.	S LEVI	-	:					17	17.92465	23.92792		25.74274	411.75922

THE COTY TO AND IS BEST QUALITY PRACTICABLE,
THE COTY TO AND TO DECCONTAINED A
SIGNIFICANT NUMBER OF PAGES WHICH DO NOT
REPRODUCE DEGIBLY.

	DRIKALI ALS PRESERVA			EGUIPHENT	BASIC AIRBURNE			DATE	92/92/2	> 2			
ASSTAIR Y	IRV ACTIVE EUUIP	FULLF	SUBASSE	SSEMPLY ANGLE	LE RECIPROC		9 4 9 B	Symthe S 12 fr	8 12 FR	IMI	INTERNAL TEMPERATURE, R1SE	NATURE, P1SE	02
EEVIN CF.E.	ENVIROBBLYTTEMFERATURE COMBITION PAIRS FOL (f.r.1) Aimidrme, immamited (f.r.2) Aimid (j begefee) c	ERATURE COI , Innahited	4611304 (F. 25	PAIRS FOLLOW R.2) AIRPORME OFGREES C	IPS FOLLOW 5) AIRPORMF.IMMABITED GREES C		(f.R.3) AIRHORNE 30 DEGREES C	LES C	E - IMMAÐITEÐ		(f.B.4) AIRBODNE, INHADITED 54 DEGREES C	, 188A911E9	
CKT	PART	; ; ; ; ;	PART	MON-SID PART NO.	•	017 F		A E <	ERROR	(1.8.1)	(1.11.2)	(6.8.3)	(1.8.4)
5		ı			9.	-		1 2 6 3 4		0.73884	0.97274	1.09375	2.71220
~ =	MICHOFLEC.						٠			0.26112	0.29582	0.31377	0.55390
~						~ -				0.4555	2645.0	97445.0	1.66484
\a \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \					.	•				22777 U		64490	0 45404
2 2 2 3 4 4 4 4		551/851			. 5	- ~				0.8684	1.04586	1.13765	2.36524
2					•					0.62860	n.69939	0.73A02	1.22587
U	-					~				1.76230	1.98834	2.10529	3.66939
U1214	MJCROELEC.	18H/188			•	eri i				1.89470	2.42255	2.69564	6.34.11
2.	THE PARTY				ċ	- •				2.63049	6.35348	•	30.02
÷	MICROFIEC.				.	- •				00757-0	2// 54-0	•	6.141.0
>	MICHOFLEC.	S81/188		_	o s	- •				0.4.56.00	27754.0	0.40073	
	TOURDELEC.	L. J. M.C. A. K.	4	•	÷ -					87790	0.00.0	A.101.0	77411
- 6	TRANSISTOR									0-22022	0.33018	0.36543	0.70551
, ~,	TKANS1510F	(81)	202			-				1.98190	2.61236		3.78707
C 133		_	5		15.	~				0.17995	0.29766	0.32672	0.40971
CR313		_	5		÷	=				0.60957	1.07787	1.19589	1.808.1
Ch 14	DICDE (VAR/REC/TUM)	REC/104)		•		-				2.68772	3.60719	3.81277	4.94604
CR 15	DI OUE CVAR	R+ C/ TUM)	•		2	. .				2.68772	3.60719	3.81277	4.946.4
•	DICOE (MC M	IXCR)	(15)			٧.			-	\$9175. G	70.02	2000	103401
.121	TEAMOTOR (ST)		E 4			- ~			•	0.60927	0.82891	0.8888 0.8888	1,819/1
1717	MOLSISHAL	(21)	# # #		20.	. –				1.01545	1.38152	1.48096	2.10034
£15	DICUE (7E'IER)	TER)	<u>:</u>		15.	_				0.39896	0.48744	6.50676	0.61370
=	RESISTOR(FIXED-COMP)	EXED-COMP)	RC R		-	•				0.00311	0.00747	0.00791	0.020.65
H2	RESISTOR (FIXED-COMP)	IXED-COMP)	¥ :		- .	- •				0.00130	0.00311	1,000.0	0.00460
~ :		I VED - CORP.)	Z 0		<u>:</u> .					1 00207	200100	70,00	
	ARTOLOGICA STRUCTURAL	TARDICANT.	E 0		-	• ^				10000	97000	0.000	
	(1101-03:11) W: C C C C C C C	(40)-(3)	. a		• •	. :				0.00806	0.01942	0.02316	0-05356
414	DESISTANCE OF SEPTEMBLY	TXED-COMP.			:-	. •				0.00259	0.00623	0.00742	0.01721
2	AESISTOR(FIXED-COMP)	TXED-COMP)	80		· ~	~				0.0010A	0.00259	0.00309	9.00.0
48.34	MESISTOR (FINED-COMP)	I MED-COMP)	. X			· ~ •				0.00108	0.00259	0.00.0	0.0071
*	RESIST OR (F	ST-JR (FIVED-COMP)	æ			_				0.00087	0.00219	0.00263	0.000 C
4 4 4	(4MO)-03X1 1) 401515 1d	(4HO)-03X1	RC R		5.	·c				C.00334	U.DOAUB	0.00-64	0.02248
K 5.7	RESISTOR (FIXED-COMP)	1766-6040)	BCB		30.	,				0.00087	0.00219	0.00263	0.00436
A 5.0	RESISTOR (+1 XED-CORF)	1 x E D - C OH1.)	55		<u>.</u>	- ·				0.00067	0.00163	•	0.00463
H 20	PLSISTOK (FIXED-COMP)	[x [D - C J b]	A C.		*	•				0.00219	0.00528	0.00630	0.01467
2	ALSISTOR (FIXED-COMP)	IXED-COMP)	8 C.		ς,					C.00054	0.00129	6.00154	0.00.55
7.7	KFS1ST3KCF	CANCO-CONT.	Z .		•					Acono. 0	42100.0	ACT 00.0	41100.0
40 %	KES ISTOR (FIVER-COMP)	1 VED-C(HIP)	3 :		<u>.</u>	4 (0.00207	0.00498	46.00.0	77510.0
# C.7	RTS1STOR(F	STOR (F1 4F0-COM")	Z .		- ;	~ .				0.00.0		0.00297	1 VOO 0
\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	STOR (LIXED-COME)	I XED-COMIT	<u>د</u>		ŏ,	- ,				0.00087	1200	•	0.000.0
* 2C		(d) F. H. C	_ :		- :					5.63199	6.15519	6.79722	
۳ ک ۳	RESISTOR CE	SISTOR(Flakb-Comp)	2 2		•	-				0.00149	0.00392	0.0047	0.01201

ASSEMILY ACTIVE EQUIP											
!	CTIVE EQUIP	SUE	SUBASSEMELY ANGLE	ANGLE REC/PROC	30 A B B	STATHES 12 FR	S 1 2 F.R	2	INTERNAL TEMPERATURE	ATURE BISE	2
ENVIRONMENT/TI (1.W.1) AIRPO (1 CERIES C	ENVINONMENT/TEMPERATURE CONDITION PAIRS (1.4.1) AIRPORME/IMMAHITED (F.R.2) A II EGREES C	01110) (f. 25		FOLLOW Rønre-inhapited S c	(f.#	.3) ATROGNI Degrees C	.3) AIRCORNE, INNABITED Degrees C		(F.R.4) ATRORNE, INHAPITED 54 DEGREES C	Inharited	
1		PART TYFE	MON-STD PART NO.	PERCT OTY STRESS	Y F.R. SOUPCE	3 E <	ERROR		-		(1.8.4)
FGV RES	RESISTOR (FIVED-COMP)	35	.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	1.		! ! ! !	 	0.00156	0.00374	0.00445	0.01033
		R C P		-	-			Ø.00052	0.00125	0.0014R	0.00344
~	4ESISTOR (FIXED-COMF)	RCH		- :	•			0.00207	. 0.00498	0.00594	0.01377
	RFS1STUR(F1XED-COMP)	RCR		- :	_			0.00052	0.00125	C-00148	0.00344
	KFSISTOR (FIXED-COMP)	RCE		9	-			0.00149	0.00392	0.00475	0.01201
H7576 RESI	RESISTURCFIXED-COMP)	RCR		69.	~			0.0029A	0.00783	0.00.0	0.02402
		RCR		50.	-			0.00125	0.00322	0.00390	0.00972
HE-T RESI	resistor (fixed-corp)	RCR		, 0	~			0.00298	0.00783	0.00050	0.02402
	RESISTOR(FIXED-COMP)	RCR		10.	-				0.00148	6.00177	0.06416
		£ T H		٥2	_			1.60000	1.60000	1.60000	1.60000
747	CFRAMIC)	×		25. 1	_			1.17346	1.24954	1.26534	1.34398
		*		35.	~			0.57710	0.61451	0.62228	0.66096
		¥	_	15.	~			0.16724	0.17809	0.18034	0.19155
		7		20.	2			0.19271	0.20520	0.20780	0.22071
		. 5		.04	_			0.25052	0.26676	0.27014	0.28693
		X		10.	_			0.77084	0.82081	0.83119	0.88285
		5		30.	4		,	0.50465	0.63320	0.64120	0.67106
	7	CSB		33.	_			0.00884	0.01058	0.01114	0.61505
170	£1.)	CSR		33.	~			0.01768	0.02115	0.02228	0.03160
	1	Z S S		33.	-			0.00884	0.0105A	0.01114	0.01595
	C	¥		×	•			0.21449	0.22755	0.23025	0.24369
*		.			•			0.42897	0.45509	0.46050	0.48734
	_	2			_			0.03241	0.06914	0.08045	0.15649
•	_	2		-	~			0.11882	0.15565	0.16888	0.30513
	. 41				· ^			0.11882	0.15565	O. TARRA	0.40514
				•				10340	70770	177 00 C	27070
		4 3			. 4			20,27,0	4774	7777	72.77.0
					•			71720			
	_	E 4		•	- ^			74770		10071	1200
	_	۲:			· -				07.7.0	1001.0	******
	しょうしょうとくしょ マン・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・	٤:		:.				67676	40404		
FIND CAP		<u>د</u>			. <u>c</u>			1010	197.2.5 197.2.5	0 54783	70101
	RE LEADSTORMER/COLL			•				*0674-0		201100	0.0000
200	CONNECTOR			.	•			600000	2000	20.00.	DI 2007

THIS DOCUMENT IS RESTOUGHTLY PRACTICABLE.
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SIGNIFIC AT ALLED OF PAGES WHICH DO NOT
REPRODUCE LEGIBLY.

	186 20		.3) (f.R.4)	10. 2 21.10993 24.05401	21,10903 24,05480
	ERATURE R	E - 184 ABJ T	(F.R	21.109	21.1
	INTERNAL TEMPERATURE RISE	(f.R.4) AIRBORNE,IMMABITED S4. BEGREES C	(F.R.2)	20.62199	20,62199
))			REV ERIOR (F.R.1) (F.R.2) (F.R.3)	18.42584	18.42583
2/26/76	:	. INKABIT	ERROR		=
DATE .	HOARD FRONT END	(f.R.3) AIRMORNE, IMMABITED 30 Degrees C	REV		
EGUIP	HOARD	(F.A.3) 30 PEG	PERCT OIT F.R. STRESS SOURCE		
RBORNE	301	-16	710	~	
BASIC A	ANGLE REC/PROC	OU NE,INHABI	56801	•	
COUIPMENT BASIC AIRBORNE EQUIP DATE , 2/26/76 AEV	SUBASSEMBLY ANG	(F.R.2) ASPHORME, INHABITED 25 DEGREES C	MON-STO		L ARE.
	SUBA	=	PART	(3)	HIS LEVE
CONTRACT MLS PROGRAM	ASSEMBLY ACTIVE EQUIP	EKVIRINWFRI/ITMPERATURE CONDITION PAIRS (1.R.1) Airhorne-Immahited (f.r.2) Ai O degres c	CKI PART PART MON-SID PERCI GIV F.R. REV ERROR (F.R.1) (F.R.2) (F.R.5) (F.R.4) SYMBL DFSCR (F.R.1) (F.R.5) (F.R.4)	OICDE (UR MIXER) (21)	TOTAL FAILURE PATES FOR THIS LEVEL ARE
CONTR	ASSEN	E X 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	CKT PART		TOTAL

COLTRACT	ACT MLS PROCRAM	OC RAM		EQUIPPENT B	BASIC AIRBORNE EQUIP	t Equip	9140	2/26/76	AEV			
ASSENDLY	bly ACTIVE EQUIP	EGUIP	SUBASSE	SSEMULY ANGLE	E REC/PROC	POARD		HOBULE	1141	INTERNAL TEMPERATURE	ATURE RISE	92
2 × 1 × 2 × 2 × 2 × 2 × 2 × 2 × 2 × 2 ×	VIRORMFMI/TEMP .m.t) Airporne U Degrefs C	KVIROWNFM1/TEMPERATURE CONDITION P. F.R.1) AIRPOENE, IMHARITED (F.R.1) (1 DEGREES C	MB 1 T 1 OM (F.	ION PAIRS FOLLOW (F.R.2) AINBORNEJNHABITED 25 DEGREES C	. INHABITED	30 PEGI	R.3) AIRRARN Degrefs C	(f.R.3) AIRPORME,IWHARITED 3U DEGREFS C		(F.R.4) AIRBORNE, INHAPITED 54 DEGREES C	TRHAP I TED	
CKT	PART L DESCR		FART	DN-ST	PERCT OTY STRESS	F.R. SOURCE	REV	ERROR	(F.B.1)	(1.8.2)	(1.8.3)	(4.9.4)
=======================================	GUARTZ CRY	CRYSTAL		FILTER YTAL	b. 6	: : : : : : :	; ; ; ; ; ;	7 1 1 1 1 1 1 1	1.24000	1.2000	1.20000	1.26000
~	HUNRIZ CHYSTAL	TAL							0.2000	0.2000	0.2000	0.2000
•	MICRUTLEC.	LINEA							0.50156	D. 00.0	1,7025	1.16554
A 7 - A 6	MICROELEC.				• -				0.48118	0.53006	0.55535	0.86356
3 3	MICROELEC	. SS1/HS1							0.26025	0.27031	0.27383	0.36.393
S i	MICHOELEC.	. SS1/#S1			- •				0.43200	0.45772	0.46673	\$1175.0
` •	MICRORLEC.								C.00.0	9001	255.0	20101
- V	MICROFICE.	LINEAR							0.49751	0.54870	0.57518	0.92941
	MICRUFLEC.	LINEA							0.48118	0.53006	0.55535	0.89156
90				-	.0				0.26025	0.27031	0.27383	0.30303
÷;	TRAUS ISTOR	(81)	Z Z	•					25692.0	0.35705	C.37696	67027.0
7 ·	FF T		1		27.				1.21695	7.59750	46776.	5.5277
÷ =	TRANSISION OF THE CASE		2 4						0.07368	0.12514	0.13792	0.21374
	DIOPE CAN	IYER)	(21)						35.81063	40.08663	41.00759	15602.94
~	TRANSISTOR (SI)	(18)	# D &		7. 4				0.33906	0.45499	0.48100	(1.62427
C 1 3	TRAHS ISTOR	(21)	102						0.14075	0.18819	0.19886	0.25705
7-283	D100E (2FN		9						17770	0.47486	1.01552	14/27-1
2 -		KESISTOR (FIXED-COMP)	200		. ~				0.00108	0.00259	0.00.00	0.00718
K.2.	_	RESISTOR (FIYED-COMP)	# C #						0.00063	0.00154	0.00184	0.00434
m Z	_	STOR (F1 XED-COMP)	RCR		-				0.00052	0.00125	0.00148	0.00344
*	Pt S1	STOP (FIXED-COMP)	E .						0.00317	0.00762	80600.0	0.02109
^ 4	× 0	SISTOR (FIRED-COMP)							0.00092	0.00232	0.00279	0.00478
	RESI	STOR (FIXED-COMP)	 		1. 10				0.00519	0.01246	0.01484	0.03442
£	RF S 1	STOP (FIXED-COMP)	R C P		۶.				0.00056	0.00175	n.n0161	0.00375
# 1 C	RESISTOR (F	STOR (FIXED-COMP)	2 E		- ,	•			0.00052	0.00125	0.00148	0.00344
= :	RESISTOR(1	SISTOR(FIXED-COMP)	2 3 CE		. •	•			0.00058	0.00140	0.00167	0.01591
2 - 4	Brststane(6	STOR (FIXED-COMP)		•	10.				0.00061	0.00148	0.00177	0.00416
81418	RFS	IXED-COMP)	202		1, 2				0.00104	0.00249	0.00297	0.00488
R1519	RE SI	STOR (TRIMBER)	E.J						18.65158	20.31212	20.78081	24.03350
k1617	REST	STOR (FIXED-COMP)	ه د ع						G.00622	0.01495	0.01781	0.04130
R 2 U 2 1	RESI	STUR(FIXED-COMP)	۵ رو د د		· ·				0.00622	0.01495	0.01781	0.04130
27.0	1010	STORICE VER-COMP.)	. a						0.00092	0.00712	0.0074	12 YOU D
478	RESISTORUE	STOR(FIXED-COMP)	A						0.00052	0.00125	0.00148	0.00344
C1028	CAPACITOR (CITOR (CEPAMIC)	ž	•					0.56509	0.60596	0.61449	0.65709
C1119	CAPACITUR (CERA:41C)	CERASIC)			20.				•	0.36780	0.31170	0.33167
5113 5	CAPACITOR								0.14297	0.18730	0.20321	0.36717
= :	CAPACITOR (DIP.	O IP. MICA	5 3						0.03781	0.201.0	0.12629	0.53744
2112	CAPACITOR (CERAMIC)	CERAMICS	5 2						0.2073	14441	12041	7 5 6 7 6
71171	CAFALI IVE	/ 3 T L W L 1 1 1	:		:						10035.0	***************************************

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THE CORPORATION OF THE PROPERTY PRACTICABLE.

SIGNIFICATION OF THE PROPERTY OF TH

COUTRACT MLS PROCERA		EQUIPMENT	HASIC AIRBORNE	41003	914	2/26/76	REV			
ASSERILLY ACTIVE CRUIP	SuB	SUBASSEMBLY ANGL	ANGLE REC/FROC	HOVE	F. T.	MODULE	INTE	INTERNAL TEMPERATURE	ATURE RISE	02
EDVINORM FYT/TERFERATURE CONDITION FAIRS (F.R.1) AIRGARE/IMMABITED (F.R.2) A L DEGREES C 25 DEGRE	0M01T10		FOLLOW Rborne, imharited S c	(f.R.3) AIR 3U DEGREES	AIRBORN Ees c	.3) AIRBORNE, INHABITED Degrees C		.4) AIRFORNE-INNABITED DEGREES C	INN ABITE D	
PART	PART	NON-STD PART NO.	PERCT OTV	F.R. SOURCE	2	ENROR	(F.R.1)	1 =	(6.8.3)	(1.8.4)
CA15 CAPACITOR(CERABLE)	×	1 1 1 1 1 1 1 1 1 1	11.	# 	! ! !		0.08468	0.09081	0.09208	0.09247
	ž		15. 3				0.25087	0.26713	0.27051	D.28732
	ž						0.07433	0.07915	0.08015	0.0#513
C224 CAPACITOR(CERAMIC)	3 3		30.				0.44599	0.47490	04027.0	0.51679
			_	•			0.02587	0.03095	0.03260	0.04668
							0.24865	0.26663	0.27038	0.24913
	: 5						0.15268	0.16257	0.16463	0.174.6
	ž						0.24405	0.26170	0.26538	0.2737
	ž						0.15144	0.16066	0.16257	0.17206
	ž						0.14234	0.15100	0.15280	0.16172
	2	_	~ `				0.06462	0.13783	0.16038	0.11190
_	3	•					0.14247	0.15115	0.15295	0.14187
	3 3		•				0.07495	2/2/0°C	6/080.0	0.08581
C10C3 CAPACITOR(VANIABLE)	ב ב						0.12202	2.130.55	0.11260	0.141.0
9	: :	÷	24. 2				n.24405	0.26170	0.26538	0.28178
	ž		5.	•			C.08108	0.08694	0.08616	0.494
	ž		15.				0.07572	0.04033	0.08129	0.0*605
	ž		24.				0.11239	0.11967	0.12119	0.12872
	:		 				0.08362	0.08904	0.09017	0.09577
(25 CAPACITOR (CERAMIC)	5 3		76.			•	0.0776	0.06055	0.08129	2.080.0
	5 3						17176	71781 0	0.10330	2,007.0
	; :		24.				0.12202	0.13085	0.11269	0.14140
			0.				0.56827	0.93455	1.03076	1.65102
J2 CORNECTOR			0.				0.28414	0.46727	0.51538	0.82551
COLNECTUR			0.				0.07326	0.13874	0.15653	0.27242
			0. 3				0.86356	1.41953	1.56563	2.50.10
*							0.04230	0.04951	0.05178	0.07032
¥							0.16922	0.19804	0.20713	0.2#129
÷:							0.12691	0.14853	0.15535	0.210%
*							0.240.0	0.04951	0.05178	0.07032
*							0.08461	20660-0	0.10356	0.14064
U10 RF IMANSFORMER/COIL							0.04230	0.04051	0.05178	0.07032
						;				
TOTAL FAILURE KATES FOR THIS LEVEL ARE.	HIS LEV	EL ARF				2.	72.74096	82.15200	84.56007	101.4971

CONTRACT MLS PROGRAM		EQUIPMENT	INT BASIC ATRBORNE FOUIP	RBORNE		DATE	2/26/76 REV	REV			
ASSEMILY ACTIVE EQUIP	ens	SUBASSEMPLY ANGLO	ANGLE REC/PROC	90	BOARD	BOARD MAIN FRANT	THANT	IMI	INTERNAL TEMPERATURE RISE	IATURE RISE	20
ENVIRONMENT/TEMPERATURE COMDITTOM PAIRS FOLLON (F.R.1) AIRHORNE,IMHAUITED (F.R.2) AIRBORNE, U DCINEES C 25 DEGPEES C	E CONDITTO ITED (F	ITON PAIRS FOLLOV (F.R.2) AIRBORNE 25 DEGPEES C	FOLLOW Irborne, Inhabited Es c	160	(F.R.3) 30 0E6	Albenber Refs C	(F.R.S) AIRBORNE, INHABITED 30 DEGREES C	FD (F.R.	(F.R.4) AIRBORNE, INNABITED 54 DEGREES C	INMARI TED	
(KI PARI PARI NON-SID PERCI GIV F.R. REV ERROR (F.R.1) (F.R.2) (F.R.4) SYMBL SYMBLE CODE	PART	KOK-SID PARI KO.	PERCT STRESS	PERCI GIV F.R. STRESS SOURC	F.B. Source	» » »	ERROR CODE	(F.R.1)	(F.N.2)	(F.R.3)	(4.4.4)
CORNECTOR CONNECTOR CONNECTOR					• • • • • • • • • • • • • • • • • • •	; ; ; ;		0.43178 0.08115 0.38267	0.70977 0.15368 0.72472	1 0.43178 0.70977 0.78281 0.08115 0.15368 0.17338 1 0.38267 0.72472 0.81764	1.25405 0.30231 1.42563
TOTAL FAILURE RATES FOR THIS LEVEL ARE	IN THIS LEY	YEL ARE	•				0	0.89559	1.58R16	1.77383	2.97192

THIS DOCUMENT IS PERFORMED FOR THE ALICABLE.

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					APA
			(F.R.4)	5.60200	19.14684
	ATURE RISE	I MH ABI TEÐ	D PERCY ATY F.R. REV ERROR (F.R.1) (F.R.2) (F.R.5) (F.R.4) D. STRESS	5.60200 5.60200 5.60200 5.60200 4.55376 7.64209 8.44574 13.54487	14.04774
	INTERNAL TEMPERATURE RISE	(f.R.4) AIRBORNE,IWHABITED 54 DEGREES C	(F.R.2)	5.60200 7.64209	13.24408
B E <	<u>=</u>		(F.R.1)	5.60200 4.55376	10.15575
2/26/76 RFV		LINHABI	ERROR		7
DATE		Alrborne IES C	REV ERROR CODE		
FOULP	BOARD	(f.R.3) AIRBORNE, IMMABITED 30 DEGREES C	F.R. SOURCE		
RBCRNE	121		PERCT STY F.R. STRES		
ASIC AI	AMTENNA SUBSYST	FOLLOW RHORNE, INMABITED S C	D PERCT OT	. .	
EQUIPMENT BASIC AIRBORNE EQUIP DATE	SUBASSEMBLY ANTER	TION PAIRS FOLLOW (F.R.2) AIRHORNE, 25 DEGREES C	NOK-SID PART ND.	BIODE SVITCH	L APE
	SUBA	WB1710M	PART 1YPE		IS LEVE
CONTRACT MLS PROGRAM	ASSEMPLY ACTIVE EQUIP	ENVIRUNMENT/TEMPERATURE COMBITION PAIRS (f.R.1) AIRNORME, IMMAGITED (f.R.2) AI U DEGKEES C	CKT PART FART NOW-ST SYMEL DESCR TYPE PART M	TASERTED COMPONENT DIODE CONNECTOR	TOTAL FAILURE RATES FOR THIS LEVEL APE

ASSEMBLY ACTIVE EQUIP	t Equip	SUBA	SUBASSEMBLY COMI	CONTROL PANEL		BOARD			181	INTERNAL TEMPERATURE	ATURE PISE	92
ENVIRONMENT/TEMPERATURE CONDITION PAIPS (f. R. 1) AIRPORNE-INHARITED (f. R. 2) A is degrees c	MFRATURE CON Nejinharited	61110A (f.	JON PAIPS FOLLOW ' (f.r.2) Atrborne,imharited 25 degrees (DV ' VE , I NIIAR I TE	<u></u>	(f.R.3) AIRRO 30 degrees c	A TRRORNE	(f.R.3) AIRPORNE, INHABITED 30 DEGREES C		(f.r.4) AIRBORNE/INNABITED 54 Degrees C	TWA ABITED	
CKT PART		PART	HON-STD PART NO.	PERCT 6	917	F.R. SOURCE	REC	ERROR	(F.R.1)	(5.4.2)	(F.R.2) (F.R.3)	(7.8.4)
					-				A 16135	15.1448	19.45741	71.RR25P
*	> 1	٠		•	• ^				1.27884	3.22623	4.16056	15.52290
ŝ					۰ ۸				1.59461	1.75268	1.80304	2.26667
	101/101			; ;	٠,				1.46596	1.60159	1.64909	2.04262
UVUIU MICKOELEC.				• e	, 10				0.78074	0.81092	0.82150	90000
UIT-) MICHOLIEC.				: c	-, ۱				0.30171	0.31495	0.31959	0.35200
					•				0.26025	0.27031	0.27383	0.30103
	101111111111111111111111111111111111111			•					0.58757	0.65204	0.68539	1.13150
ביים עונעניניני					-				0.52891	0.58464	0.61347	1.999 P.
UI/ MICKUELEC.		4		.			_		0.14226	0.20216	0.21573	0.29012
RC-0102404		. 0		Ş	-				0.56896	0.56896	0.56896	0.56896
	•	L 9		-					0.05879	0.15619	0.18795	0.47438
	(15)		_	-	_	•			0.05542	0.09799	0.10872	0.17259
RESISTOR	RESISTOR (POT-COMP)	2		70	_			-	1.00037	14.22634	15.23927	23.72709
E1 RESISTOR	MESISTOR (FIXED-CORP)	# C #		'n.	-				0.00054	0.00129	0.00154	0.00359
	RESISTOR (FIXED-COMP)	PCR		.	-				0.00061	0.00148	0.00177	0.00416
	RESISTOR (FIXED-COMP)	BCB		-	-				0.00057	0.00137	0.00163	0.00379
R4 RESISTOR	RESISTOR(FIXED-CORP)	202		-	-		•		0.00057	0.00137	0.00163	0.00379
	RESISTOR (FIXED-COMP)	PCR			-				0.00054	0.00129	0.00154	0.00359
R7 RESISTOR	STOR (FIXED-COMP)	# <u>2</u>		۳.	-		•	=	0.00054	0.00129	0.00154	0.00359
RFS1	RESISTOR(FIXED-COMP)	RCB		۳.	-				0.00054	0.00129	0.00154	0.00359
	STOR (FIXED-COMP)	20		*	-				0.00059	0.00143	0.00170	0.00399
1544	DECISION (POREN-FILM)	2 2 2		,	-				0.00686	0.00.58	0.00898	0.01113
	(X 1) J-8 J700) 601 V1 V 3	3		**					0.00679	0.00848	0.00887	0.01098
				-	_				0.00043	0.00199	0.00237	0.00551
					_				0.00052	0.00125	0.00148	0.00344
	7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			7	-				0.00058	0,00140	0.00167	0.00391
	COLUMN TOCKIE / DB	E ,		: -	· p=7				1.26000	1.26000	1.26000	1.26000
A21107	COLLES BOTABLES				•			~	98.49598	98.49598	86567.86	98.49598
					-				0.26981	0.51098	0.57650	1.00518
				6	_				0.24516	0.46430	0.52383	0.91435
LAWA.	LAFP. INCANDESCENT			; ;	9			_	16.00000	16.00000	16.00000	16.0000

THIS DOCT THE IS DEED DUBLITY PRACTICABLE.

THE COPY & STITUTED TO DUSC. TAINED A

STONIELOUS DEED DE PAGES WHICH DO NOT

HEROLOGE LEGISEY.

2		(F.R.4)	.6013	.54991	24271	.99452	.49863	. 49843	.4n252	2445	0.5567	82170	0.29742	.27516	.54991	34.05096	61.910.5	10015	94578	.29704	702621	.63864	2.58275	*****	11685	0.00	71160	.77244	.00001	.32114	. 55070	2000	.21000	452.97570
		(f.n.3)	.54333 0	۰ ۵	.67836		•	1.85642 2.		7 16891.7	. 38145	19786 12	.25821	.44941	99677		10.39893 61	.44756 .48477	.72705 0	.17699			.12990	2 . 90,000	28021	03472 0	03978	•	.00001 115	•	7.54900	Alore	21000	241.46798
INTERNAL TEMPERATURE RISE		(F.R.2)	0.52595	0.43695	78048.0	7.09934				791136	0.17177		0.25323		0.43695		1 29966.21	0.43643 0.45652	0.69926	0.16221	5221		7,010.1	0.61733	0.28316	0.02912	0.03333	0.71234	115.00001 11	3.28650	7.65/46	0.000	0.21000	221.79745
>		(F.R.1)	0.47364	0.39678	0.7260	6.12100	1.53025	1.53025	0.30799	1.43686	305975	11040	.23830		.39878	2.23036	07550.4	0.3787.0	0.61596	0.11240	0.11240	19.66854	0.76156	702070	0.26502	0.01207	C.01375	0.66429	115.00001	1.79619	0.67632	1988	0.21000	174.0033R 2
2126/76	78E, 1	CODE																																1.
GUIF DATE	R.3) AIRRO Degres (1							.•															·	•			•					٠
RNE F		- N	-	• ·	- •	- **	0. 2	~		٠.		,		o. 2		٠.	•	•	-	53. 1		5. 184						5. 5	=	72 2	•			•
Y S	FOLLOW Rhorne, 1N S C	0 PE												-	•		-/*			'								52						•
EQUIPPE SUBASSEMBLY	11104 PAJRS (F.R.2) A 25 DEGREI														-	-				#4#	202	Z				80.8	Z	×						LEVEL ARF.
7 4 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	ENVIRONME-AT/TEMFERATURE CONDITION PAIRS (f.w.1) Aimforme.imharited (f.m.2) A u decuees c			151/HS1	SSI/MSI	551/R51	\$51/#S1	SS1/MS1	SS1/HS1	\$51/HS1	581/H51		SSI/HSI		SSI/HSI	•		201/100	15H/15S				LISE AR		1587155 5517851				DE SCENT	•			TOGGLE /PR	TOTAL FAILURE RATES FOR THIS LEVEL ARE
CONTRACT MLS PROGRAMASSEMBLY ACTIVE EQUIP	ENVIRONMENT/TEMPERATURE CO (f.m.1) Aimforme, immanited u degwees c	ART ESCR	1			MICKOFLEC.					MICHOELEC.					ROP MENORY	HOT BEHORY							MICHOFIEC.		-	RESISTOR (FIXED-COPP)	CAPACITOR (CERAMIC)	LAFF. INCARDESCEN	COHNECTOR			SWITCH, TOG	FAILUNE RAT
CONTRACT	ENVIRO CF.R.1 U DFC					US-12		20		=	77	~		2			0.5%0			14 5B	04.88		_				_	•					-	TOTAL

CONTRACT MLS PROGRAM		EGUIPHENT	SMALL COPM AIRE EG.	A A B		DATE	3126176	> =			
ASSEMBLY ACTIVE EQUIP	SUB	SUBASSEMPLY ANGI	ANGLE REC/PROC	2	BOARD	DIGITAL PROC	T PROC	=	INTERNAL TEMPERATURE FIST	BATURE FIST	2
ENVIRONMENT/TEMPERATURE COMBITION PAIRS (f.m.1) AIRBORNE, IMMABITED (f.m.2) A O DEGREES C	E CONDITION (F.		FOLLOW Irboane, inhabited Es c	.	(f.m.1) AIRBO 30 Degrefs C	AIRBORNI Iefs c	(f.m.)) AIRBORNE, INHABITED 30 Degrees C		(f.a.4) AIRBOPHE, IMHAPITED 54 Degpees C	. 1 hh a p 1 7 E b	
	PART	NON-STD PART NO.	PERCT OTY STRESS	•	F.R. Sounce	RE	ERROR CODE	(F.R.1)	(f.R.2)	(F.F.3)	(4.9.4)
ANCHOLIST TO STATE OF THE STATE	i 		0	-	9	• • • • •		25.00070	25.00000	25.00000	25.0000
				~				7.34796	9.65762	10.42137	16.433.5
BOR REBORY			•	~				26.58851	34.17202	36.70162	56.61305
MICHOELEC. SSI/MSI	15		•	_				1.07505	1,16763	1.20:006	1.46.60
				_		7		1.43042	1.56454	1.61152	2.0000.5
	15		ċ	m				2.02505	2.14323	2.15.462	2.57751
			•	-				0.70675	0.74%	76.465	といってる。()
	=======================================		÷	-				1.11868	1.21.23	1,25310	1.54100
	22		0	~				2.70007	7.85764	2.01283	1.37601
				•			-	7.09966	17.97769	23.196.1	34.65.44
MICROELEC. SSI/MSI	21		ö	~				1.78410	1.91568	1.06177	2.34357
MICROELEC. SSI/MSI	21		6	~				1.A6596	1.96757	2.00316	16102.5
MICHOFLEC. SSI/MSI	21		•	_		•		0.89205	0.95724	G.944.P9	1,17175
MICROELEC. LINEAR	•		•	-				0.96739	1.04895	1.12408	1.81162
MICROELEC. SSI/MSI	21		•	-				1.13946	1.24242	1.27K4P	1.57720
	23			-				0.41639	n.43249	0.43713	7.7.7.0
	11			-				0.41639	0.43249	0.43*13	7.7.7.0
MICROFLEC. SSI/MS	1		.	-				0.41639	0.43249	0.43213	7.7.7.9
CAPACITOR(TANT. EL.) CSR	EL.) CSR		30.	-				0.00405	0.00963	0.01014	0.01452
CONNECTOR			•	-				0.30936	0.58549	6.46101	1.152%
QUARTZ CRYSTAL			•	-				0.20000	0.20000	00002.0	0.21.110
TOTAL FAILURE RATES FOR THIS LEVEL ARE.	THIS LEV	EL ARE					88	83.52258	105.75352	114.78056	201.5:456
		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	•				1	, , , , , , , , , , , , , , , , , , ,	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		

THIS ROUTHING IS PEUT NUABILY PRACTICABLE.

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SIGNETICHNI NURSEN OF PAGES WHICH DO NOT
PERFONDE INSIDIX.

CONTRACT NLS PROGRAN		EQUIFAENT	SMALL COMM AIRB FG.	M AIRB		. 1110	2/26/76	P £ ¢	·			
ASSEMBLY ACTIVE EQUIP		SUBASSENBLY ANGLE REC/PROC	LE REC/PRO	ي	BUARD	PROCESSOP 1/0	0/1 40	INTE	RNAL TE	INTERNAL TEPPFRATURF KISF	KI ST	ž
ENVIRONMENT/TERPERATURE COMBITION (F.R.1) AIRBORNE/INNABITED (F. 6) DEGREES C 25	RE COMPITI	100 PAIRS FOLLOW (F.R.2) AIRBORNE,IWHARITED 25 DEGREES C	DV LE, INHABIT		(f.R.3) AIRBOI 30 degres C	AIRBORNE Fes c	.3) AIRBORNE, INHABITED Degres C		F.R.4) AIRPOL 54 DEGPEFS C	(F.R.4) AIRPORME, IMHARITED 54 DEGREES C	.	
CAT PART SYMBL DESCR	34A1	HOR-SID	PERCT DIV		F.A. Source	> 14	ERROR	(f.a.1)	(F.B.2)		(f.R.3)	A. 97)
	111111111		6	-	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2.46454	6.05859	7.77.296	296	28.75303
AND MORAL PACE				- ,-				1.02308	2.581.98			12.41"32
	**		ò	۰ ۰				7.89834	P.95667	•		16.57.13
MICROFIEC	A E		0	_				0.96239	1.06795		,	7517371
MICHOELEC.	- W			•				4.66353	5.21952		717	9.35437
MICROELEC.	HSI		ö	•				3.56819	3.73136		354	4.68713
MICROFLEC.	HS.		0.	_				0.70675	0.74963		465	0.5791.5
	HSE		•	-				0.89205	0.957#4		786	1.1717
MICROCLEC.	HSI			-				0.5P1N2	0.61175		224	6.71.911.
	HSI		•	~				5.26044	5.70544		121	1.15249
RAP MEMORY			ċ	_				1.77491	4.49442		420	21.6666
	HSI	•		-				1.07545	1.16763		979	1,46,69
MICHDELEC.	HS I		•	~				0.96547	1.00784		248	1.14.40
UP MICROFLEC. SSI/MSI	HSI		=	-			,	0.41639	0.43549		513	7 .7 .7 .0
D MICROFLEC.	MSI		e •	-			•	0.96869	1.04521		<u>ار</u>	1.20464
U12 MICROELEC. SSI/MSI	MSI		•	-				0.41639	0.43249			7 . 7 . 7 . 0
_	NS I		•	-				0.0000	0.0000		3	+ . Dist. 1.1.
MICHOELEC.	¥		•	-				0.96239	1.06795		£0%	1.84147
MICROELEC.	HSI		•	- ·				U.4K273	0.50392		77	2/5-0
	_		• ;	- 1				6,176.0	5 T C C C C C C C C C C C C C C C C C C	-	77.6	
			:	~ •				C. /8662	1.49655		G :	
\$100E (S1)			<u>.</u>	• (0.30473	100100			
RESISTOR (FIXED-COMP)		•	· ;	12				7, 400.0	3/ 10° 0	71310.0	2	71740 H
9ES1S108(#14EB-C08F)			;	• (0.000				
AES 15108 (71289-CORP)	COMP) RCB		, ,	2 <				0.00538	47.47.00 0.005.00		9 9 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	5 0345
これのこうのはでんと思るころころはは			:;	•							?	
BESISTOR (FINER-CORP.)				~ -				0.00184	707070	75.00.0		2.20.0
			•	u r				20000			***	
			-	~ ^				0.01329	0.01558		77.	0.01162
/ E3F/-E3A-3/40F31434	Coke Coke			- 2				0.00726	0.01744		22.)	11-11-11
			6	-		•	•	0.25732	0.487		14675	0.9 864
							P.	40640			2100 / 73	
TOTAL FAILURE MATES FOR THIS LEVEL	OR THIS L	EVEL ARE	:				•	37.07334				

### 1008-510 1018-510 1018-510-510 1018-510-510 1018-510 1018-510-510 1018-510-510 1018-510-510-510-510-510-510-510-510-510-510	Control Cont	CONTRACT	ICT MLS PROGRAM	SRAM		EQUIPMENT	SHALL COMM AIRM FO.	AIRN FO.	DATE	2/26/76	A7.			
		A S S E ME		1101	2005		F REC/PROC	UOARD	FOVER	SUPPLY	2	FORAL TEPFIN	NATURE PISE	*
		6 . T	DMAFNT/TEMPE! 1) AIRBORE/! [GREES C	RATURE COA Inhabited	911161	=	L. INHABITED	300	AIRHARA RFES C	16 . I NH AR I T	÷.	4) AIRFORNE. FGPEES C	, THEAPTIFP	
		CKT	PART	1 /	PART	MON-STP PART NO.		;	256	E 2 2 0 2 C 0 3 E	(6.4.1)	(6.2.2)	(F. H. 3)	
MARKED M	MANURAL (1) MANU	5	MICROELEC.	LINEAR		· · · · · · · · · · · · · · · · · · ·	9.	-		; ; ; ; ;	0.84626	0.93542	0.07455	1.50.1
MANISTRE (11) MAY		711		LINEAR			•	_			7.2449.0	0.75752	C. 78 x 0 \$	1.26.13
		-		(51)	2 i			- 1			0.51296	0.69473	Jo / 2 / 9	1.0.1
		~ :		(25)	e i		j,	,			7.	7525	20,474	201010
Control Cont		۳ ر ت			2 1		, .				10100		2777	76476
Colored Colo		•					; ×	• •			0.15161	2.1072	0.21114	1.77.0
1	1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,) 9		(15)	2		25.				0.15161	0.19781	0.21004	11.27.19
10.00 (1006 (ERF) 6	~		(21)	2		<u>-</u>	_			U. n9983	0.13422	0.14192	11.174.75
1006 (10.00 (51) (51) (52)	3	(55) 300		6.0		23.	•			C.51997	0.73487	11,01743	1. 35 2 3 3
1006 (S1)		~ = 3		ER)			-	_			C.33147	0.41244	£5.47.3	0.51871
1000	100E (S1)				4 .9	•	-	_			0.05542	05/61)*0	0.167.72	0.17250
					4 9		37.	- 1			0.17259	0.26768	0.29170	271.7.0
		9 5 8			a. (• • • • • • • • • • • • • • • • • • • •	~ (777770	0/259.0	200000	27.6
								~ ~			0.17418	7647.0	37.71	5 7 7 C
					L Q		• ~	•			0.11499	2,202.2	C. 22419	0.745.0
	The state of the component of the comp	CB 23			, 4		:-	. ~			0.11003	0.19598	0.21745	0.34517
RESISTOR(FIRED-COMP) RCR			TRANSISTOR	(31)	RPR			-			0.09943	0.13422	6.14192	0.10405
	NESTSTORICFREE-CORP) RCR	=	RESISTOR (FE)	KED-COMP)	200			- 1			6.00061	0.00142	6.11.17	4.11.41/
RESISTOR(FIRE-COMP) RCR 1. 1. 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		2 :	MESISTOR(FI)	XED-COMP.	# C #						00000	C 100.0	0.5000	44.00° 0
		2 1	DESISTOR (FT)	KFB-COMP)			-				0.00052	0.00125	0.17.0	77.000
		2	RESISTOR(F11	KEB-COMP)	# J		-				0.00052	0,00125	C. PU14P	0.00344
RESISTOR(TRIPMER) R.4 10. 1 1 1 1 1 1 1 1 1		9	RESISTORCFI	KED-COMP)	101		-	-			0.00052	0.00125	4711117	11.611 144
		-	5	IMERI	2		<u>.</u>				5.88156	6.46234	6.42407	7.73401
			RESISTOR (F1)	TED-COMP.								34150.0	771-01-1	77.77
	FESTSTORIFIED-COMP) RCR	1		TED-COMP)			.08				0.00213	0.00577	11.00705	2.01
RESISTOR(FIXED-COMP) RCR RESISTOR(FIXED-COMP)	RESISTOR(FIXED-COMP) RCR RESISTOR(FIXED-COMP)	R1516	RESI	KED-COMP)	5		70.	~			6.00356	0.00051	0.01157	0.67969
#ESISTOR(FIXED-COMP) #C# 40. 1 1 0.00105 0.00125 0.00125 0.00125 0.00125 0.00125 0.00125 0.00125 0.00125 0.00125 0.00125 0.00125 0.00135 0.001	#ESISTOR(FIXED-COMP) #C# 40. 1 1 0.00105 0.00125 0.00125 0.00125 0.00125 0.00125 0.00125 0.00125 0.00125 0.00125 0.00125 0.00125 0.00125 0.00125 0.00125 0.00125 0.00135 0.01137 0.00125 0.00137 0.00125 0.00137 0.00125 0.00137 0.00125 0.00137 0.00125 0.00137 0.00125 0.00137 0.00125 0.00137 0.00125 0.00137 0.00125 0.00137 0.00145 0.00125 0.00137 0.00145 0.001	17	_	XED-COMP)	#C#		20.	-			0.00073	0.001*0	0.60216	0.00515
		121	_	XED-COMP)	ı		, 0,	_			70100.0	0.1111.266	11.06.521	(. ()) ()
RESISTOR(FIXED-COMP) RCR RESISTOR(FIXED-COMP)	RESISTOR(FIXED-COMP) RCR RESISTOR(FIXED-COMP)	175	NE S1	XED-COMP)	=		- ;	-			0.00052	0.00125	1,00145	0.00.44
RESISTOR(FIXED-COMP) RCR 4. 1 RESISTOR(FIXED-COMP) RCR 4. 1 RESISTOR(FIXED-COMP) RCR 1. 101155 0.001	RESISTOR(FIXED-COMP) RCR RESISTOR(FIXED-COMP)	23	RE SI	XEB-COMP.	¥ (<u>.</u>	.			r.nnr.1	27101.0	27 Lu. 1 10	11 7000 10
RESISTOR(FIXED-COMP) ACR 1. 1 1 0.00052 0.00175 11.61142 14.51142	RESISTOR(FIXED-COMP) RCM RESISTOR(FIXED-COMP) RCM 1. 1	\$2E	16.51	KED-COMP.			- 4				0.00055	2100.0	5 to 1	(1) . (1) . (4) . (5)
RESISTOR(FIXED-COMP) RCR 1. 1 1 0.00052 0.00125 0.0014: RESISTOR(FIXED-COMP) RCR 2. 1 1 0.00052 0.00124 0.24727 0.2014: RESISTOR(FOWER-FILM) RNR 2. 1 1 0.00057 0.000429 0.001	RESISTOR(FIXED-COMP) ACR RESISTOR(FIXED-COMP) ACR RESISTOR(FIXED-COMP) ACR RESISTOR(FOWER-FILM) RNA RESISTOR(FOWER-FILM) RNA RESISTOR(FOWER-FILM) RNA RESISTOR(FOWER-FILM) RNA RESISTOR(FIXED-COMP) RCA RESISTOR(FIXED-COMP)	24		150-COMP3			; <u>.</u>				E. 00052	0.19125	13. Cit 16.9	772 (1)
RESISTOR(FIXED-UU) REGUG LU. 1 0.10124 0.24522 0.24151 RESISTOR(FIXED-UU) REGUG 1. 1 0.00154 0.24522 0.24151 0.00155	RESISTOR(FIXED-UW) REGUG	812	RESISTOR (F1)	KED-COMP)	2		: . :		•		0.00052	0.00125	£.014:	0.00344
RESISTOR(FIXED-COMP) RCR RESISTOR(FOWER-FILM) RNR RESISTOR(FOWER-FILM) RNR RESISTOR(FOWER-FILM) RNR RESISTOR(FIXED-COMP) RCR RESISTOR(FIXED-COMP)	RESISTOR(FIXED-COMP) RCR RESISTOR(FOWER-FILM) RNR RESISTOR(FOWER-FILM) RNR RESISTOR(FOWER-FILM) RNR RESISTOR(FIXED-COMP) RCR RESISTOR(FIXED-COMP)	R27	RESISTOR (FI)	KED-UU)	RE 6UG		02	_		_	0.10124	11.24.22	0.27.151	1.376.5
RESISTOR(POWER-FILM) RAR 2. 3 0.001672 0.00439 0.04 P77 1.04 P77 1	RESISTOR(POWER-FILM) RMR 2. 3 0.001672 0.00439 0.04 P77 RESISTOR(FIXED-COMP) RMR 3. 3 0.00167 0.00717 0.04 P77	131	RESISTOR (FI)	KFD-COMP)	1 0		:	_			0.00052	0.00125	ווייטועה	77.100.11
RESISTOR(POWER-FILM) RMR 1. 1 0.00745 0.007470 C.1177.	RESISTOR(POWER-FILM) RMR 1. 1 0.00745 0.00747 0.10777	R32	5	VER-FILM)	Z Z		? .	_			0.00672	0.00×39	(; or 977	
RESISTOR(FIRED-COMP) RCR 1. 11 C.10057 C.10167 C.10165	RESISTOR(FIXED-COMP) RCR 1.11-11-15 C.100157 C.1011-15 C	233	3	VER-FILM)	E i			- 1			0.00445	0 2 4 7 0 ° U	2.74 F. C	0.61471
RESISTORIENCE CORP. RCR 3. 1 C. CCCS 0.00137 0.0114.5 RESISTORIENCE CORP. RCR 7. 1 C. CCCS 0.114.57 (14.7 RESISTORIENCE CORP. RCR 7. 1 C. CCCCS 0.114.57 (14.7 RESISTORIENCE CORP. RCR 7. 1 RCR 7. 1 C. CCCCS 0.114.57 (14.7 RCR 7. 1 RCR 7.	RESISTORIFIAED-COMP) RCR 3. 1 0.00057 0.0011.5 PESISTORIFIAED-COMP) RCR 3. 1 0.00157 0.0011.5 PESISTORIFIAED-COMP) RCR 3. 1	4 2 4	= :	MER-FILED	¥ .						1.100.11 7.000.7	20117	2 (C.2) (1)	15115
7 RESISTOR(FIXED-COMP) RCR 3. 3 C. LUGUSZ (1.(1.1.7.2	PRESISTENCE LEGISTE 1. 1 C. LUCIS C. LU	4 7 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		7 E E C C C C C C C C C C C C C C C C C						i	0.00057	25 60 0	0.00163	0.00370
		R 37	RESISTOR(FI)	KED-COMP)			: -				6.00057	0.00137	F.11.10	2

CONTRACT	T MLS PROGRAM		EBUIPRENT	SMALL COMM AINB FB.	KB CO.	DATE	9/142/2	BEV			
A S S E MOL Y	V ACTIVE EQUIP	SUBA	ISSEMBLY ANGLE REC/PROC	E REC/PROC	HOARD	PONER	POWER SUPPLY	1116	INTERNAL TERFERATURE	ATUBE GISE	20
ENVIRONMENT, (F.B.1) AIRI O DEGREES	ENVIROMMENT/TEMPERATURE COMBITION (F.R.1) AIRBORME, IMMABITED (F. 0.0) DEGREES C. 23	M 1110N	FAIRS FOLLOW R.2) AIRBORNE, IMMARITED DEGREES C	IL . I MHAR I TED	(F.R.3) AIRBO 30 DEGREES C	AIRBORN Rees C	(f.g.3) AIRBORNE, INHABITED 30 DEGREES C		(f.R.4) AIGBORNE-IWMARIIFD 54 Degres C	HEAPET P	
CKT P	6 0 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	PART	NON-STO	PERCT 9TY STRESS	f.R. Source	> 14	ERROR	(f.B.1)	(5.8.2)	(f.8.3)	:
R41 RESISTOR	(FIXED-CORP)	#C#	 	13.	Ĭ 6 6 8 1	; ; ;	• • • • •	0.00064	0.00157	0.64188	0.0144
	RESISTOR(FIXED-CORP)	2:		20.				0.00073	0.00180	0.00216	0.00:11
2	CAPACITOS (ALUR, EL.)	: 3		70.				2.67684	4.6737	5.34712	11.5 . 1
:	:	CSB		, O,				0.06190	0.07408	C. N7 B02	0.1117
	CAPAC 110R (CERANIC)	<u>ئ</u>		50.				0.45433	0.48719	70767.0	0.520
3	CAPACITOR(DIP. MICA)	52						0.00540	0.01476	5.017U	27700
	7	283				~		0.00284	0.00339	G. ner 5.7	0.01.51
_	•	CSR		15.				0.00104	0.00175	C.00131	0.01.11
2		×		10. 2	•			0.1673A	0.17949	0.17.02	0.1.4/7
31		¥ :		20.	•			0.10462	0.11217	5,511.0	0.1/16
-	CAPACITOR(IANI, EL.)			20.	-		;	0.04128	0.05000	12.03.00	0.17.4
_	٤٤.)	CS		60.				0.06190	0.0740	0.07802	6.1117
_	_	3		40.				0.54052	0.94375	1.070.1	2.35.92
-	7	2						0.97522	1.70274	1.94.8114	4.21601
(33	TOR (CERANIC)	ž		±0.				0.08369	0.08975	10101	1.00/3
_				- ·	,			n.02820	0.03401	0.03452	0.044
77	POZEN XFAM/FILIEN							0.07870	105501	0.13452	
								0.0250	10770	25770	
								0.02820	0.03301	0.03452	0.044
_	PONER XFMR/FILTER			•				0.02820	0.03301	0.03452	0.011:8
_	POWER XFMA/FILTER			•				0.02820	0.03301	0.03452	0.046.7
_	POWER KFAR/FILTER							0.02820	0.03301	0.03442	0,046.5
_				-				0.03452	0.04767	0.05213	0.00410
12 Pr	POWER XFRR/FILTER			- -				0.03452	0.04747	0.65213	1,000
3	CONNECTOR			•				0.10565	0.19773	0.2226#	D. 375.
TOTAL 64	TOTAL FAILURE RATES FOR THIS LEVE	SLEVE	A ARE				=	18.49953	24.56127	26.40634	7.17

			2000/1000	ROARD	SYNTHESIZER					
	SCBAS	ISSEMPLY AMBLE MELITROL				IZER	=	iatermal tempresting filt	ATURE PISE	Ę
ERVIRONTENT/TENPERATURE CO (4.8.1) AIRBORNE, INNABINED U BEGREES C	COMBITTON IED (F.R	-	PAINS FOLLOW .2) AIRBORME,IMHABITED DEGRES C	(F.R.S) AIRDO 30 PFGRFES C	AJRDORNE IFES C	(f.r.3) AIRDORNE/INHABITED 30 Pforers C		(F.R.4) Alphorme,IMHAPTTED 54 degrees c	IMHAPITED	
CKT PART SYMBL BESCR	PART TYPE	MOK-SID PART NO.	PERCT OIV	F.R.	26.	E R 8 0 R C 0 0 E	(F.R.1)	(f.P.2)	(f.e.3)	(6.7.4)
			0.				1.18215	1.55438	1.75000	4.13957
MICROFLEC.						-	0.41779	n.47331	70200	0.59624
			٥.				0.72560	0.87932	5 65 PR4	7.02747
UZ MICROELEC.			٥.				0.83557	0.94662	10700.	1.77.63
MICROFLEC.							0.74303	0.81748	365.4.3	1.3/113
U6 UB MICROFLEC. SSI/MSI			°.				1.55951	1.67357	2021	
MICROFLEC. LINEA							1.00575	704111	7.87.	
MICHOELEC. LINEA			· ·				*******	3 17173	7 21 26.2	7.4.1
<u>*</u>					•		30130	10. 21157	35700 21	7 17 17 67
BOR BERORY							0.40120	0.71235	0.746.76	0.56616
S MICROELEC.							0.69120	0.73235	0.746.3	0.86616
7 MICROELEC.							0.542.0	1.04895	1.12408	1.84142
A MICKUELEC. LINEA TRANSPERSON (C1)	2		· -				0.06448	0.08637	121.17	11.11 43
			65.				0.22022	0.33018	1.34543	(1.70 51
	. Z		35. 1				1.97190	7.61736	2.71441	3.7731.7
1 2 01008 (S1)	9		15. 2				0.17995	0.29766	0.32672	0.49971
3 91096	a 9						0.60957	1.07787	1.10500	1.80546
_			10.				2.68772	3.60719	3.11227	7 1970 7
CRIS DIODE (VAR/REC/TUN)						•	2.68772	3.60719	3.81277	70 / 76 7
	(21)						44524	60.0200	(1.11.49)	36366
OTT TRANSISTOR (SE)	2 .		25.				0.15161	1884.0	0.717.0	
2							1 01555	1 18152	76.187	7.001.
GIA TARBINION (SI)	E L						0.39898	0.48744	C. 50/ 76	0.613/0
AF 5 1 5 7 6	3 BCB						0.00311	0.00747	1.407.0	0.02015
_	_		-				0.00130	0.06311	F. (1:371	0.00 × 60
			-				0.00052	0.00125	771000	77.00.0
31			÷.				0.00207	40 YOU C	\$ \$ CO TO TO	77510.0
RII RESISTOR(FIXED-COMP)	_						0.00104	0.00.4	10000	
SES SESE							0.00400	0 10623	16.742	12767
MIG MESISION(FIXED-LORP)	E 0 C		-				0.0010	0.00259	0.00.00	0.00/1
							C-00108	0.10259	6, 11, 5110	0.0.73
NOT NESTRICATED AND THE STATE OF THE STATE O	_		30.				0.00087	0.00.0	1,607.1	0.01.446
	2						0.00334	0.00.09	1.10°64	0.1.7.4
BS RESISTOR (FIXED-COMP)	2						C.00087	0.00219	f.14-263	1: 00:434
	Ž.						6.00067	0.00163		C. C. 4 C S
RS9 RESISTOR(FIXED-COMP)	2		•			_	0.002	11.0527	11 5 341	11.61467
RE S 1	Ē						0.00054	0.00129	0.00154	
HE S I	2						70000	60700	70500	0 0117.7
64 RESISTOR(FIXED			•				70,000	0 10001	70707	
67 RE							C - 0000 Z	F.00219		2
77 #E			•				5.65100	15510		
RSC RESISTORCIALITACES							0.00149	5.01 TO	1, 11, 475	17,17
) 							

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THE COPY FIGHTS OF THE THIS A
SIGNIFICANT HITTEL OF PAGES WHICH DO NOT
REPRODUCE THISTY.

CONTRACT	RACT MLS PROGRAM		EGUIPHENT	SMALL COPH AIMP FO.			DATE	5/56/76	> 1			
ASSEMBLY	MBLY ACTIVE EQUIP	SUBASS	ISSEMBLY ANGLE REC/PROC	LE REC/PR	ĕ	8048	STVTHE SIZER	S17ER	7	THIFFHAL TEMPERATURE FISS	ATURE CISE	07
3.0	CF.T.1) AIRBORNE, INMABITED (F.R.2) AIRBORNE (F.R.2) AIRBORNE (F.R.2) AIRBORNE (F.R.2) AIRBORNE (F.R.2) AIRBORNE	611190 (7.	ION PAIRS FOLLOW (F.B.2) AIRBORNE/IWHARITED 25 DEGREES C	SU SE INSARI	9	(f.R.3) AIRPO	AIRFORNI PEES C	(f.R.3) AIRFORME, IMHARITED 30 Degrees c		(F.R.4) AIRPORME/IMIAPITED 54 DEGREES C	, IMIAP I TEB	
CKT SYMBL	PART	PART		PERCT OT) to	r.h. sounce	2	EPROR	(f.R.1)	(1.1.2)	(1.9.5)	(4.1.6)
94		22		-	-			t 1 1 1 1 1	0.00156	0.00 74	0.00445	0.010.1
2	RESISTOR (FIXED-COMP)	# D		:	-				6.00052	0.60125	(,,,,,,	1.11.344
R7172	_	55		:	•				6.00207	0.00497	0.16594	0.01.77
173		RC R		-	-				0.00052	0.00125	0.0014	975.10.0
# 7.4 # 7.4	RESISTOR (FIXED-CORP)	5		9	- ,				C.00149	26:00.0	1.18475	1 - 1 - 1
~	6 RFSISTOR(FIXED-COMP)	20		, 00°	~ •				0.00798	0.00781	C . CC . C	C17CU
8 9 4	RESISTOR (FIXED-COMP)	=		20.	_				27000	0.00322	1.501.1	
10	RESISTOR (FIXED-COMP)			•	~ •				36200.0	0.00783		21967.0
72	RESISTOR (FIXED-COMP)			=	-				i . buuc ı			÷1.50.
	THE BESTON	Ī		20.	- ;				01709	10000	1.60	1.6.1.
ວ	CAPAC 1 TOR (CERANIC)	2		25.	=				1.17346	1.24.54	1.26.534	1.56.16.
2	CAPACITOR (CERAMIC)	ž		35.	~				C.57710	0.41451	C.1727R	9,179.0
2	CAPACITOR (CERAMIC)	ž		15.	~				0.16724	0.17.00	0.17634	0.101.2
513	CAPACITOR (CERAMIC)	ž		20.	~				C.19271	11.205.21	C.217.1	1.22.1
[2	CAPAC 1 TOR (CERANIC)	×		.04	-				0.25052	0.24474	0.27114	としなべら
223	CAPACITOR (CERANIC)	×		Ξ.	2				7.022.0	6.821.91	11111	
C33	CAPACITOR (CERAMIC)	2		30.	•	٠			0.59465	0.63320	C. 64 170	9:1.9:1
5	CAPACITOR (TANT.	CSE		33.	-				0.00884	0.01058	0.01114	6.015°
C1820	CAPACITOR (TANT.	£S)		33.	~				0.0176#	0.02115	11.0222E	5.1, 11.5
673	CAPACITOR(TANT. EL.)	CSR		33.	-		•		0.00k84	A.010.	0.01114	ט ט ט נייי
C3 2		ž		۶.	~				0.21449	0.22755	0.23425	
(3843		ž		·.	•	•			C.42807	6.1.54.0	1. 461.50	
773		2		٠.	_				0.03241	0.06.14	0.07:045	0.1.1.0
C4546	CAPACITOR (VAR.	3		Ť	~				0.11772	6.15565	C. 16 '	4.4.513
64748		2		*	~				0.111.82	0.15565	0.17788	9.404.14
CSC	CAPACITOR (CERANIC)	ž		₹	~				C.92501	207.16.0	S 77 :50° U	1.1 5. 47
CS3		2		10.	~				0.28594	057220	C* 41.145	7.712.1
C 25	CAPACITOR(DIP. MICA)	5		.	-				6.00549	0.0140°	25 L 5 J	
CS 3	CAFACITOR (VARIABLE)	2		۶.	~				C.044×3	L. 13r 2r	1.,141,91	
360	CAPACITOR (CERANIC)	ž		۶.	m				0.24323	0.260.2	0.24 44"	1
C 6 5	CAPACITOR (CERAMIC)	2			~				0,16161	11.17400	(.17:52	
	RF TRANSFORMER/COIL			•	=				0.42304	0.49510	0.51747	1.2442.1
	CONNECTOR			j	~				6.26356	1.41953	1.57.51.8	2.5. 11
	CONNECTOR			•	-		•		0.11104	0.22456	6.24.22	£ . 60 . 3
								;	*****			
	IDIAL PAILURE MAJES FOR IMIS LEVEL	7 167	L AKE	:				90	64.rU3ra	\n***\		7

CONTRACT	CONTRACT MLS PROGRAM		EQUIPMENT SMALL COPE AIRE FQ.	SMALL	EACU	A 1 B B	F9.	DATE	DATE 2/26/76 MFV	A Y				
ASSEMBLI	ASSEMBLY ACTIVE EQUIP	SUBA	SUBASSEMBLY ANGLE REC/PROC	E REC/	PROC		HOAPP	HOAPD FRONT END	9 2	Ξ	INTERNAL TEPPERATUPT BIST	EPPERATU	IPT BIST	Ë
ERVIROR! (F.R.1) (D DEGI	ENVIRONMENT/TEMPERATURE CONDITION (F.R.1) AIRBORNE, INNABITED (F.R. C. BEGREES C.	167710H (F. 25	TION PAIRS FOLLOW (F.R.Z) AIRBORNE,INHABITED 25 DEGREES C	E . 1 N H A	181760		F.R.3) AIRNOR 30 degrees c	AIRDORNI Ees c	(F.R.3) AIRBORNE,IMHARITED 30 Degrees C		(f.R.4) AIRFORMF,IMHANIIED 54 DFGPFES C	SAMF, THE	11110	
CKT PART SYMBL DESCR	CKT PART PART NON-STO PERCT OTV F.R. REV ERROR (F.R.T) (F.P.2) (F.P.3) (F.".4) SYMBL DESCR TYPE PART NO. STRESS SPURCE CODE	PART	NON-STD PART NO.	STR	55	7	PURCE	> 1	EPROR CODE	(1.8.1)	(F. P	~	PERCT OTY F.R. REV ERROR (F.R.1) (F.P.2) (F.P.3) (F.".4) STRESS SOUNCE CODE	(1, 1)
•	PIODE (NY MINER)	(35)	10, 2 1.10003 24.05411	=	10. 2	2	t 1 t t 1	i ! ! !	1 1 1 1 1 1	18.42584	20.62199	99 21	21.10003	24.05411
TOTAL FA	TOTAL SATISTER BATES FOR THIS LEVEL ARE	S LEVE	1 ARE						18	.42583	20.621	96	18.42583 20.62199 21,10993 24.03	26.05

CONTRACT	ACT HLS PROGRAM	222		EQUIPMENT S!	SMALL COMM AIRM FG.	IIAN FO.	DATE	2/24/74	BE <			
ASSEMBLY	BLY ACTIVE EQUIP	7100	SUBA	ISSEMBLY ANGLE REC/PROC	REC/PROC	8048	B. f. B	. Nobul E	Ē	INTERNAL TEMPFHATURF	ATHRF "ISF	2
6 0 B	ENVIRONNENT/TERPERATURE CO (f.r.1) Airrorne, immabited () degrees c	RATURE CO Immabited	COMP1710N ED (F.	PAIRS FOLLOW R.2) AIRRORNE/IMMARITED i degrees (, IMMARITED	(F.R.3) 30 DEG	A TREORN	(f.R.3) AIRPORNE/IMMABITED 30 DEGREES C		(f.r.4) AIRPORNL/IMMAKITED 54 begres c	JNHAGITED	
Ct T SYNBL		1 9 9 1	PART TYPE	NON-STD PART NO.	PERCT 917 STRESS	F.R. Source	a f	FREOR	(1.8.1)	(f.#.2)	(۲.۴.3)	4.1.1)
	QUARTZ CRYSTAL	rat.		FILTER XTAL	0.0				1.20000	1.2000	1.20000	1.20960
=		TAL			ė,	_			0.2000	0.2000	0.21:00	4.2000
5	MICROELEC.	LINEAR							0.96259	1.05.45.	1.12401	C7124-1
A - 1 4	MICHOELEC.	LINCAR				•			7,43007	0.84.0	146.21.2	77077
<u> </u>		SS1/8S1						,	0.41639	0.43249	0.43913	7 (7 7.0
6		\$\$1/H\$1			•				0.69120	0.73235	6.746.76	0.86616
~n	CROELEC.	LINEAR							1.06709	1.19120	1.25489	2.107.72
<u> </u>		LINEAR							0.769%	0.84710	95.44.0	1.420.0
\	MICROFLEC. L	LINEAR				_			7,000	0.4775	2/3/A C	0.007
. 4		551/851			::				0.41639	0.43249	0.43513	9.9.9.9
-			RPR		.01				0.26952	0.35705	0.37190	170.50
8					27. 1				1.21693	1.59750	1.(P.66.6	7.27533
63	STOR	(15)	2		9.	_			0.11554	0.15428	0.14184	0.21064
= :	0100E (S1)		9		•				0.07368	0.12514	0.15707	1.213/4
70	DIODE CHU MI	XER)			• •	_		•	55.81065	\$0.0850.04 \$1.00	00117	
7 6 0	TOAMS		2 2		7				14675	01881	74.00	25256
C H 2-4	_		2		15. 2				0.79796	46726	1.01152	127.77
CB3	_		G		5. 2	_			C.12815	0.22192	1.24511	1.7 1.0
6 - (RESISTOR (FIXED-COMP)	(ED-COMP)	20		r.				0.00108	0.00289	602.66	11,04.17
2 "	ALSISTOR (FIXED-COMP)	STOR (FIXED-COMP)	Z 0						0.00063	20154	0.00184	75 500 0
2 4	3 3	STOR (FIXED-COMP)			2.0				0.00312	.00.00	116.0	
	RESISTOR(FIX	STOR (FIXED-COMP)	# C #		•				0.00054	0.00135	0.00141	0.0017
9	RFS1STOR (F1X	STOR (FIXED-COMP)	8 C8		33.				6.00092	0.00232	C. 1111.270	5/2 T 111 " C
~	3	STOR (FIXED-COMP)	# C #		 	_	,		0.00519	0.01244	7,710,0	0.07427
E 6	MESISIOR (PIN	SICK(FINED-COMP)	¥ 0			_			0.00000	0.00155	19101.0	() (III) ()
=======================================	RESISTOR (FIX	STOR (FIXED-COMP)	RC 28						0.00058	0.00140	C.10103	0.00
R12	RESISTOR (FIX	STOR (FIXED-COMP)	HC.		19.				0.00072	0.00177	1.00212	4 . 5 1.11
R13.	RESI	STOR (FIXED-CORP)	E :		10.				0.00041	0.00148	0.00177	0.00k.1k
# 14 Ja	Kes	5108(*) XEG-COMP.)	¥ -						19 65158	0 11313	20777	
R1617	RES	STOR (FIXED-COMP)	R C B		1. 12				0.00622	0.61495	0.01701	2 1 7 2 2
K 2021	RESISTOR (FIX	STOR (FIXED-COMP)	# C #		1. 12				0.00622	0.01495	1.4.1.1	11, 17 1 1
H22	RESISTOR (FIX	STOR (FIXED-COMP)	8 C 8						0.00052	0.00125	C.CC142	0.06 **
H 2 3	RESISTOR(FIX	STOR (FIXED-COMP)	RC 8		.53.			_	F.86.0°2	6.00232	1.11.75	.2 4 1:1 - 1
824	RE S I	STOR (FIRED-COMP)	æ ;		-,				0.00052	0.00124	J. 00 16 2	277 10.0
2117	CAPACITORCERABIC	TANE COLUMN	<u> </u>						0.2650 0.020	03702 0	23170	
C110	CAPACITOR (VAR.	ID. CER.)			10,				14297	0.18730	0.21.60	
35	CAPACITOR (DIP.	IP. HICA)			1. 7				1.0.741	0.101.0	2000	776.26.11
C112	CAPACITOR (CERANIC)	BAMICS			10.	_			1.59215	1.53.47	\$1.4.1	1
C 2 0 2	CAPAC J TOR (CERANIC)	RAMIC)	ž		-				11.20713	0.11/41	14:4:	1: 141 :4

ASSEMBLY ACTI- ENVIRONMENT/T (F.R.1) AIRBO O BEGRES C	ACTIVE EQUIP	, 6119			940						
CALINOMNE (F.R.1) / O DEGRI		1000	SUBASSEMPLY ANGL!	ANGLE REC/FROC		<u>.</u>	FOBULE	=	INTERNAL TEMPTERATURE ALSE		÷
	ENVIRONMENT/TEMPERATURE CONDITION PAIRS (F.R.1) AIRBORNE/IMHABITED (F.R.2) A O DEGREES C	(F.		FOLLOW PBORNE, IMHABITED S C		R.S) AIPPOR PEGRES C	(f.R. 5) AIRPORME, IMMARITEB 30 PFGREES C	 	.4) AIRPORME, IMMADITE DEGREES, C	THE STIFF	
		PART	MON-STO	PERCT	ATY F.P. SOURCE	BEV	F9909	(1.8.1)	(1.1)	(f.f.3)	(1.8.4)
C213 CAP	CAPACITOR (CERANIC)	, CK	, , , , , , , , , , , , , , , , , , ,	11.		, , , ,		0.08468	0.09081	0.09.00	17460"0
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	CAPACITOR (CERANIC)	¥ ;			- 1			C. 074.33	0.07015		165.7.1
C224 CAP	CAPACITOS (TERANIC)	.			` ~ ~			000 VO U	80740	0.02312	92 : 40 : 0
	CAPACITOR (TANY, EL.)	25		0	- •			0.02587	0.03095	6.03260	2 / / 7 / 3
	CAPAC I TOR (CERAMIC)	3		6	•			C.24865	0.26665	0.27035	1.2.713
	CAFACITOR (CERAMIC)	5		•	~		•	C.15268	0.16257	U.16463	0.174.6
	CAPAC 1108 (CERAMIC)	2		24.	~			0.24405	0.24170	0.2653	0.2-37
	CAPAC STOR (CERANIC)	ž		12.	2			0.15144	0.16046	0.16257	0.17207
	CAPAC 1708 (CERARIC)	5		≟,	~ ;			0.14234	0.15100	0.15280	0.1/1/2
	CAPACITOR (VARIABLE)	<u>.</u>			~ 1			29590.0	0.13773	2001.0	0.5.1.0
_	CAPACITOR (CERAMIC)	¥ ;		ทั้ง	~ -			0.14247	0.15115	0.15795	
114 CAP	CAFACILOR (CERATIC)	٤ ۵		•	- ^			1879U 3	4444	7600	36.5
	CAPACITOR (CERARIC)	2 2		24.				0.12202	0.13085	0.13269	0.1:1.0
820	CAPACITOR (CERAMIC)	×		. 72	~			0.24405	0.26170	0.20538	11.27.17
	CAPAC 1 TOR (CERAM1C)	3		٠,	_			0.08108	0.08694	C. 6.7 x 16	11.64.27
C21 CAP	CAPAC 1 TOR (CERAN1C)	X		12.	-			0.07572	0.08033	0.0:120	0.657115
	CAPACITOR (CERANIC)	<u>ح</u>		24.				C.11239	0.11967	0.12119	~/ % < 1
	CAPACITOR (CERANIC)	.		15.	- - ,			0.08362	0.0800	0.09417	7150011
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2	CAPACITOR(CERAMIC)	z :		. 7.	•			4) L) L 0	0.122.0	(221.0	
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	CONTROL			• •	٠.			0.3577		1.000	
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ē i	CONNECTOR			.	- 1			0.07326	0.13774	0.150.53	1.575.1
	CONNECTOR			•	~			0.86356	1.41053	1.56563	2.50.10
				;				0.04236	0.114.051	6.1517	2.5.7.0
17-5 RF	TRANSFORMER/COIL			•	• ~			0.16966	40.44.0 44.85.0	,	
	TO PERSONAL PROPERTY COLUMN			.	`-			07670	0 1.4.951	15120	
	TRANSFORMEN/COLL				- ^			0.05461	0.0000	0.10754	0.140.4
	TRANSFORMER/COLL			S	. 20			0.37113	0.43987	11.466.55	1 2 3 1
U10 RF	TRANSFORMER/COIL			6				0.04230	0.04051	C. (517)	11.17.12
							**	766354	30474 34	66 77 95	60378 600

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ENVIRONMENT/TEMPERATURE COMBITION PA (+.R.1) AIRBORNE,IMMABITED (+.R.2 () DEGREES (25 DE	TURE CONSIDED	ITION PA		IRS FOLLOW) Airborne, innabited Grees C	.	(f.R.3) AIRHOI 30 DEGREES C	AIRHORN IFES C	(f.R.3) AIRHORNE/IMHABITED 30 DEGREES C		F.R.4) AIRPOI 54 OFGRFES C	(F.R.4) AIRPORME, IMHARITED 54 OFGREES C	
CKT PART		PART	HON-STP PART NO.	PERCT	710	f.R. Source	P F C	RFV ERROR CODE	(F.B.1)	(F.R.1) (F.P.2)	(f.R.3)	1
HI NA BOR BEBORY) ! ! ! ! ! !	é	•	, , , , , , , , , , , , , , , , , , , ,			9.85816	24.23436	31,13185	115.01211
3				6	~				2.04615	5.16197		24.87/14
UM MICROFLEC.	154/155				~				2.55138	2.80428		3.676.5
UTO MICHOELEC.	SS1/HS1				~				2.34553	2.56254		3.27 870
MICROELEC.	18W/188			•	~				1.24918	1.29748		1.45452
MICROFLEC.	SSI/HSI			•	_				0.48273	0.50792		0.572:0
MICROELEC.	SS1/HS1			•	-				0.41639	0.43249		7,747.0
MICHOELEC.	LINEAR				_				0.046.3	1.04326		1.717.1
MICROELEC.	IEAR			0	-				0.84626	0.03542		1.59841
		PNP		Э.	_				0.14226	11.20216	11.215/3	0.25572
TRANSISTOR (SI)		PNP		60 .	-		•		0.56896	0.56896		A. 5. ROK
0100E (6E)		9		-	-				0.05879	0.15619		N. 424.74
· 9108E (S1)	•	66		-	~				0.05542	00000		0.17259
RESISTOR (POT-COMP)		2		, 0,	-				11.00037	14.22634	-	73.727.9
A) RESISTOR(FIXED-COMP)		===		m.	_				0.00054	0.00129		3 2 2 2 2 3 3 3
RESISTOR (FIXED-COMP)	_	2		10.	-				0.00061	0.00147		0.01416
A3 RESISTOR(FIXED-COMP)		25		-	~				0,00057	0.00137		0.EX.S.0
		101		-	-				0.00057	0.00137	0.00163	0.00.57
R6 RESISTON(FIXED-COMP)		2		3.	-				0.00054	0.00129	L. Cu154	0.00359
K7 RESISTOR(FIXED-COMP)		RCR		×.	<u>-</u>				0.00054	0.00129		0.00150
RESISTOR(FIXED-COMP)		121		۳.	-				£.00054	0.110129	0.01154	0.07.534
H9 RESISTOR(FIXED-COMP)		# C #		•	_				0.00059	0.00141		0.00100
A)U RESISTOR (POWER-FILM)		-		÷	_				0.00686	85400.0		0.01113
mil mesiston(Power-Film)		# X X		ις.	-		•		0.00679	0.00848		27.11.C
R12 RESISTOR(FIXED-COMP)		101		-	_				0.00087	0.1010	C.fu237	1.00551
A13 RESISTOR(FIXED-COMP)		BCR		-	-				C.0005¢	0.00125		0.111, 544
#14 RESISTOR(FIXED-CORP)		1 2		7.	-				0.0005A	0.00140		0.003.1
SWITCH, TOGGLE/PB	8/13			•	~				1.26000	1.2666		3.27.14
SUITCH, ROLARY-MP	-H-				۰				98.49288	98.49R	•	#6 YO 7 . NO
CONNECTOR				.	-				0.269#1	11.5109R		1.1.1
CONNECTOR				ċ	-				91572.0	0.444.0		0.0177
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IN 19891 SIME BOTES FOR THIS INTO I	FOR THIS	IEVE	ABE					148	148.85240	120.96105	100,02527	205 626
PINITE BERREIS AKADI				•								

ASSENBLY	SUBASSENBLY	BOARB		(F.R.1)	(f.R.2)	(f.R.3)	(****)
ACTIVE EQUIP	ANGLE REC/PROC	ENVEL OPE PROC	(4= 1)	38.56366	46.91083	0-1772-35	106.27/155
ACTIVE EQUIP	ANGLE PEC/PROC	DIGITAL PROC	:	83.5258	105.75352	114.78016	21.7.58656
ACTIVE EQUIP	ANGLE REC/PROC	PROCESSOR 1/0	(0= 1)	37.09559	40.12817	54.60917	119.0.454
ACTIVE EQUIP	ANGLE REC/PROC	POWER SUPPLY	(4-1)	18.49953	.24.56127	24.40434	41.1273
ACTIVE EQUIP	ANGLE REC/PROC	SYNTHES17ER	:	62.A0386	79.44201	85.4115411	150.01441
ACTIVE EQUIP	ANGLE REC/PROC	FRONT END	(0= 1)	18.425#3	201.02199	21.11093	24.0541.0
ACTIVE EQUIP	AMELE REC/PROC	H.F. MOBULE		74.15226	85.86808	88.42022	107.57517
ACTIVE COUIP	ANGLE REC/PROC	RAIN FRAME	•	0.89559	1.58214	1.7777	7.91.107
ACTIVE EQUIP	ANTENNA SUBSTST		(0.1)	1.13843	1,91052	2,11143	3.51721
ACTIVE EQUIP	CONTROL PANEL		•	148.85260	170.99105	180.87527	110929-502
OVERALL FAILURE A	VERALL FAILURE RATES FOR THIS FRUIPHENT	ARE		485.94976	586.77551	02777-929	1051.14"21

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1.03422 0.33539 39.05239 23.72709 0.52000 1.56000 7.45556 1.39879 0.42687 1.24.2587 1.24.2587 1.24.2587 1.24.2587 1.24.2587 1.24.2587 1.24.2587 1.57999 1.57999 1.57999 1.57999 1.57999 1.57999 1.57999 1.57999 1.57999 1.57999 1.57999 1.57999 1.57999 1.57999 0.43824 0.13709 0.95264 15.23926 15.23926 1.52000 0.44480 0.44480 0.44480 0.44480 0.44480 0.44394 1.59999 1.59999 1.59999 1.59999 1.59999 1.59999 1.59999 1.59999 1.59999 1.59999 1.59999 1.59999 1.59999 1.59999 1.59999 0.10465 0.10465 0.19732 11.00436 0.19736 1.52000 0.52000 0.520000 0.520000 0.520000 0.52653 0.56653 0.66653 0. 017 COMPONENT TYPE

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APPENDIX F

THE EFFECT OF RAIN ON THE MLS PHASE III RADOMES

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THE EFFECT OF RAIN ON THE MLS PHASE III RADOMES

The Basic Narrow and Small Community systems at NAFEC have experienced monitor shutdown several times this summer during heavy rainfall. The system monitor indicated a Beam ERP fault on the azimuth antennas. The Beam ERP is set to indicate a fault at the -3.0 dB level. During a recent storm the Beam ERP was closely monitored and a level of -2.5 dB was observed during a period of fairly heavy rainfall. The drop in ERP was suspected to be caused by rain water on the array and monitor horn radomes. This was verified with a simulated rainfall test using a NAFEC Fire Department engine to spray water on the antenna. A -11 dB reduction in Beam ERP was experienced when the array antenna was sprayed and -4 dB when the monitor horn was sprayed. These were the maximum values observed under an extremely heavy rainfall simulation, probably not naturally possible.

The significant difference between the two antennas may be due to the difference in the physical size of the two antenna radomes or the differences in the radome material. The larger area of the array radome may allow a thicker water film to build up on its surface. The different radome materials can have significantly different water-shedding or wettability properties. The monitor horn radome is teflon fiberglass which has excellent water shedding properties due to its wax-like surface finish. The array radome material is a polyester resin and its watershedding properties are probably highly dependent on the condition of its surface finish. A dull, weathered surface would be considerably worse than a new, shiny surface. It should be noted that the Basic Narrow array radome has been in the field over a year and its surface is probably fairly weathered due to exposure to the elements. The technician on-site reports that he observed a much higher degree of water filming and surface wetness

on the array radome as compared to the monitor horn radome.

RF attenuation due to rain water on radomes is a well known problem and has been extensively investigated. See attached Essco paper, "The Effect of Rain on Satellite Communications Earth Terminal Rigid Radomes". Several radome manufacturers have addressed this problem in their design by employing a Dupont Tedlar film on the radome surface. This material not only has good water-shedding properties, but also provides excellent protection against ultraviolet radiation and solar heating. Tests have demonstrated that a one-mil thick Tedlar film has a life expectancy in excess of 30 years.

A one-mil thick film of Tedlar is normally applied to the radome outer surface at the time of manufacture by a bonding process. Tedlar tape is also available, coming in 72-yard rolls up to 36 inches wide, and having a thickness of approximately 3-mils, which could be applied to the existing MLS radomes in the field.

A suggestion was made that we simply wax the array radomes in the field to increase their water-shedding properties, understanding that a wax finish can only be expected to last four to five weeks. In view of this, it is suggested that we wax the Basic Narrow radome in the field as a temporary fix and repeat the simulated rain test to determine if this alone is adequate to solve the rain attenuation problem. If not, then an overhanging roof extension can be added to the antenna case to protect the radome from direct rainfall.

If waxing the radome significantly helps the rain attenuation problem, than a permanent fix would be to cover the existing radomes in the field with Tedlar Tape. Two 72-yard rolls of Tedlar tape have been ordered for this purpose, one 6 inches wide and one 36 inches wide. A two-week delivery has been quoted by the supplier.

NOTE: The on-site technician reports that he waxed the Basic Narrow radome and repeated the rain test. The maximum loss dropped from -11 dB to -7 dB. The next step should be to repeat the test with the Tedlar tape on the radome.

Articles Of Timely Interest Aperiodically Published By The RADOME HOUSE

NUMBER 4

THE EFFECT OF RAIN ON SATELLITE COMMUNICATIONS EARTH TERMINAL RIGID RADOMES

ELECTRONIC SPACE STRUCTURES CORPORATION, WEST CONCORD, MASSACHUSETTS

REPRINTED FROM THE MICROWAVE JOURNAL, SEPTEMBER, 1966

THE EFFECT OF RAIN ON SATELLITE COMMUNICATIONS EARTH TERMINAL RIGID RADOMES

A. COHEN and A. SMOLSKI, ELECTRONIC SPACE STRUCTURES CORPORATION, WEST CONCORD, MASSACHUSETTS

INTRODUCTION

Measurements on the Andover, Maine Communication Satellite Earth Terminal air inflated radome have indicated serious effects due to rain on the antenna system performance. These results, published in the Bell System Technical Journal, have been compared with an expected performance loss through water film thickness determined from a formula developed by D. Gibble of Bell Telephone Labs. Because the messured and the culculated values of the performance degradation appeared to be in agreement, two conclusions have been generally propagated, namely: (1) that water films predicted by the Gibble formulation do exist on spherical radomes, and (2) that other radomes subjected to rain will exhibit performance losses in accordance with the predicted water film thickness as demonstrated by the Andover, Maine installation.

In order to verify the effect that rain would have on a rigid metal space frame radome as contrasted to the air-inflated type, an extensive measurement program was conducted. The results of this measurement program have shown that both above conclusions are inaccurate.

REVIEW OF PREVIOUS RAIN EFFECT MEASUREMENT

The Bell article presented the transmission loss degradacion due to rain on the air-inflated radome at the Andover, Maine Satellite Communication Earth Seation. These measurements of transmission loss vs. the rate of rainfall are shown in Figure 1. It was stated that the high losses measured for the air-inflated radome were due to a water layer or water film on the radome surface. In order to theoretically account for the Andover performance, a formula for calculating this water film thickness as a function of the rate of rainfall was put forward by D. Gibble,2 also of the Bell Telephone Labs.

Using Gibble's formula for calculating the water film thickness, t, caused by various rain rates:

$$t = \left(\frac{3\mu Rr}{2w}\right)^{1/2}$$

where

 $\mu = viscosity of water$

R = mdius of radome

r = race of rainfall

w = density of water

and referring to the transmission loss

vs. water film thickness curve of Figure 2,3 one can construct a curve (Figure 1) which could represent the theoretical loss due to rain as a function of the rate of rainfall. One can observe that the correlation is good and might conclude that the measured losses were indeed due primarily to the various water films on the radome surface.

However, in the Gibble formula, only classical laminar flow has been assumed and, in addition, the initial





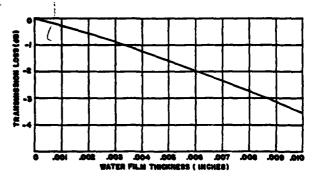






Figure 3 — Seem detail of air in-

velocity of the falling rain drops has been neglected. Both these effects may markedly reduce any possible film thickness on a spherical structure. In addition, several other questions relating to the general validity of the Andover experience remained unanswered. For example, rain water on top of an air-inflated radome as well as sag under its own weight tends to flatten it out. The resulting curvature effects can reduce the rate of water run-off from the radome surface thereby allowing more water to be accumulated. Another concern is the fact that the Andover antenna-radome placement is nonoprimum, the antenna being far off axis inside the radome. It is possible that this has seriously increased the reflected ground noise when water was present. Further, it is likely that the Andover radome fabric soaks up some moisture, at least the first outside fabric layers.

All of the air-inflated fabric types and coatings tend to age due to ultraviolet irradiation, and, in general, these radomes have a fairly short life, partly as a result of the subsequent depolymerization. As an example, Table I shows the results of the water absorption tests on the air-inflated type fabric as compared to the solid fiberglass laminate materials employed in rigid space frame radome designs. Note the

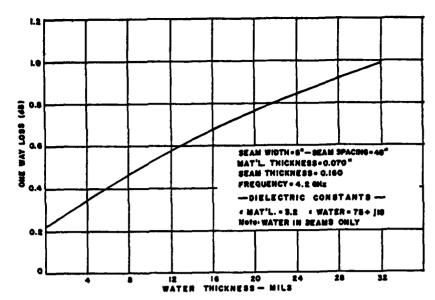


Figure 4 - Loss on Andover type radome.

relatively large percentage of water absorption for the air-inflated material and the resulting changes in the electromagnetic characteristics of the material.

In addition, the seams of an Andover type air-inflated radome are approximately 5-inch lap joints covered with 20 mil hypalon tape giving an effective thickness in excess of 0.160 inches. These seams are spaced approximately 4 feet apart at the equator tapezing soward the top and bottom of

the radome. The very important point here is that the seams are much stiffer than the main "window" area of the radome, and when the radome is inflated with internal air pressure, these seams may not expand to the same spherical surface as the main membrane areas. The result is, in effect, a corrugated surface with the main membrane areas protruding further outward than the seams, as illustrated in Figure 3.

Table I
Dielectric and Water Absorption Properties of
Hypolon Coated Dacron Fabric and Fibrous Glass Reinforced Laminate®

		Hypalon C	oated Dacron F	ıbric		
		3 GHz (S	ample #1)		8.5 GHz (Sample #2)
	K		er Absorption Weight	K		er Absorption Weight
Scandard Conditions	3.12	0.014		3.12	0.012	
After Water Immersion	6.79	0.080	13.2%	6.16	0.133	10.5%

Fibrous Glass Reinforced Laminate
(in accordance with MIL Specs MIL-R-7705, MIL-R-7575 and MIL-P-8013**)

		3	GHz		8.5	GHz
	K	Tan 8 War % by	er Absorption Weight	K	Tan 8 Was % by	er Absorption Weight
Standard Conditions	3.98	0.0113		3.97	0.012	
After Water Immersion	4.02	0.0152	< 0.5%	4.02	0.015	< 0.5%

[.] William B. Westphal, Laboratory for Insulation Research, MIT.

MIL-P-8013 Plantic materials, polyester resin, glass fiber base, low pressure laminated.

MIL-R-7705 Radomes, general specification for.
 MIL-R-7575 Resin, polyester, low pressure laminating.

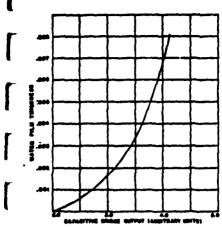


Figure 6 — Meseurod water film vs. bridge output.

Accordingly, the air-inflated radome is made up of vertical corrugated sections which, upon rainfall, can in effect act as rain gutters. The falling water thus can form very high density electromagnetic scattering ribs regularly spaced in the form of a diffraction grating. Figure 4 is a theoretical calculation of the transmission loss that is to be expected when rain water of various thicknesses flows in the seam

corrugations only. Note that only small corrugations in the order of 0.03 so 0.04 inches are necessary in order for large losses to be experienced.

Since all of the above comments, inchaling the possible deleterious rain channeling diffraction grating effects, exist for the air-inflated radome it was considered of major importance to thoroughly investigate and clarify the effects of rain on radomes. The following measurement program was therefore undertaken and completed.

MEASUREMENT PROGRAM

The primary objective of the measurement program was to determine the transmission loss which occurred due to rain on a faceted rigid radome surface. A secondary objective was to determine and measure within reasonable accuracy any water film which might form on the faceted radome surface.

Antenna-Radome Setup

In order to perform the transmission loss measurements a precision 30-foot diameter paraboloid was mounted on an azimuth turneable. The entire struc-

ture was enclosed with a 55-foot diameter metal space frame radome. A 6-foot parabola was used at the transmitting station, and 4.2 GHz was selected as the operating frequency. The transmitted signal was modulated at 1000 cycles. At the receiving station the signal was detected, amplified and monitored on the expanded dB scale of a VSWR amplifier. The output was channeled into a zecorder which recorded all test runs. A block diagram of the test semp is shown in Figure 5.

Rain Field

To simulate rain on the radome surface a system of three rotating water sprinklers were positioned on rop of the radome. Each sprinkler had two adjustable spray nozzles which rotated at approximately 140 rpm. Initial tests to establish the rain field pattern of the sprinklers were performed on a level plane. The spacing, relative position, nozzle setting and line water pressure were adjusted to create the desired rain field rates. Rainfall indicators were placed at various locations in the rain field pattern es-tablished by the sprinklers. The combination of adjusting the nozzle settings and sprinkler relative positioning, along with the rapid nozzle head rotation rates, created a very satisfactory simulated rain environment.

The rainfall indicators which were randomly placed at various locations parallel and perpendicular to the antenna aperture plane showed that a fairly uniform rain field could be readily generated. In this manner, rain fields with rain rates of approximately 10, 20 and 40 mm/hr. were established for the tests. The sprinkler system, after calibration, was then placed on the cadome. Sample rainfall indicator tests were repeated in order to assure continuity of calibration and the final tests run.

With regard to the choice of rain rates established for this experiment, it should be noted that the percentage of time in any year for which given rainfall rates are exceeded are not generally available. However, a rainfall rate of 3 mm/hr. is likely to be exceeded for somewhat less than 2 per cent of an average year at Tokyo and for perhaps about 0.5 per cent of an average year at London or Paris. At Halifax, Canada and Washington, D. C. the corresponding values are both about 1 per cent. A rainfall rate of 25 mm/hr. is likely to be exceeded for percentages of an average year

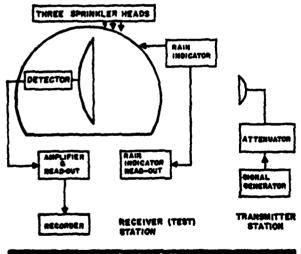


Figure 5 — Block diagram of measurement test set-

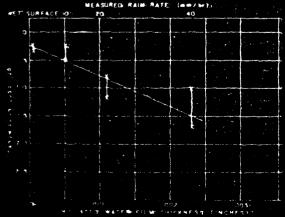


Figure 7 — Transmission loss vs. rain rate and indicated water film

Model No. M35-70 produced by Electronic Space Structures Corp., West Concord, Mass.

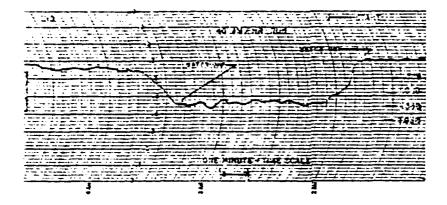


Figure 8 — Typical recorded data run (40 mm/hr.).

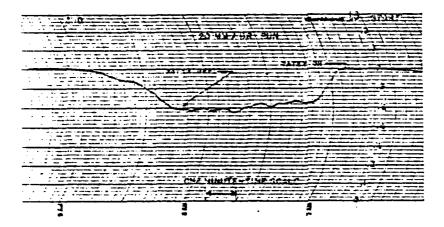


Figure 9 - Typical recorded data ren (20 mm/hr.).

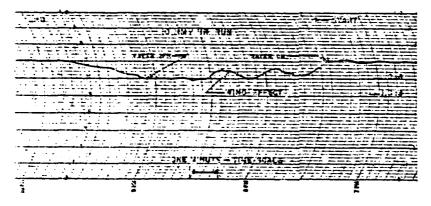


Figure 10 - Typical recorded data run (10 mm/hr.).

varying from about 0.1 per cent at Tokyo to perhaps less than 0.01 per cent at London or Paris. The range of rainfall rates thus established were more than adequate to cover practically all cases to be experienced.

Water Film Thickness Measurements

Considerable effort was expended to develop a measuring device which would indicate the water film thickness

on the surface of the radome. The device selected was basically a capacitance type bridge, the sensing element being a split flat capacitor (4 x 1-1/2 inches) which was secured to the inside surface of the radome. Initially the bridge was balanced with a dry surface. As moisture, water droplets, water streaks or rivulets, or a water film forms on the outside surface, the bridge becomes unbalanced and an

output voltage is generated. The capacity bridge was initially calibrated by depositing measured amounts of water over the area of the sensing capacitor, and a water thickness vs. bridge output curve was determined (Figure 6). During the simulated rain tests the sensing capacitor was mounted high on the 55-foot diameter radome at an angle of about 50° from the horizontal.

Measurement Results

A summary of measured transmission loss values is presented in Figure 7. Typical recorded data runs are shown in Figures 8, 9 and 10. An interesting run is that for the light rain (Figure 10) which shows the effect of the wind on the rainfield. This effect was only prevalent when the combination of light rain or mist and windy conditions existed during the measurements.

In all tests it was noted that it took less than two minutes to recover to within 0.2 dB of the reference signal level. From this observation and from further tests on a small test panel it was concluded that this last 0.2 dB loss was due to a wet surface or separated parches of very thin water films and droplets on the surface of the radome. In contrast, for the air-inflated radome at Andover, the received signal does not return to the essentially dry state for about 30 to 45 minutes, indicating that the high losses observed are not due to large water films but rather to the possible water absorption characteristics, diffraction grating effects, radome curvature effects, etc.

Figure 11 is a graph showing the measured transmission losses. These are compared with the expected transmission loss for a 55-foot radome that would be predicted, based on the Gibble formula and the Andover experience. Note that the maximum measured loss of 1.0 - 1.7 dB for the 40 mm/hr. simulated rainfall is in sharp contrast to (1) the loss of 3.4 dB which would be the value obtained for a film thickness derived from Gibble's formula or (2) the value of about 4.2 dB if one projected the calculated loss curve of the air-inflated radome (Figure 1).

A further observation was that with the heaviest rainfall rate simulated (40 mm/hr.), the water film chickness indicator read from 3.2 to 3.3 units which infers (from Figure 6) that the water film chickness was about 0.0025 inch. The transmission loss theoretically expected from a 0.0025 inch water film is about 0.75 dB (Figure 2). This agrees with the measured results with an accuracy within a factor of two.

An explanation of this discrepancy may be that only one water film thick-

ness indicator was available and installed during this test series. It is very possible that the indicated water film is not representative of the overall effective water film over the entire radome surface. Also, the water film indicator was calibrated by creating a uniform water film over the entire surface of the split sensing capacitor. However, rain on the faceted rigid radome surface took the form of streaks, rivulets and water film patches. Uniform films of any appreciable thickness simply did not exist on the rigid metal space frame radome. In any event, as an initial attempt at measuring and correlating the water film thickness, the results were enlightening.

Figure 11 — Transmission loss vs. rain rate for 55-foot metal space frame radome.

A. Theoretical performance (55-foot radome) — based on Gibble formula Andover type radome. B. Measured losses — untreated radome surface — 55-foot metal space frame radome. C. Measured loss — treated radome surface — 55-foot metal space frame radome.

Radome Surface Treatment

During visual observations of the radome surface during the simulated rain, it appeared that a pattern of rivulets, streaks and various water run-off paths developed. To enhance the water streak and rivulet formation and to inhibit or prevent any water film from forming on the radome, the surface was treated so as to decrease its wetability. As shown in Figure 11, the results were better than anticipated.

Using the highest simulated rain rate (40 mm/hr.), where previous measurements showed 1.0 - 1.7 dB losses, the measured transmission loss was less than 0.3 dB. The water film indicator correlated this value. The capacitance bridge output increased to only 2.2 units from a 2.0 reference. This increase was previously measured when the transmission loss was about 0.2 to 0.3 dB. Also when viewing the treated surface of the radome, during a heavy rainfall, it appeared that no uniform water film existed but that small and many water streaks had formed to rapidly run off the radome in narrow rivulets.

CONCLUSIONS

The results of the measurement program show that even with rain rates as high as 40 mm/hr, the transmission loss through the untreated surface of a 55-foot rigid metal space frame radome is only 1.0 - 1.7 dB. The transmission loss decreases to 0.8 - 1.2 dB at 20 mm/hr, and to 0.3 - 0.5 dB at 10 mm/hr.

If the radome surface is treated so as to inhibit the formation of any water film, the transmission loss will decrease to less than 0.3 dB at the highest rain rate of 40 mm/hr. Since rainfall rates seldom exceed 10 mm/hr. it should be clear that the effects of

rain on a faceted rigid metal space frame radome can be practically eliminated.

Initial attempts at measuring and correlating the effective water film thickness were encouraging. Accuracy within a factor of two for this difficult experiment was achieved.

Recommendations for further effort include direct measurement of the noise temperature attributable to rain on the radome. In this regard, it should be noted that an upper bound to the noise temperature contribution resulting from rain on a rigid radome is, in fact, determined by the transmission efficiency measurements. For example, practically all of the transmission loss is in the form of scattered energy, and for a treated radome surface at 40 mm/hr. rain rates and for angles close to the horizon the worst condition would result in one half of the total transmission loss, or 0.15 dB, being directly absorbed by the "hot" earth. This would cause a noise temperature contribution of approximately 10° K to be exhibited.

Note that as the elevation angle increases (toward the zenith angle) this noise temperature contribution would decrease rapidly due to the shielding effect of the antenna inside the radome. In comparison, from the Andover type air-inflated radome experience, a noise temperature contribution of as high as 65° K was recorded with a rain rate of approximately 2 mm/hr.!

In conclusion, this series of experiments shows that:

1. The Gibble formula for the prediction of water film thicknesses (and hence transmission efficiency) does not satisfy the measured values of transmission efficiency for rigid radomes in rain.

- 2. There is a marked difference berween the performance of the air-inflated (as calculated from the Gibble formula) and faceted rigid metal space frame radomes in a rainfilled environment.
- Water films of only a few thousandths can exist on inclined surfaces before rapid run-off occurs.
- 4. Appropriately treating the radome surface so as to further inhibit the formation of any water film can eliminate practically all the effects of rain, even in rainfalls with 40 mm/hr. rates.

ACKNOWLEDGMENTS

This work was sponsored by the Electronic Space Structures Corp. The 30-foot diameter precision reflector used in the program was supplied by Communication Structures, Inc., West Concord, Mass. William Moseley of Electronic Space Structures Corp. assisted in the physical setup, data accumulation and reduction. Dr. John Ruze, MIT/LL witnessed the experiments reported upon and presented the detailed results at the IEE Conference on the Design and Construction of Large Steerable Aerials (June 6 - 8, 1966).

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